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AFWAL-TR-87-3098 PART IV



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UNSTEADY LOW-SPEED WINDTUNNEL TEST
OF A STRAKED DELTA WING, OSCILLATING IN PITCH

PART IV: PLOTS OF TIME HISTORIES OF PRESSURES AND OVERALL LOADS

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APRIL 1988

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Results of a wind tunnel test of an oscillating straked wing. The report provides unsteady							
airloads and pressure distributions for a range of incidences (-8 to 50 deg.) and ampli- tudes (1 to 16 deg.). The wind speed was 80 meters/second, which provided reduced fre-							
			root chord. Th				
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continuous time history of the pressure and overall loads were measured. Flow visualiza-							
tion was performed for flow of 30 meters/second using a pulsating laser ligh sheet. In part IV, the plots of time history data for both pressures and overall air loads for							
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 $\perp A$ survey of the test conditions and their runnumbers is given in table 10 of part I.

Appendix B includes plots of overall air loads vs. incidence for continuous oscillating model. A survey of the runnumbers of these plots is given in table 11 of part I.

FOREWORD

This report summarizes the results of the windtunnel test of an oscillating straked wing conducted under a cooperative program of research between General Dynamics Fort Worth Division, Fort Worth, Texas, and the National Aerospace Laboratory (NLR), The Netherlands. The model and support system was designed and fabricated at NLR under a separate program with General Dynamics and NLR funding. The test preparation, windtunnel test and reporting were performed at NLR under Air Force Contract F33615-85-C-3013, for the Flight Dynamics Laboratory of the Air Force Wright Aeronautical Laboratories, Wright-Patterson Air Force Base, Ohio. The work was administered by Mr. D.W. Kinsey of the Aeromechanics Division (AFWAL/FIM). Additional technical monitoring support was provided by Mr. T. Cord of the Flight Control Division (AFWAL/FIG).

The program manager and principal investigator was Dr. A.M. Cunningham Jr. at General Dynamics and Mr. R.G. den Boer was the principal investigator at NLR. Mr. den Boer was assisted by the following NLR specialists: C.S.G. Dogger, E.G.M. Geurts, A.J. Persoon, A.P. Retèl and R.J. Zwaan.

This report consists of six parts. Part I presents a general description of the model and test program and a discussion of the results. Part II contains the steady pressure distribution plots and the major part of the zeroth and first order harmonic unsteady pressure distribution plots. Part III contains the remainder of the unsteady pressure distribution plots and plots of the steady and the zeroth and first order harmonic unsteady overall loads. Part IV contains time history plots of the unsteady pressures and overall loads. Part V contains power spectral density plots of the overall loads at harmonic oscillation and time history plots of overall loads for (1-cos) model motions. Part VI contains results of the flow visualization program.

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LIST OF SYMBOLS

ALPHA,α	wing incidence	(deg)
Ъ	local wing span	(m)
bw	wing span (bw = 0.8000)	(m)
вета, в	sideslip angle	(deg)
С	local chord	(m)
C1	wing rolling moment coefficient	
Cm	wing pitching moment coefficient	
	ref. axis = rotation axis $x/cr = 73.27$ %	
Cn	wing yawing moment coefficient	
CN	wing normal force coefficient	
Ср	pressure coefficient	
cr	root chord (cr = 0.7855)	(m)
CT	wing tangential force coefficient	
CY	wing side force coefficient	
DALPHA, da	harmonic oscillation: amplitude of unsteady wing	
	incidence	(deg,rad)
f, FREQ	frequency	(Hz)
1	wing rolling moment (figure 1, part I)	(Nm)
TD.	wing pitching moment (figure I, part I)	
	ref. axis $x/cr = 73.27 \%$	(Nm)
n	wing yawing moment (figure 1, part I)	(Nm)
N	wing normal force (figure 1, part I)	(Nm)
RUN	run number	
t	time	(s)
T	wing tangential force (figure 1, part I)	(N)
	apex: x=0 (figures 1, 5, part I)	
у	spanwise coordinate in wing reference plane	
	(figures 1, 5, part I) y-axis is the rotation axis	;
	x/cr = 73.27 %	(N)
Y	wing side force (figure 1, part I)	(N)
GREEK		
a, ALPHA	wing incidence	(deg)
da, DALPHA	harmonic oscillation: amplitude of unsteady wing	
-	incidence	(deg,rad)
8,BETA	sideslip angle	(deg)

APPENDIX A

PLOTS OF TIME HISTORIES OF PRESSURES FOR CONTINUOUS OSCILLATING MODEL

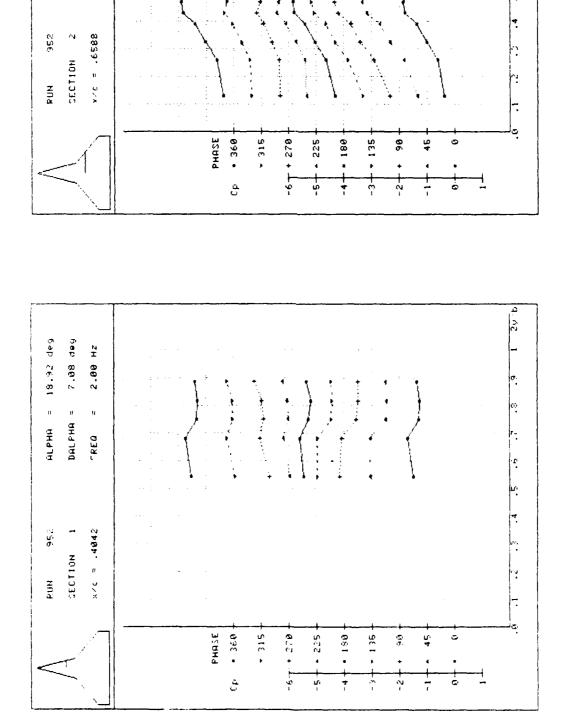
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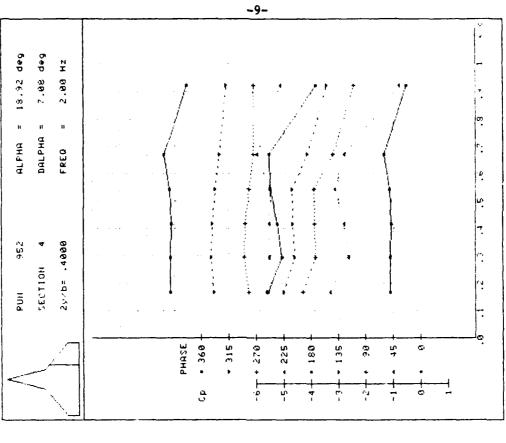
- * x/c indicates the position of the pressure sections relative to the root chord (cr = 0.7855 m),
- * 2y/b indicates the position of the pressure section relative to the wing span (bw = 0.8000 m).

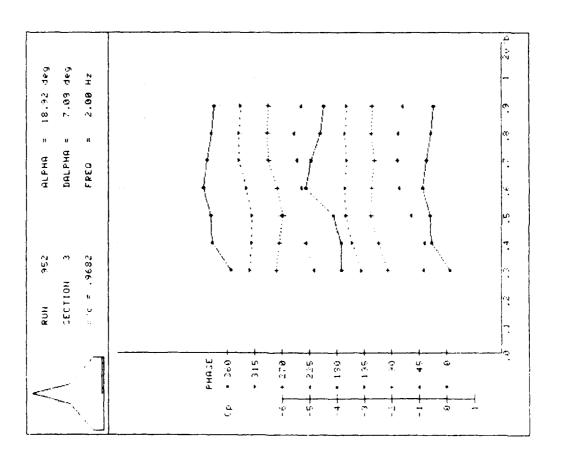
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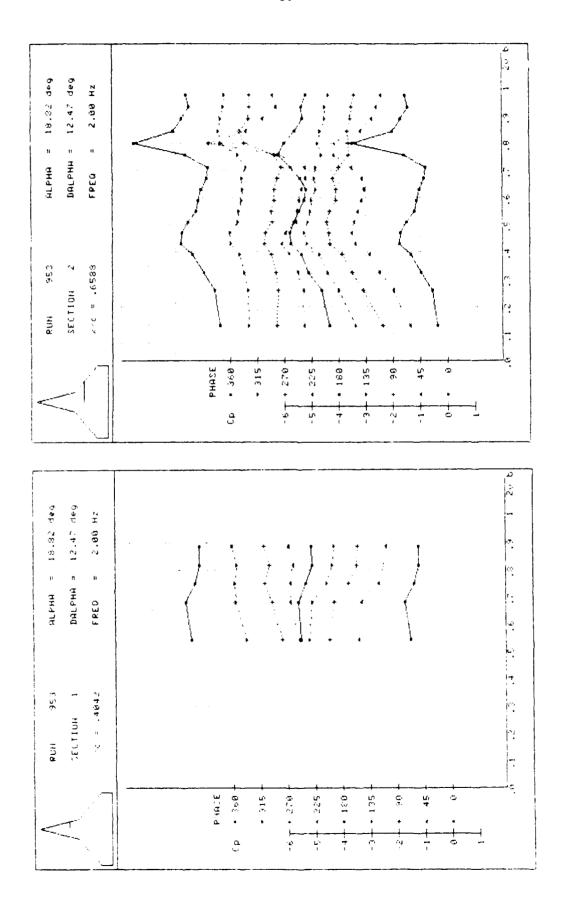


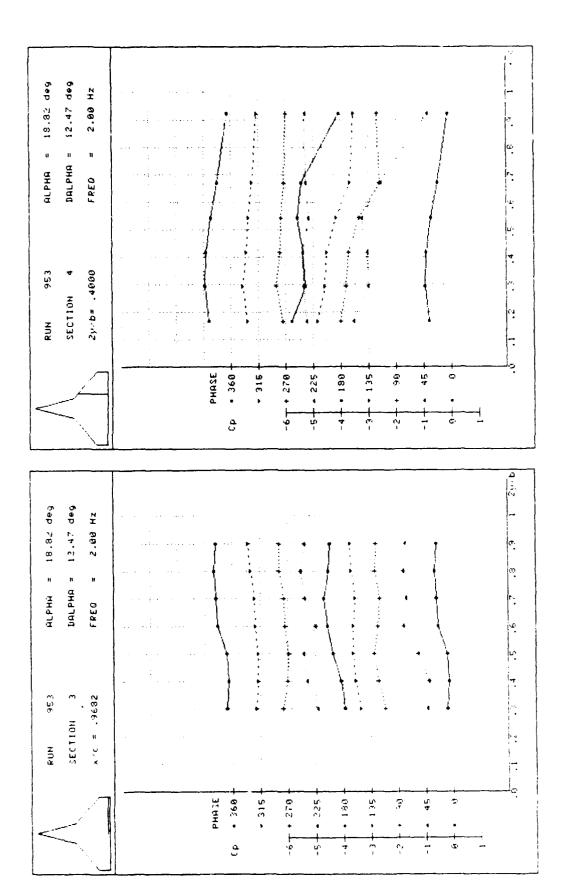


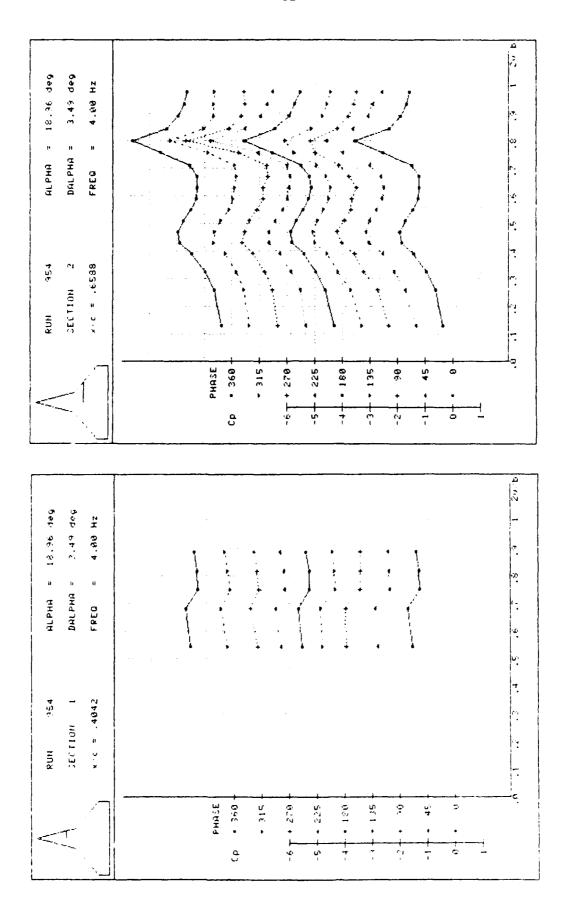


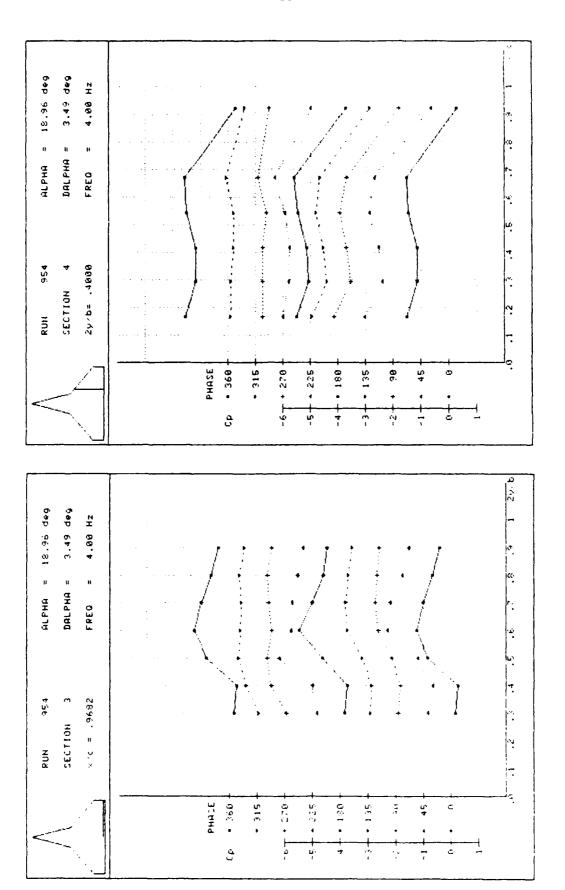
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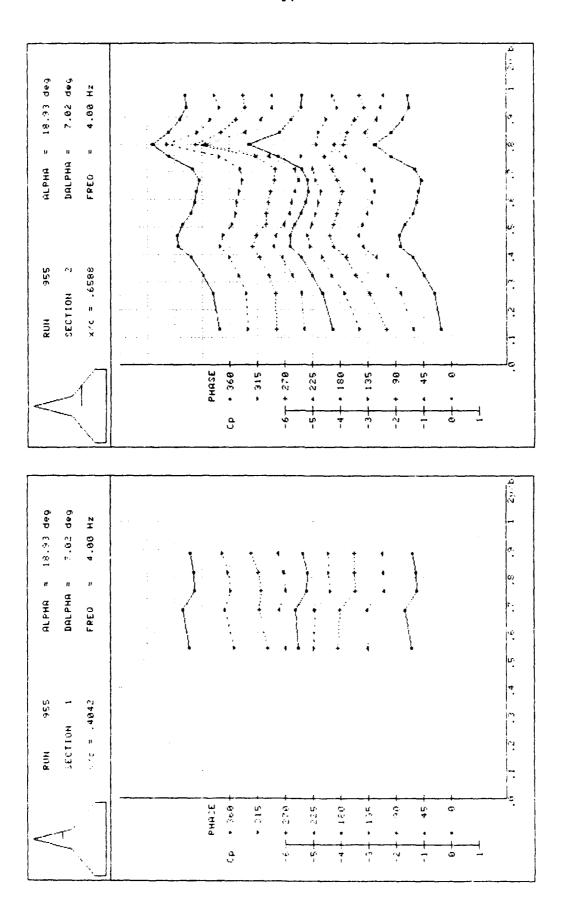
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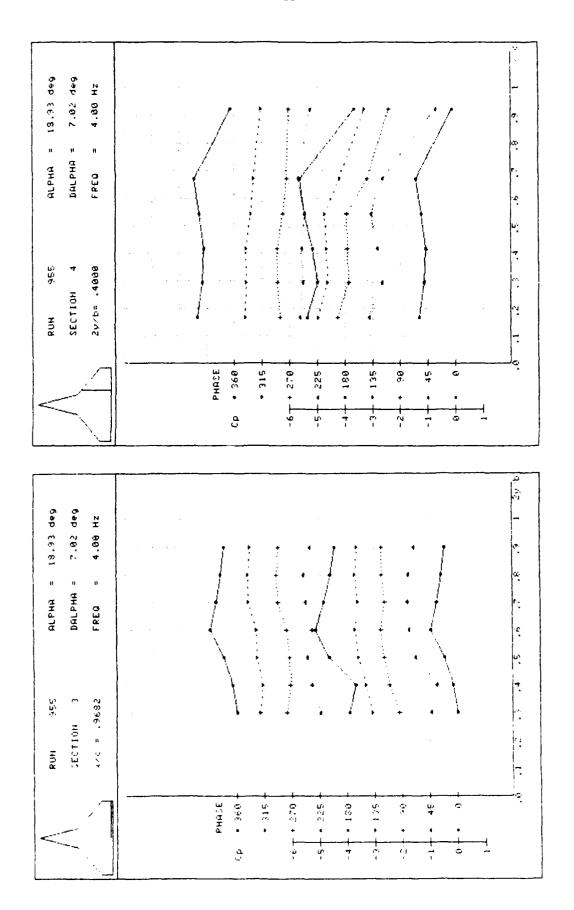


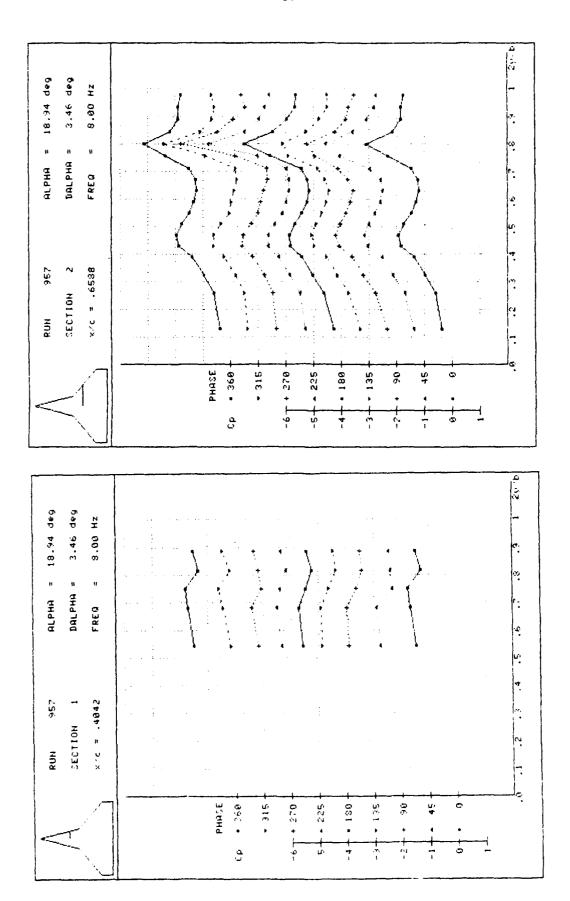


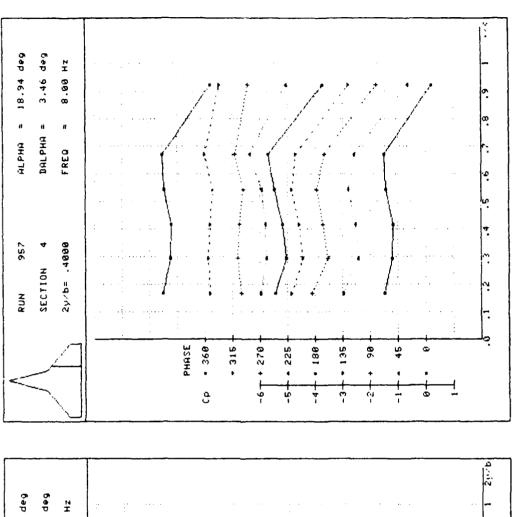


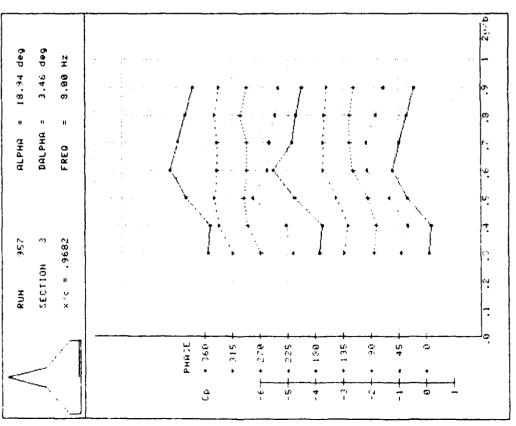




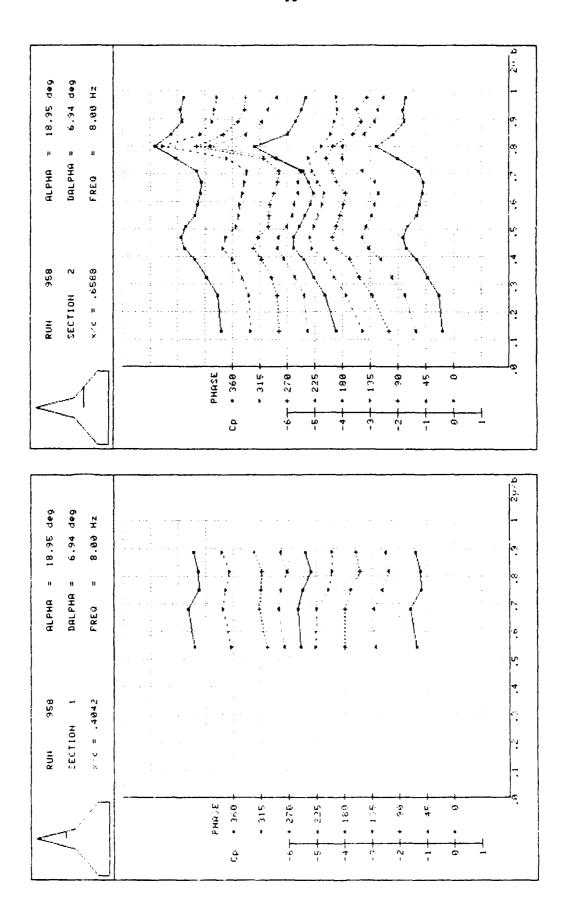


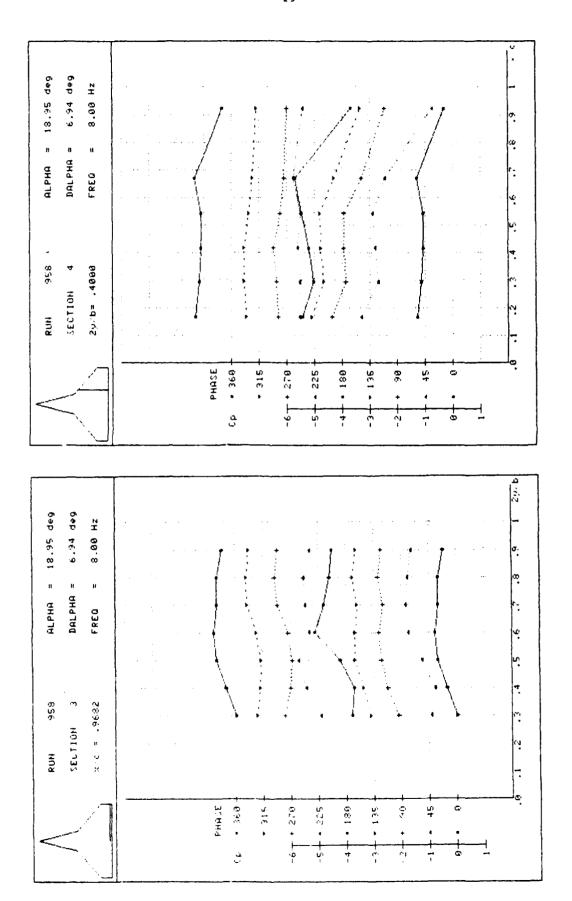


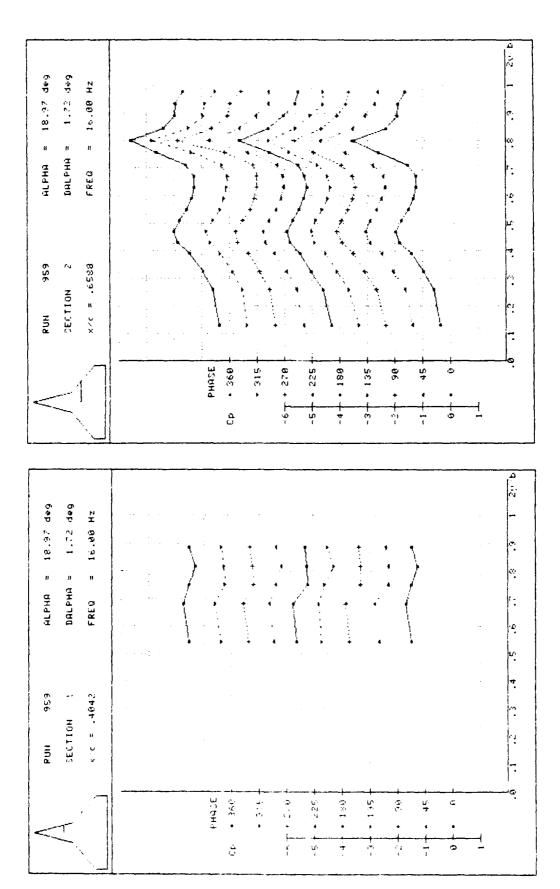


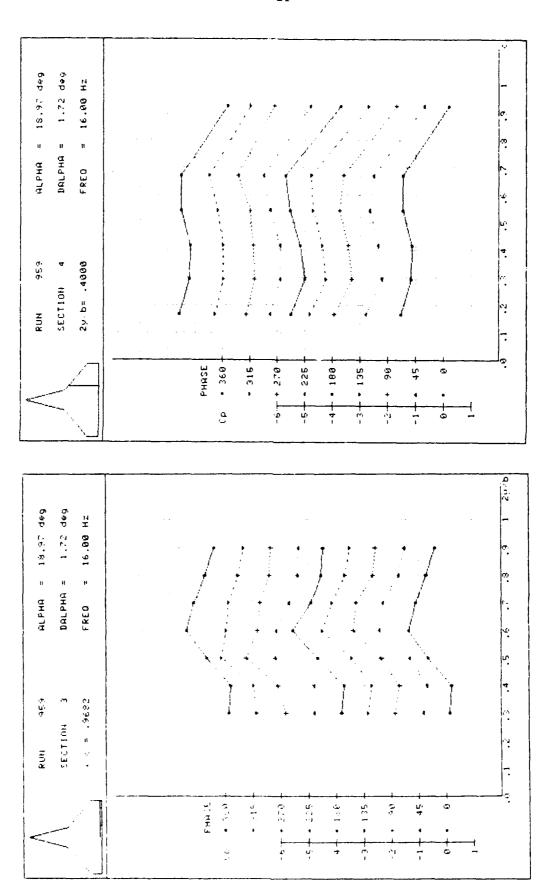


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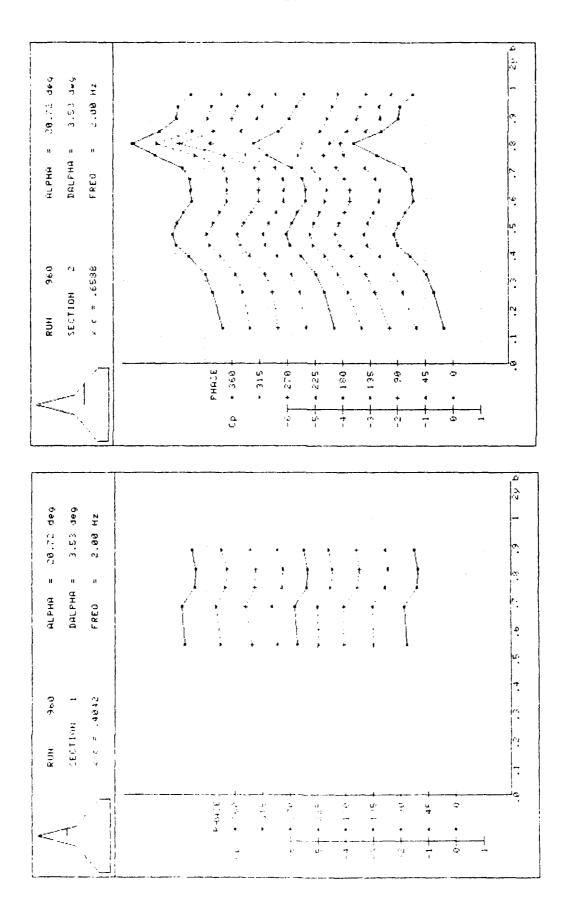




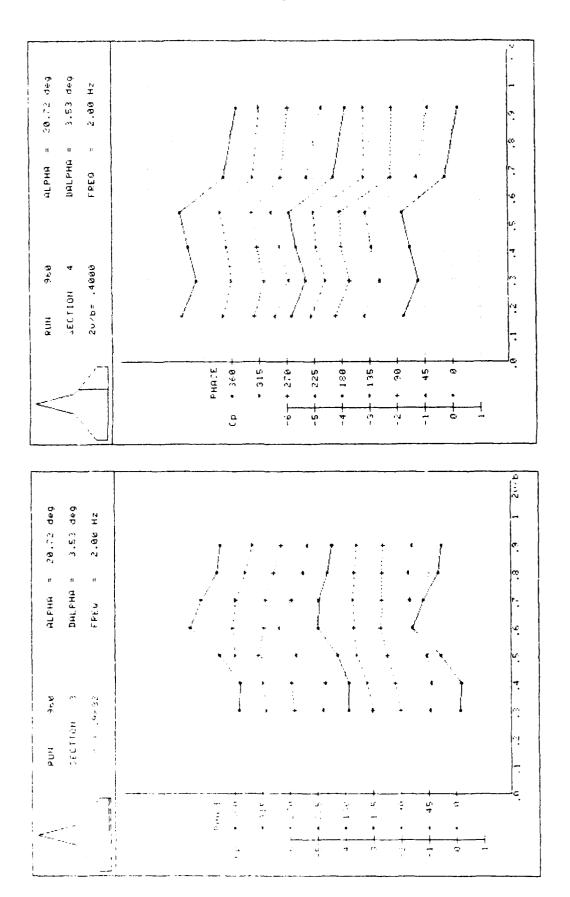


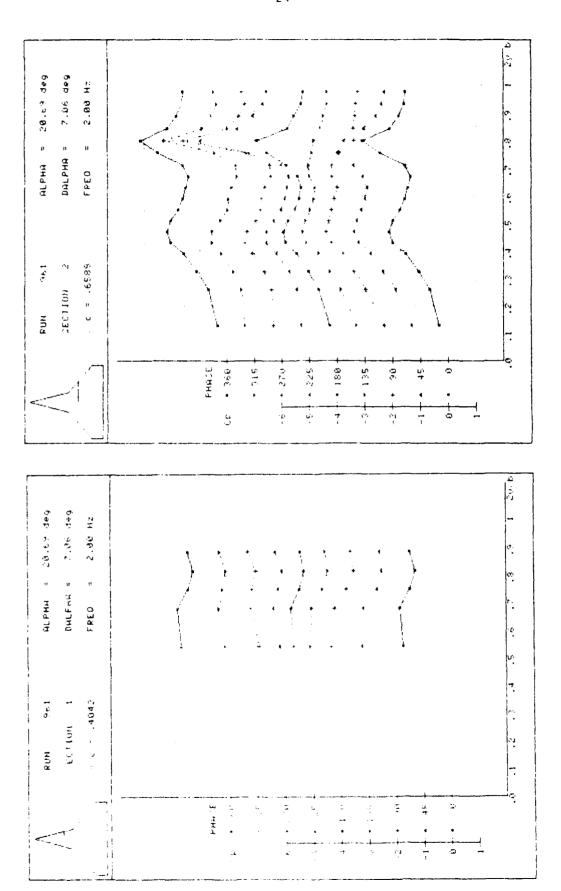


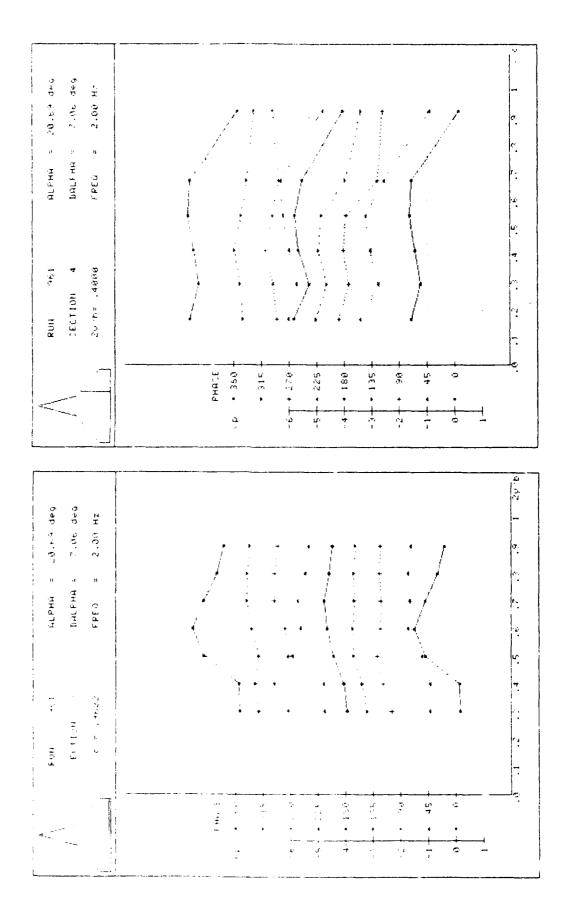
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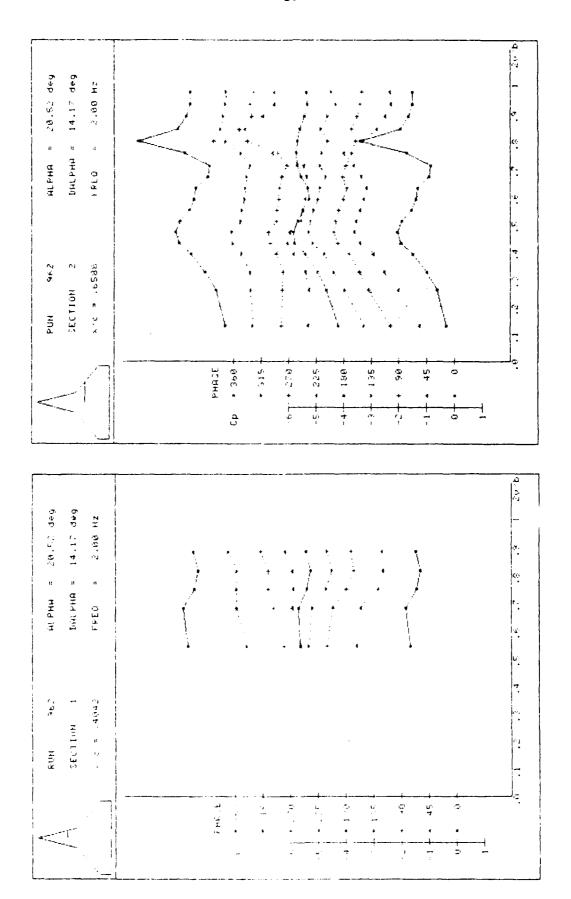
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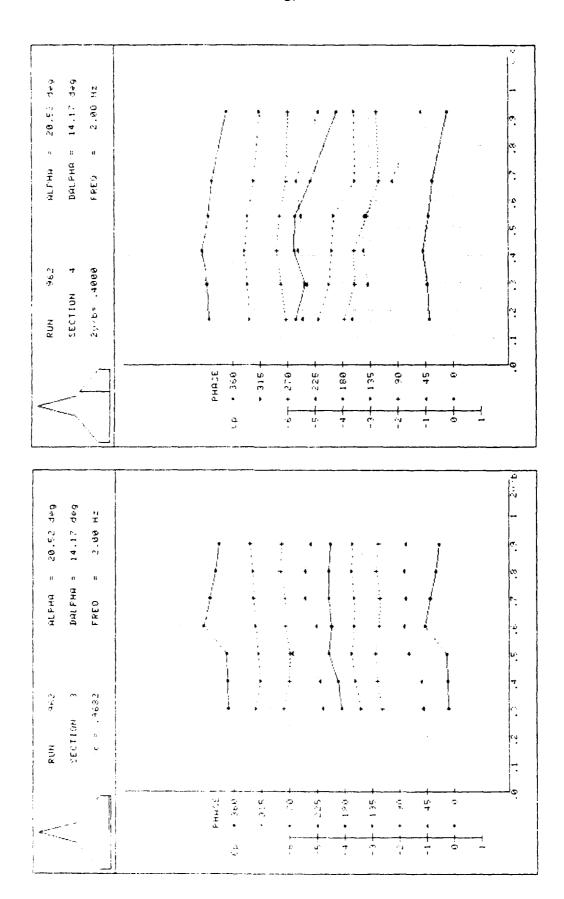




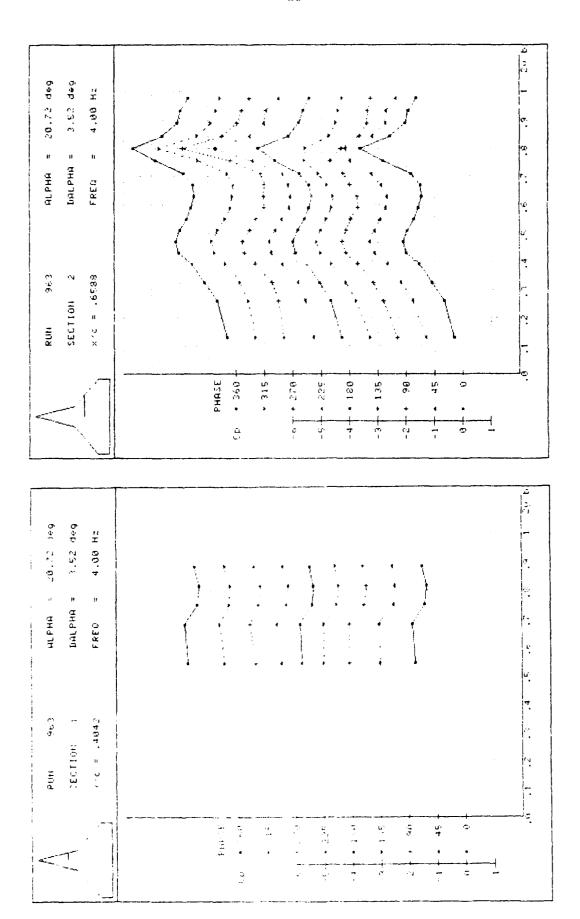


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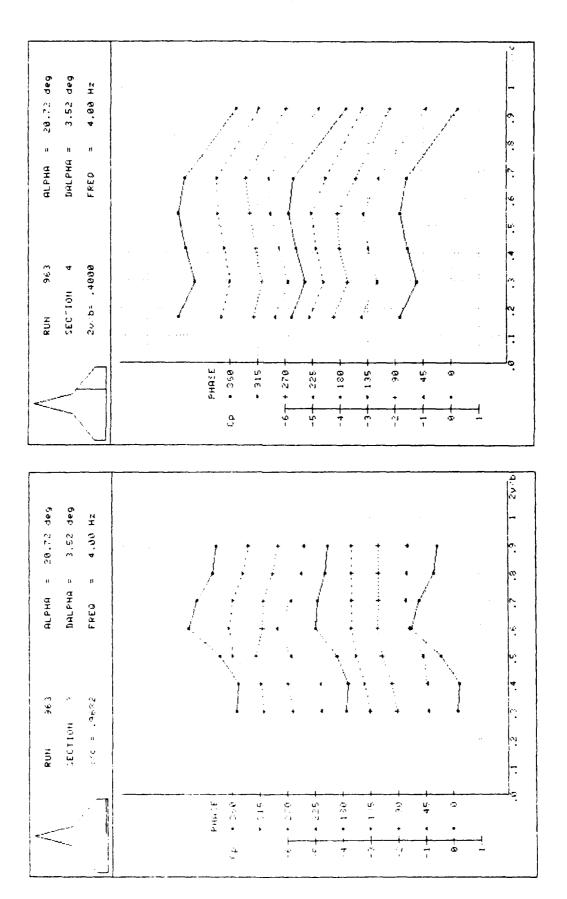


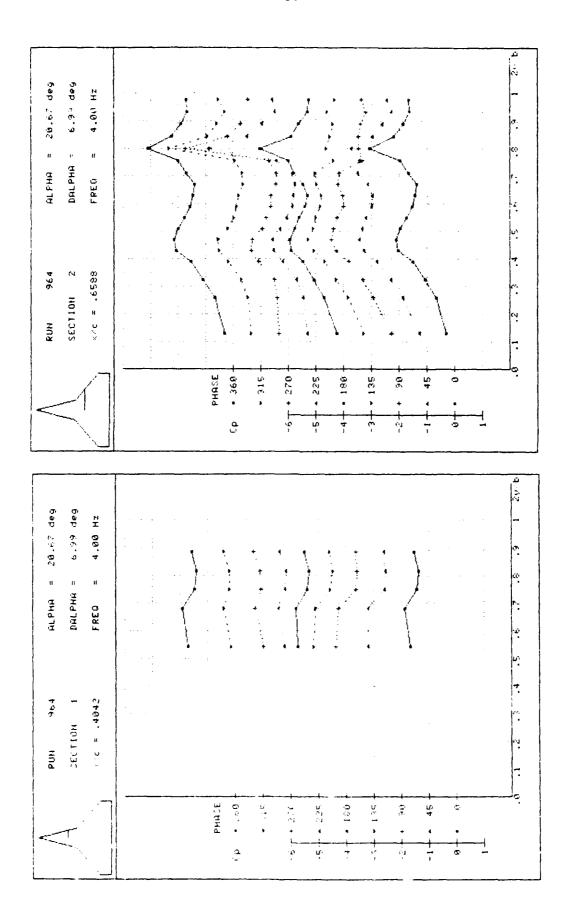


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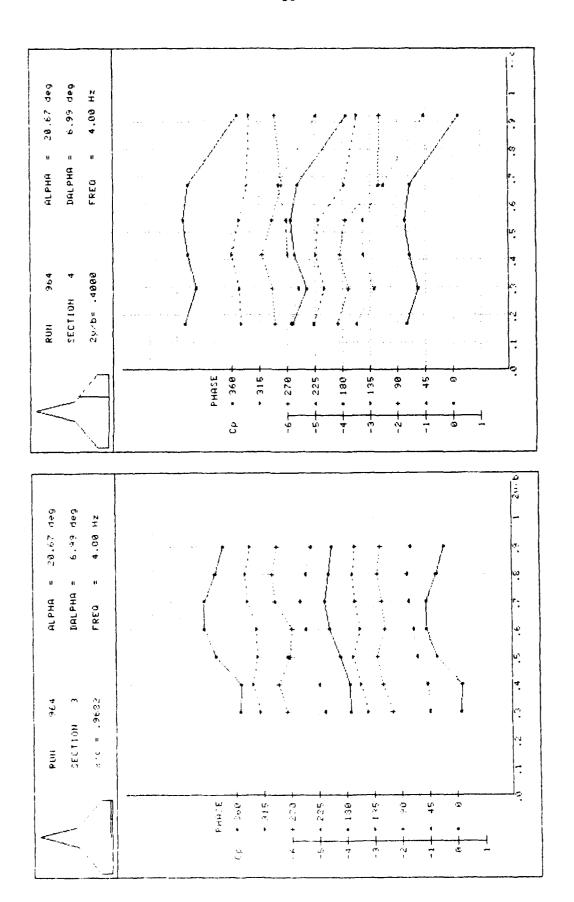


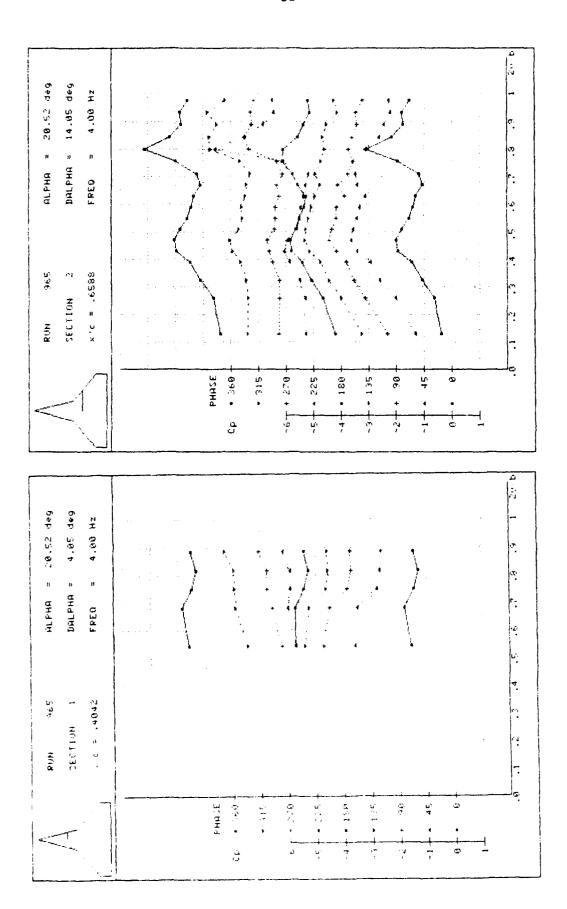
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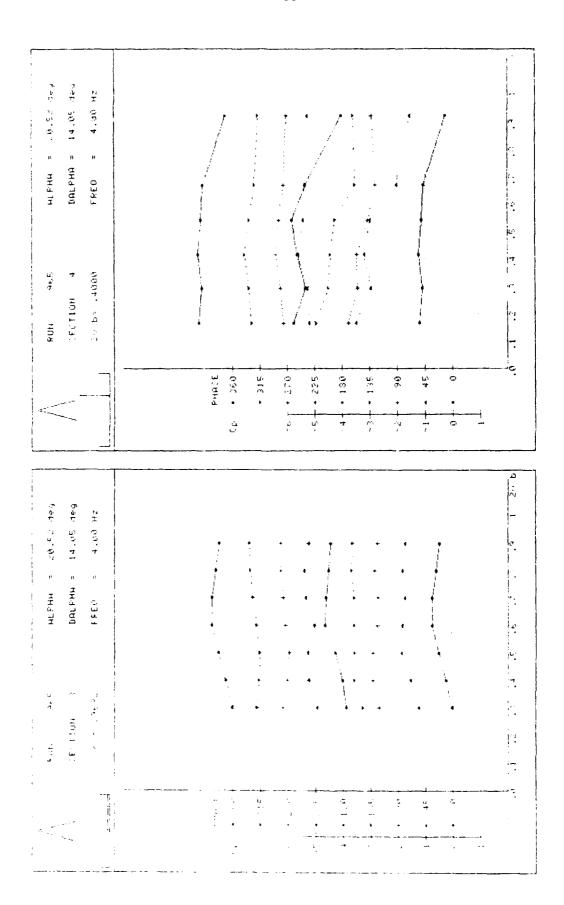


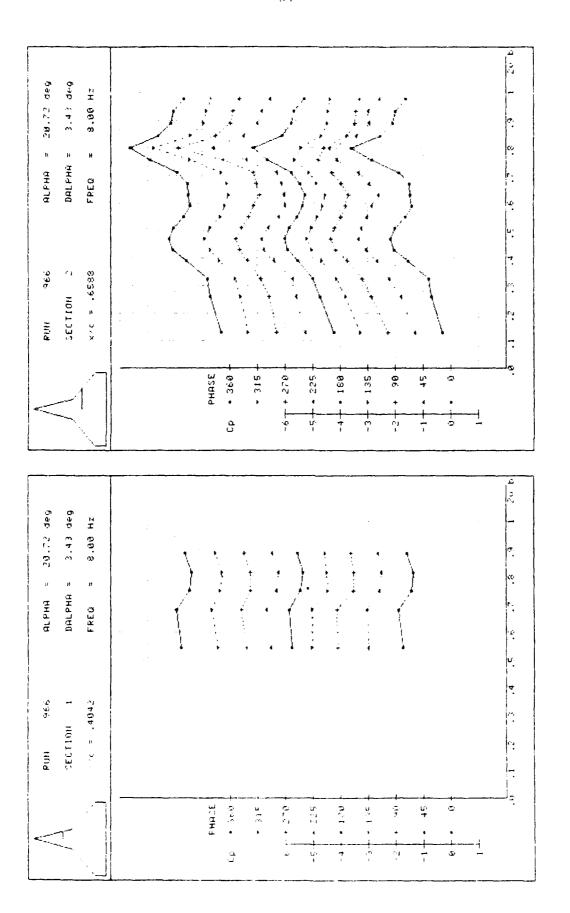
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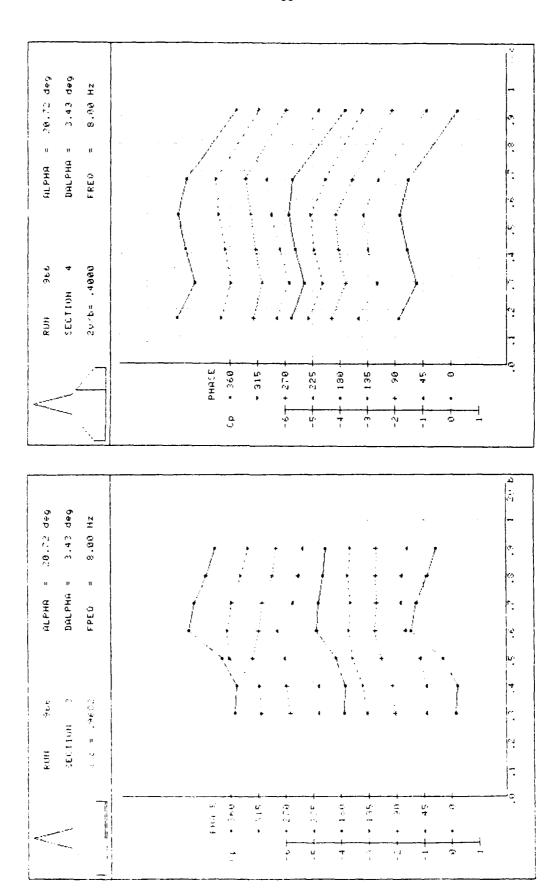


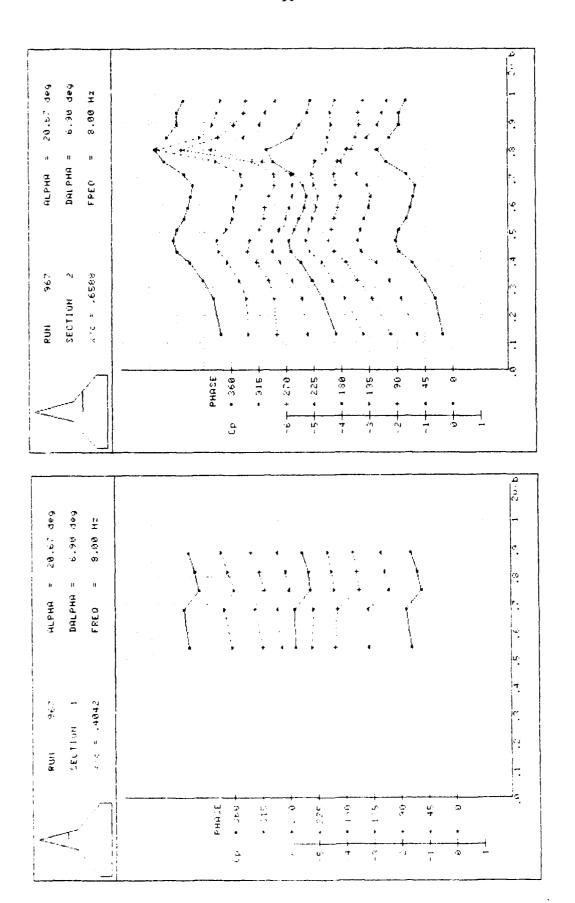


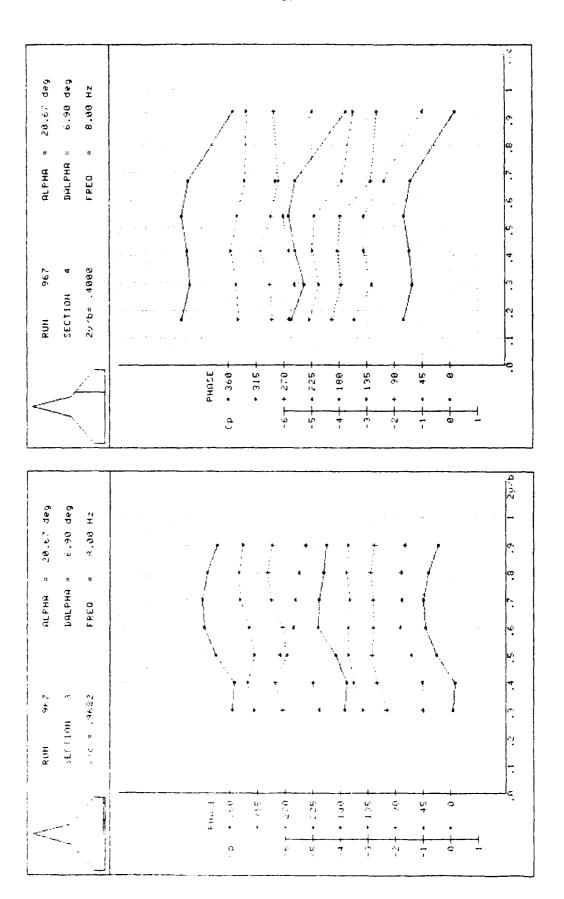
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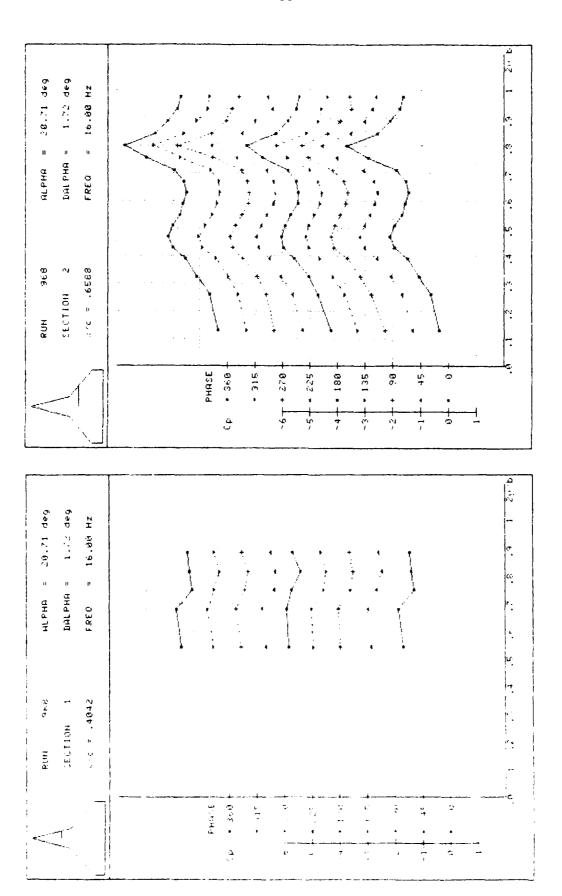


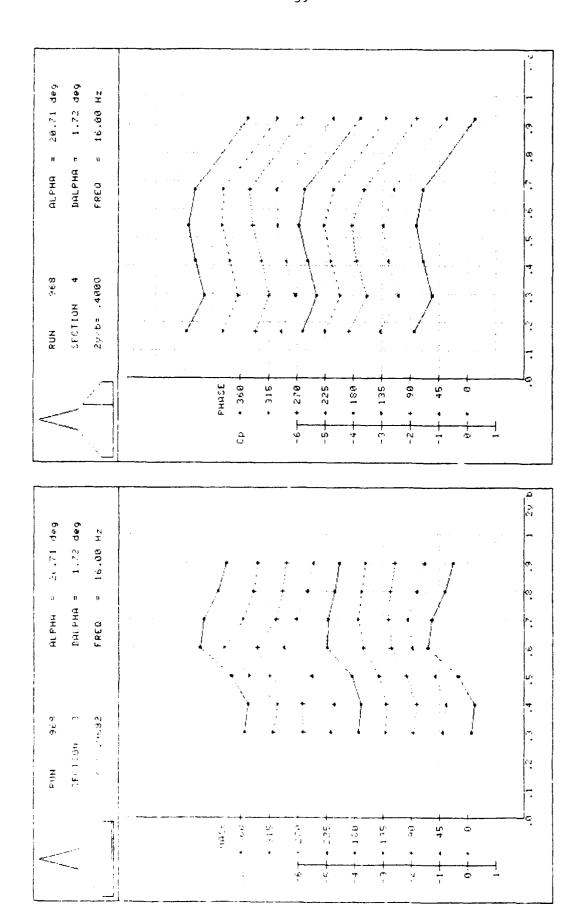




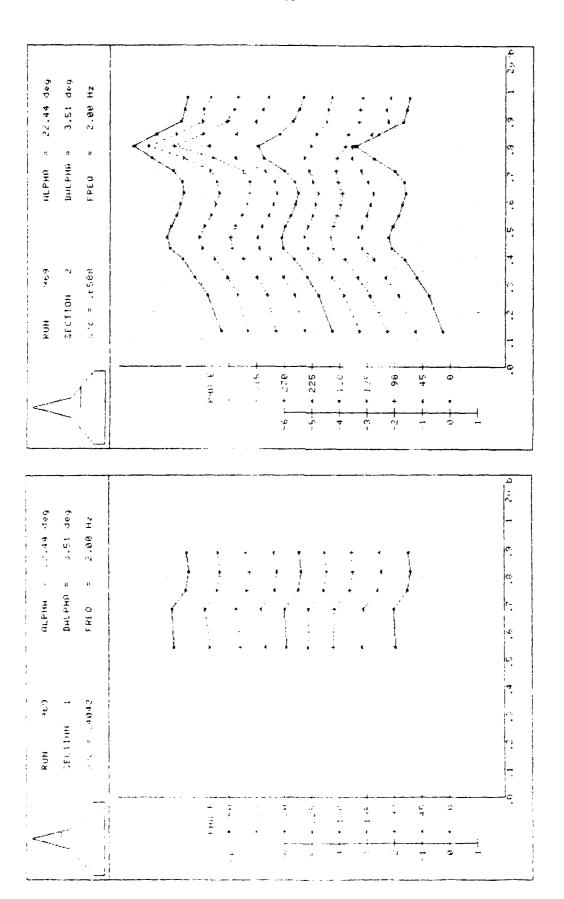


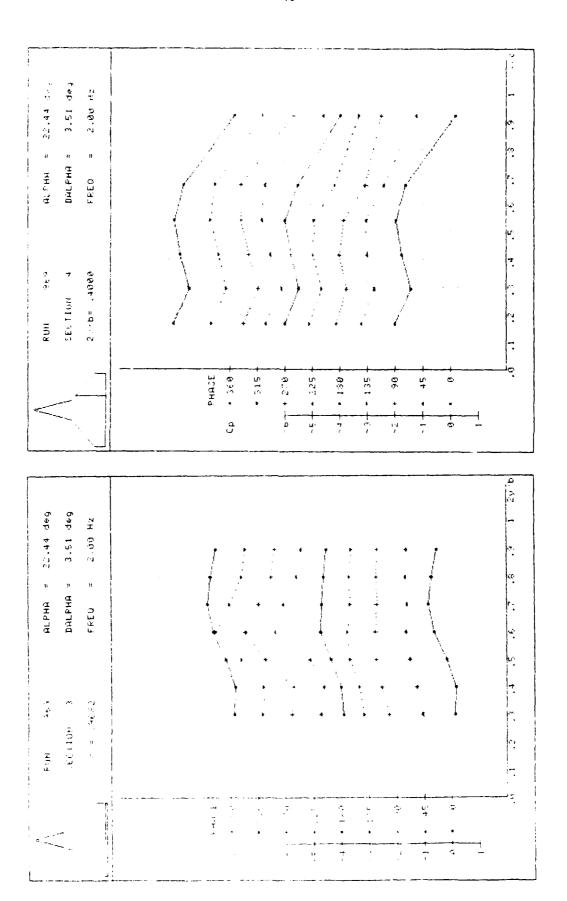


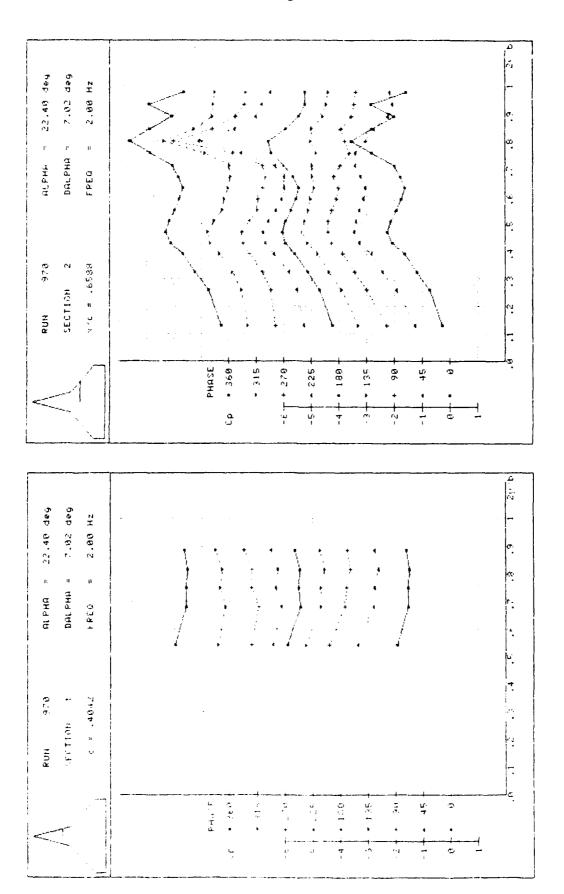


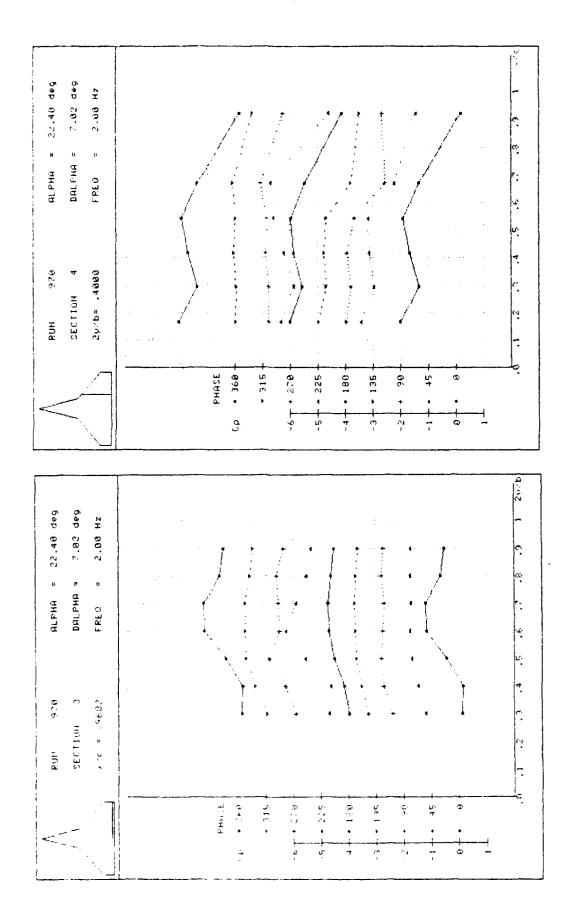


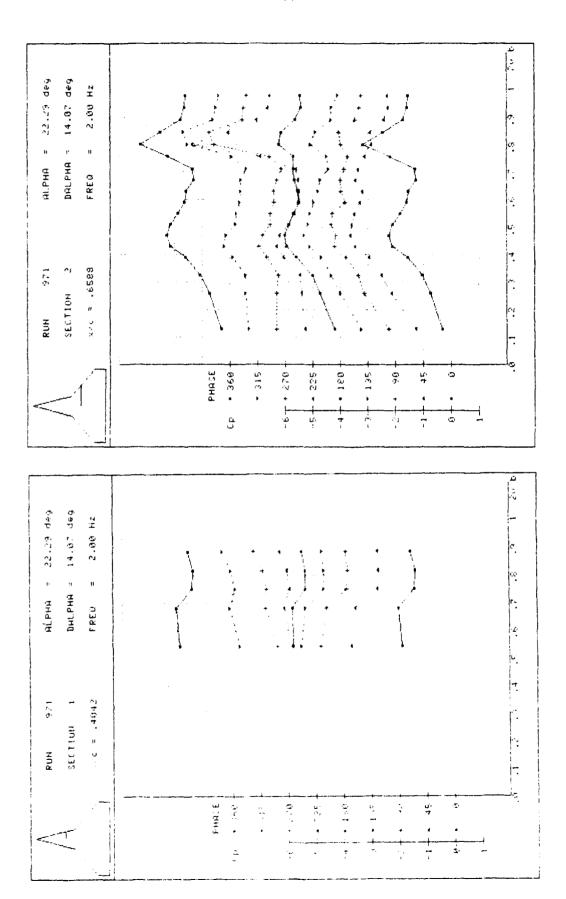
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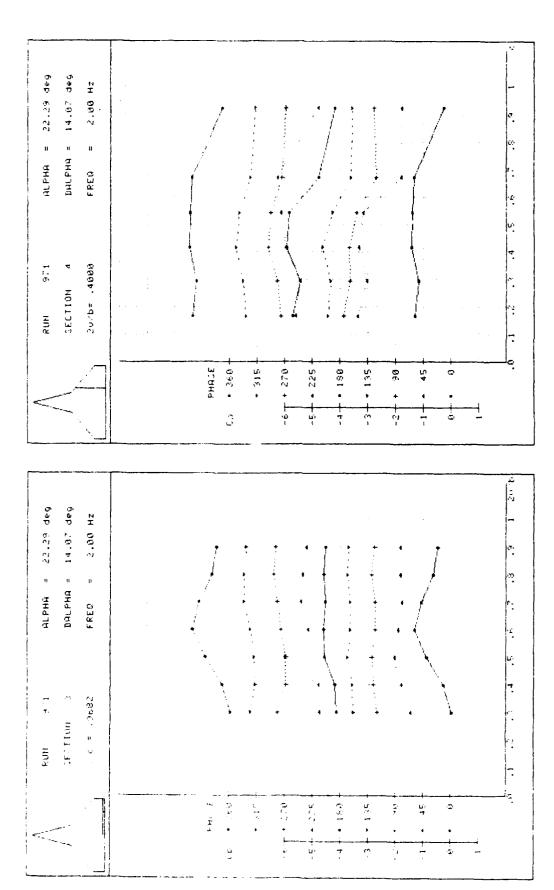




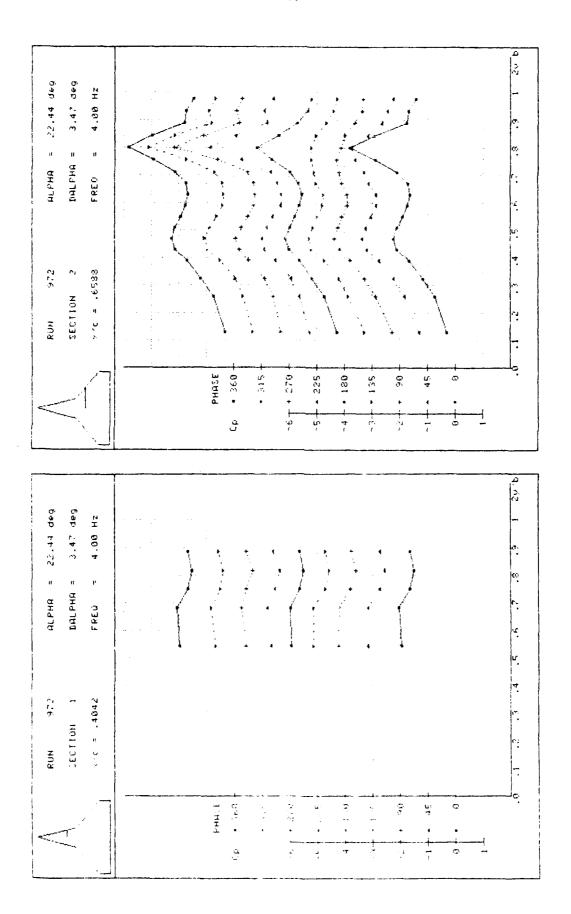


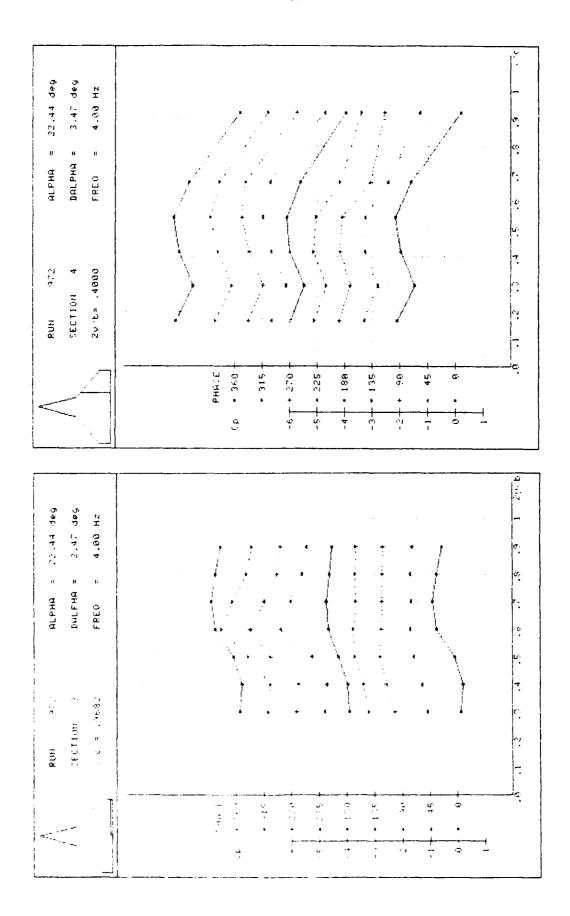


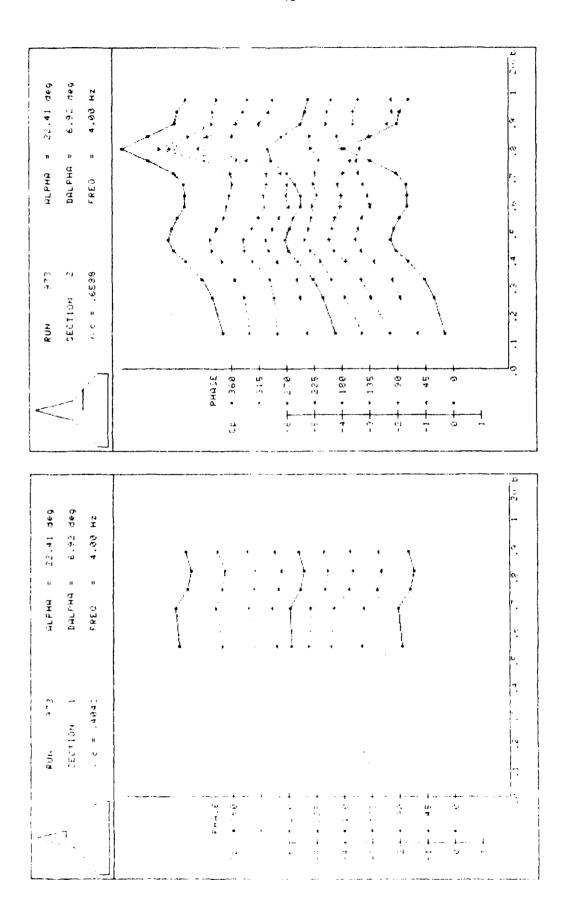


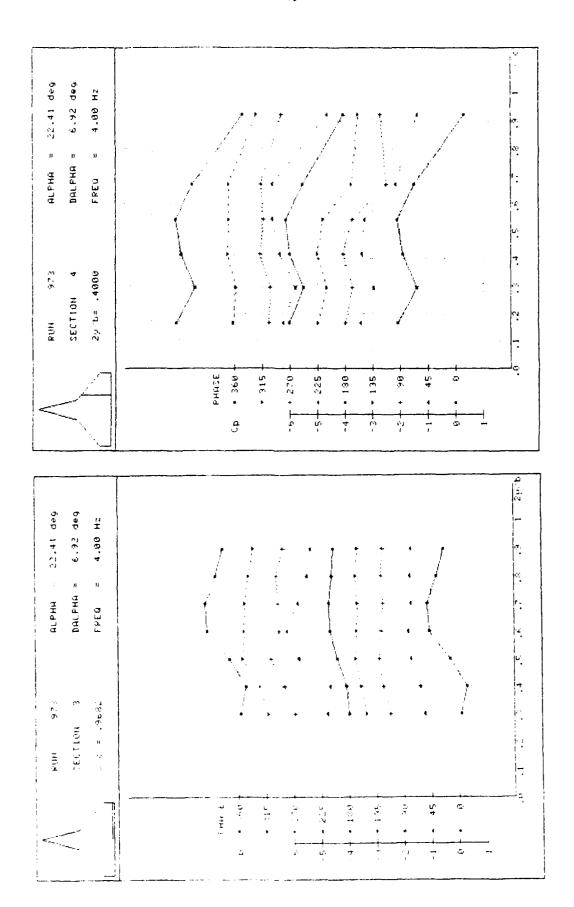


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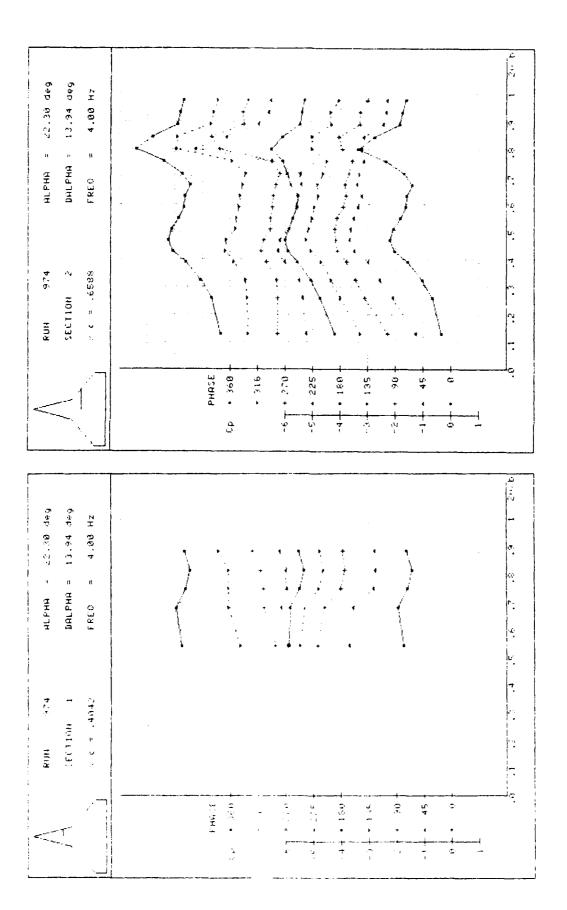


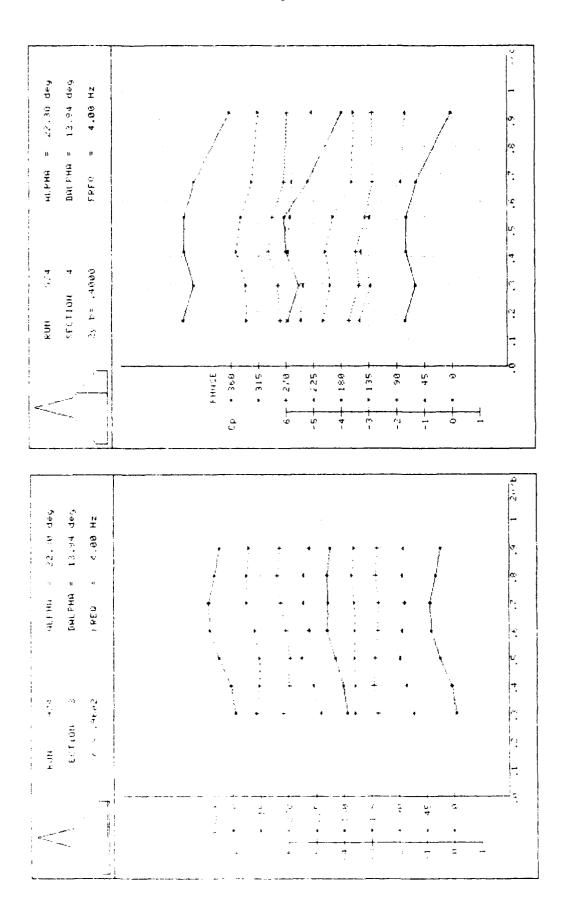






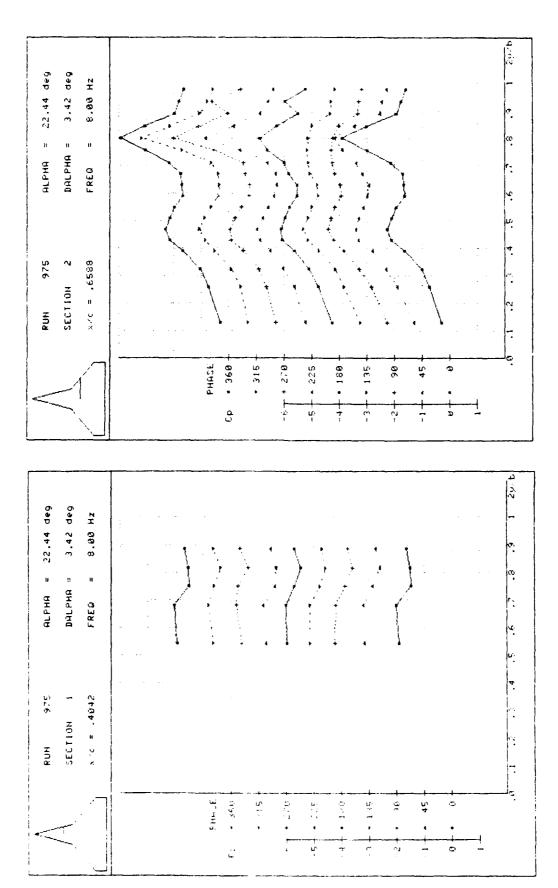
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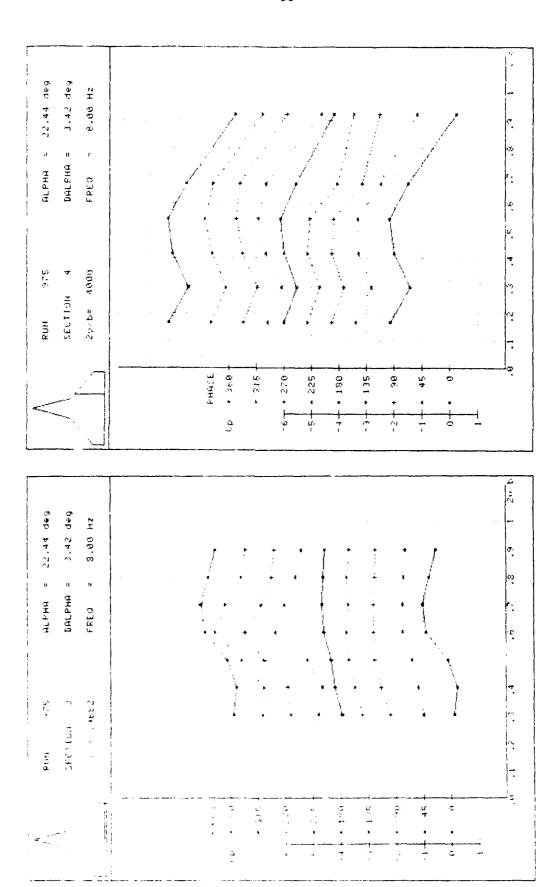


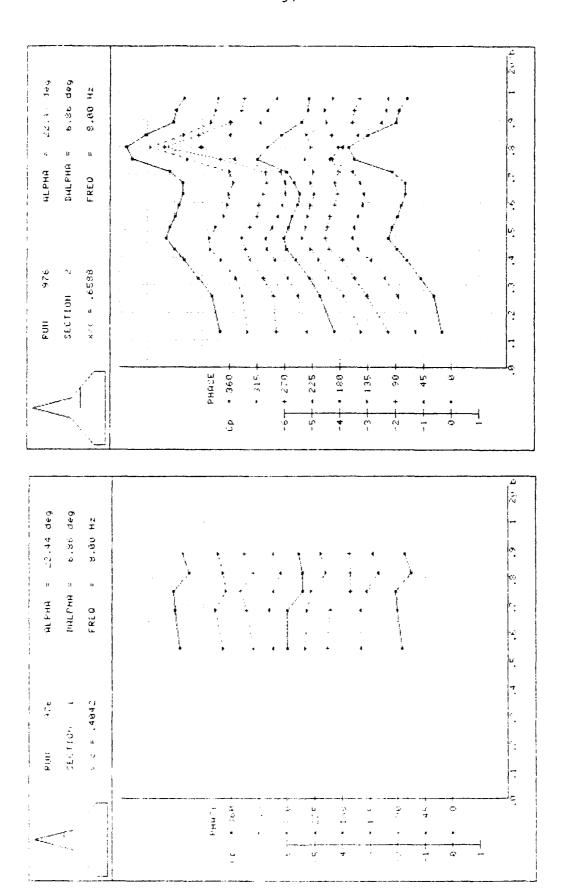


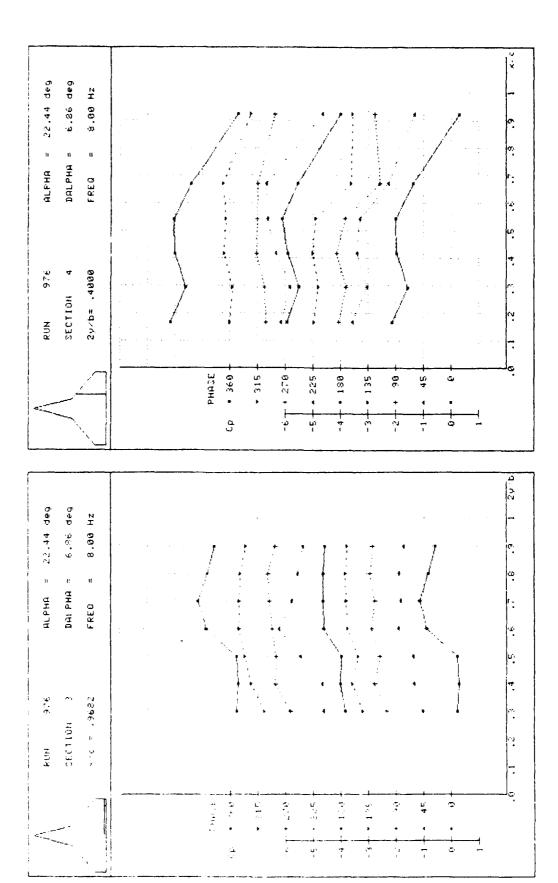
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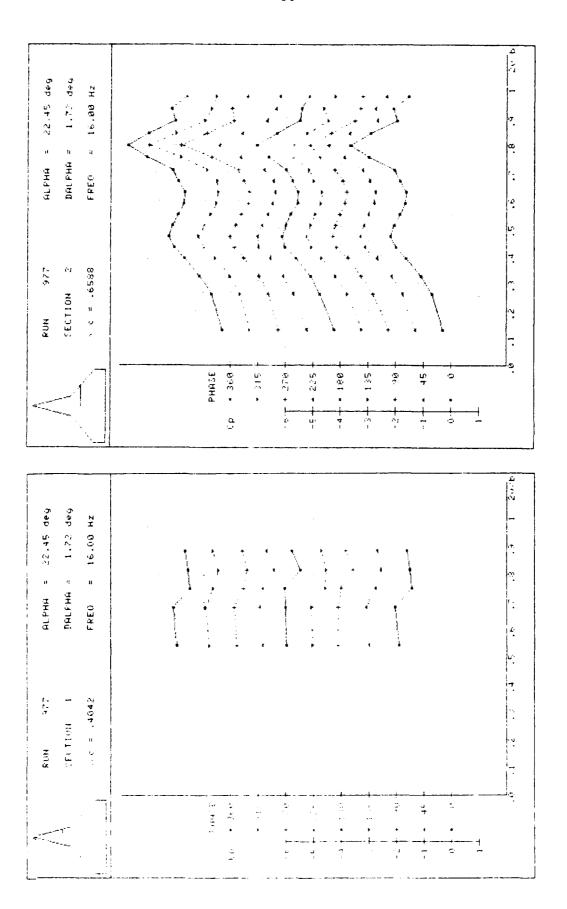
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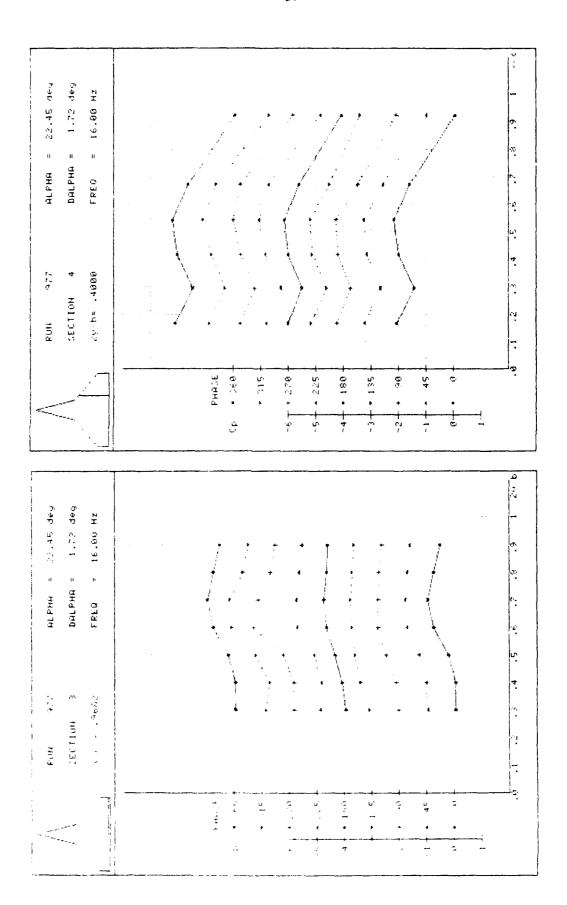


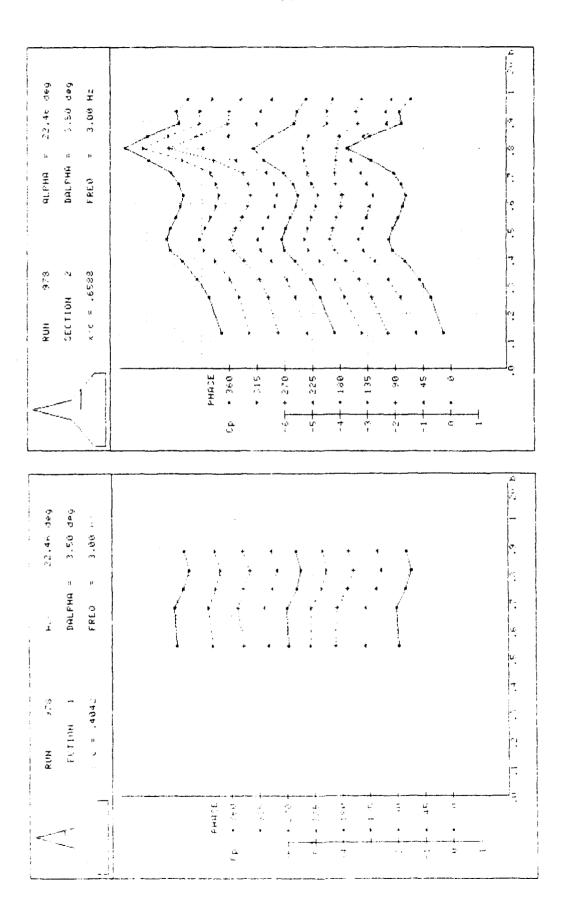


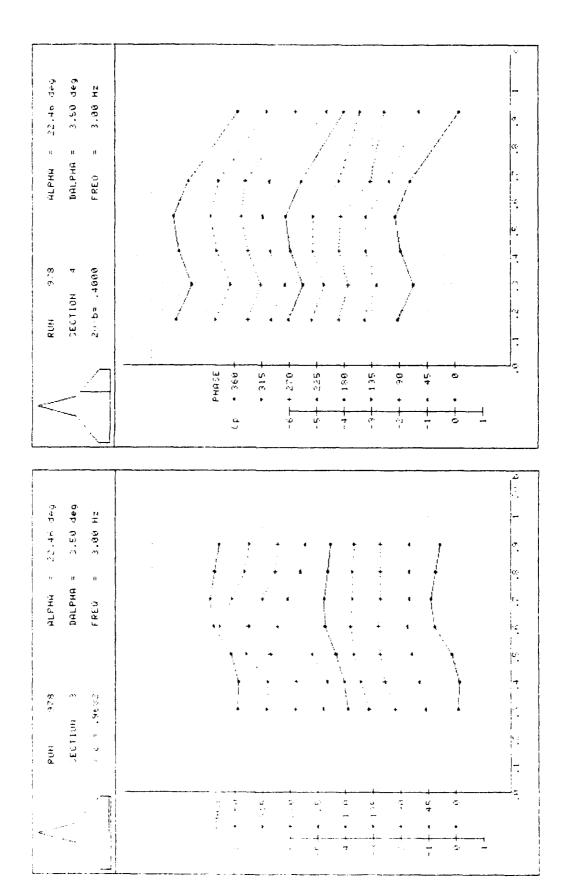




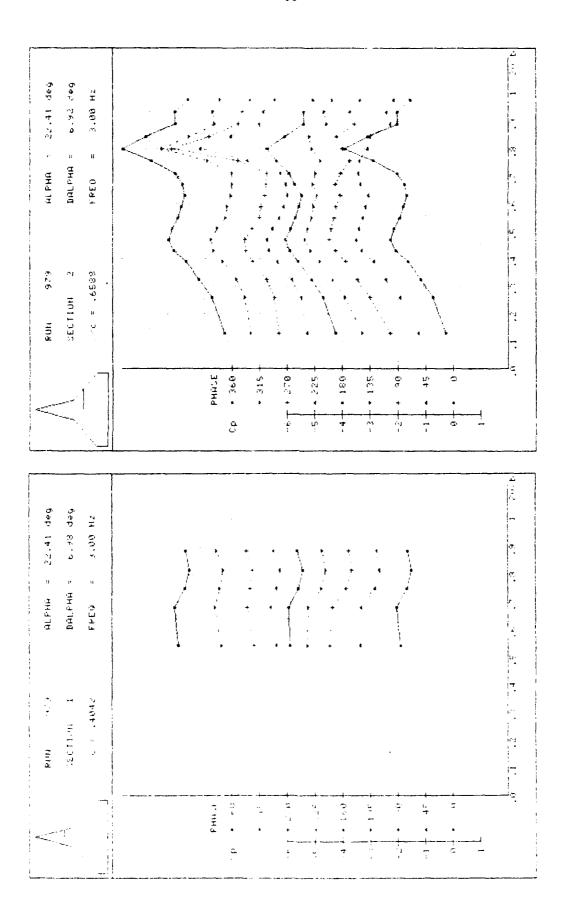




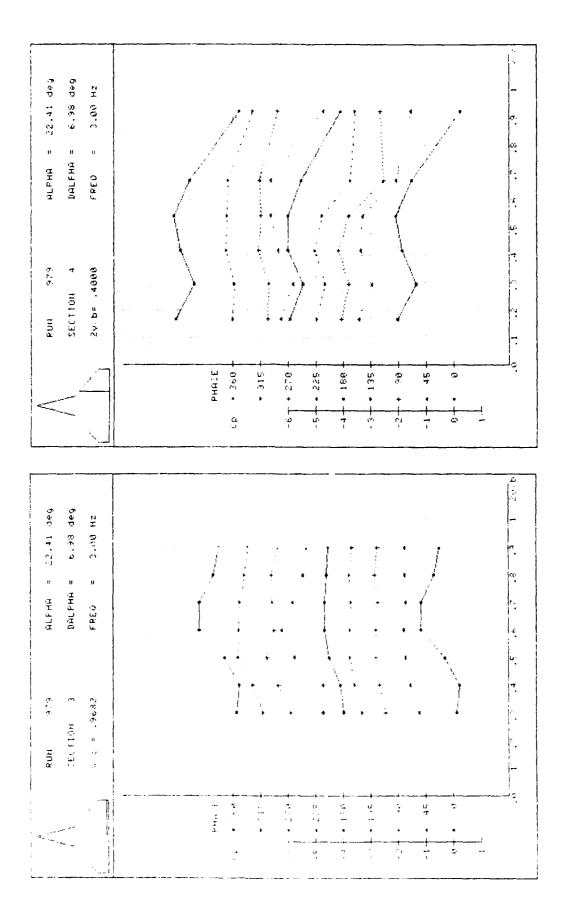


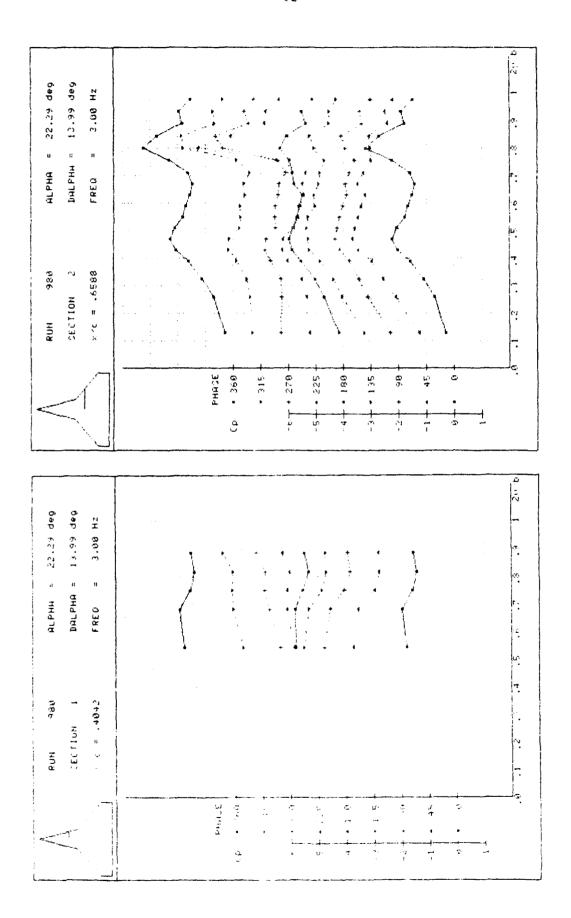


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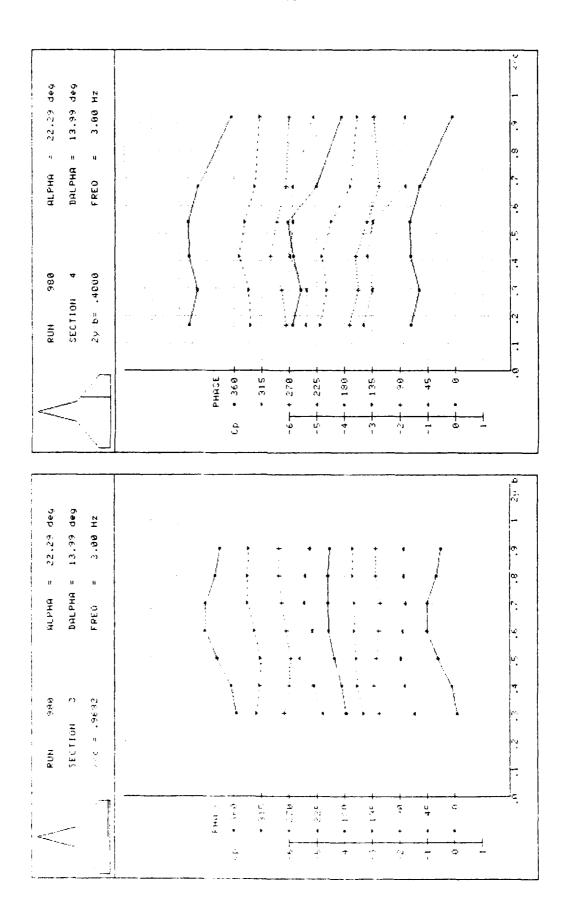
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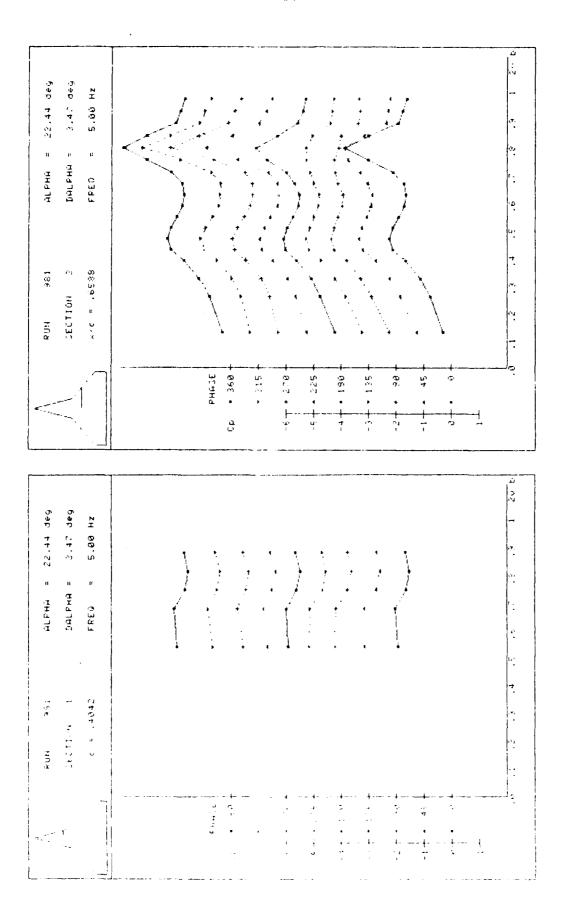


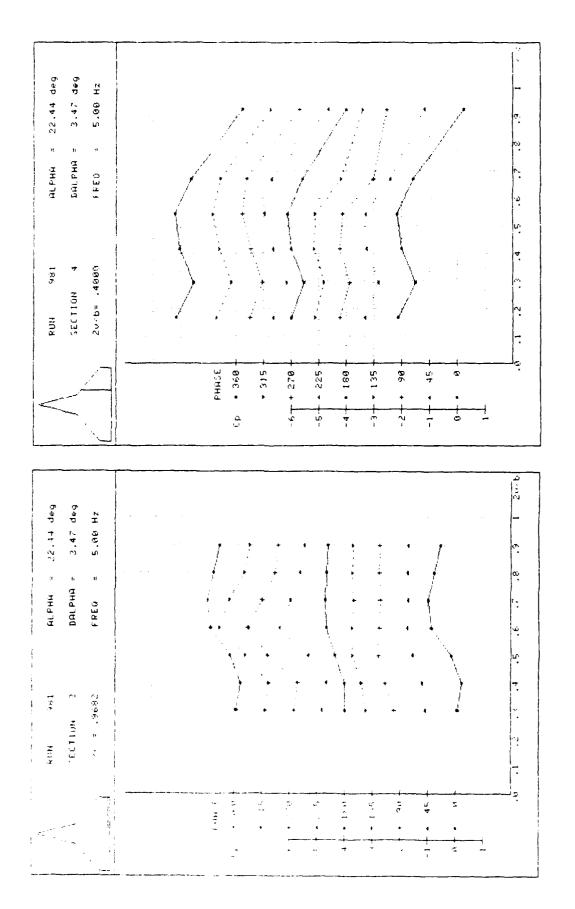


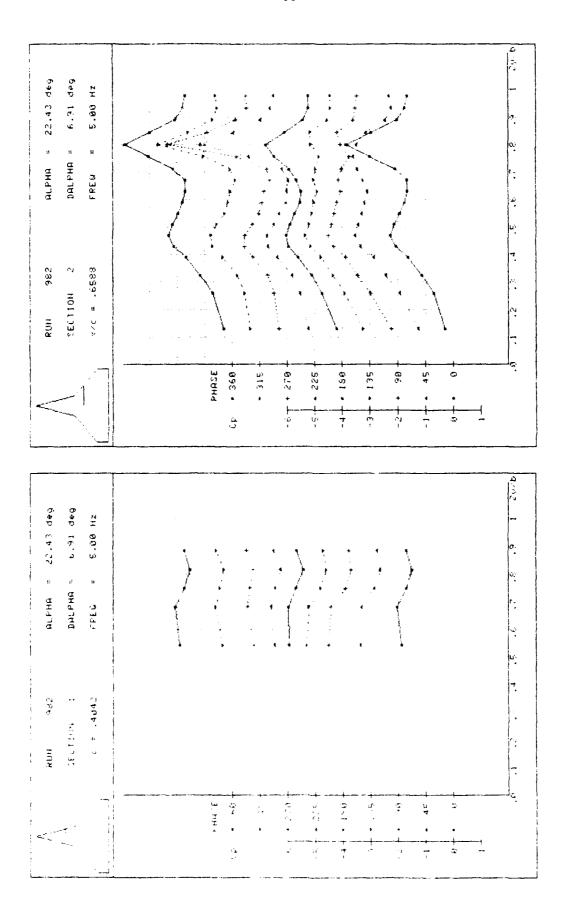
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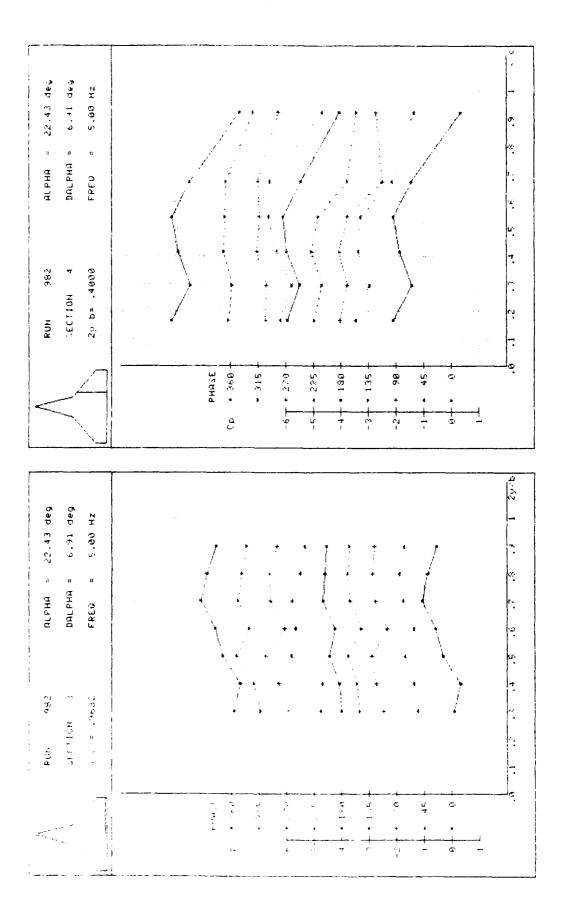
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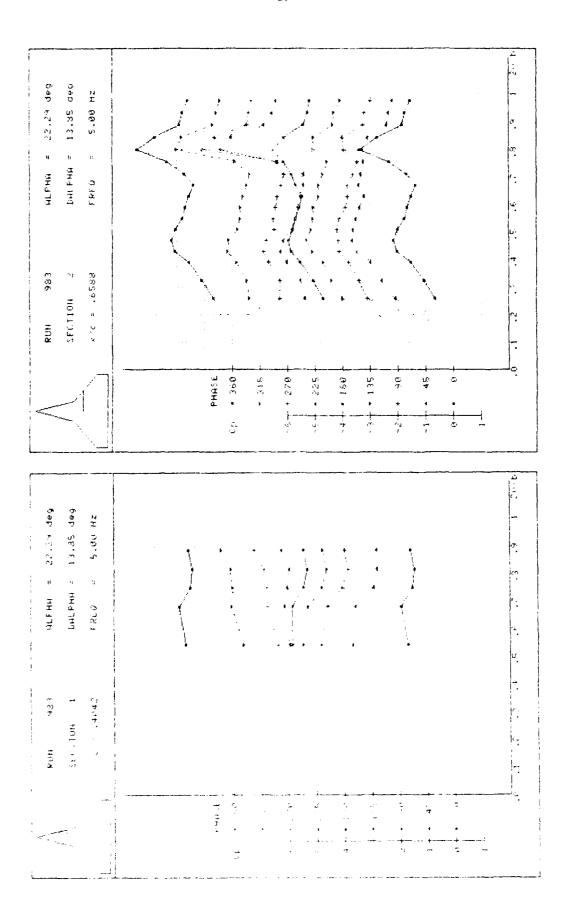




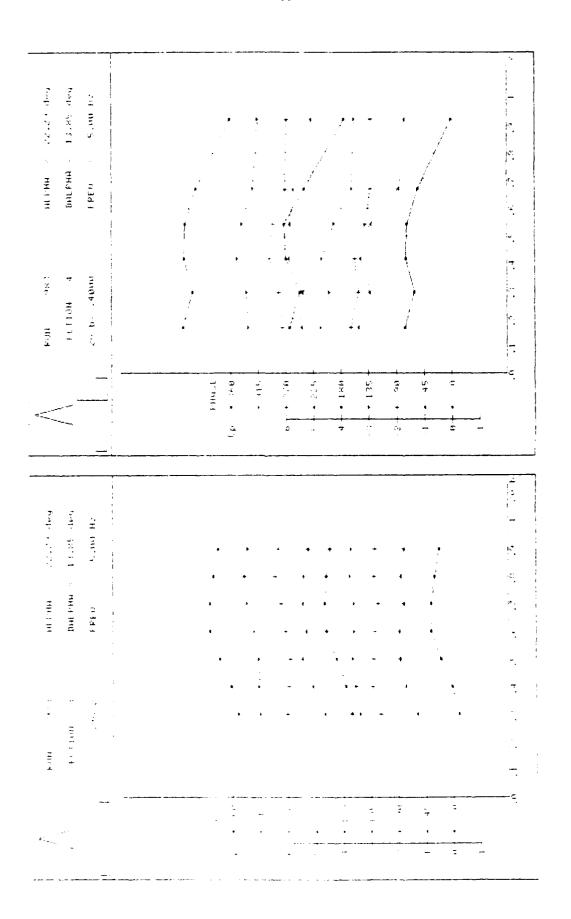


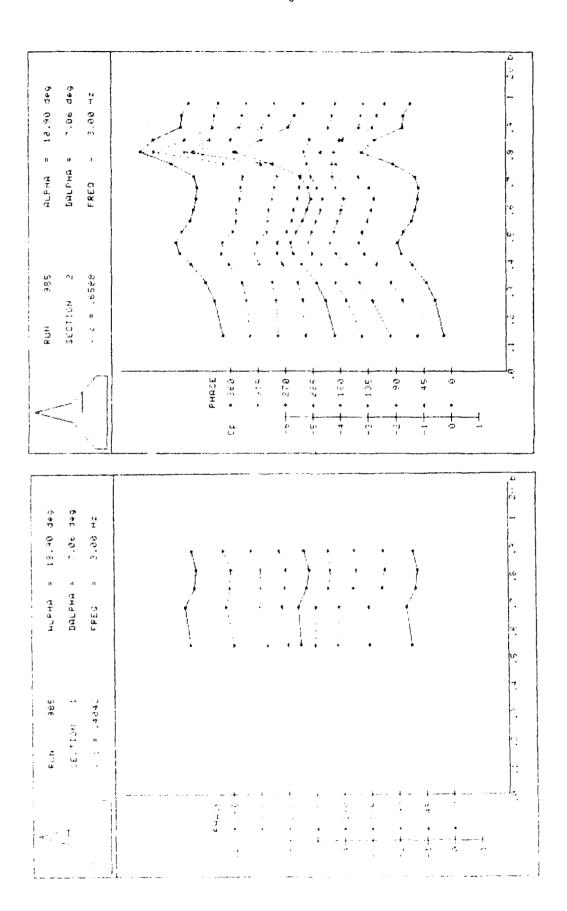




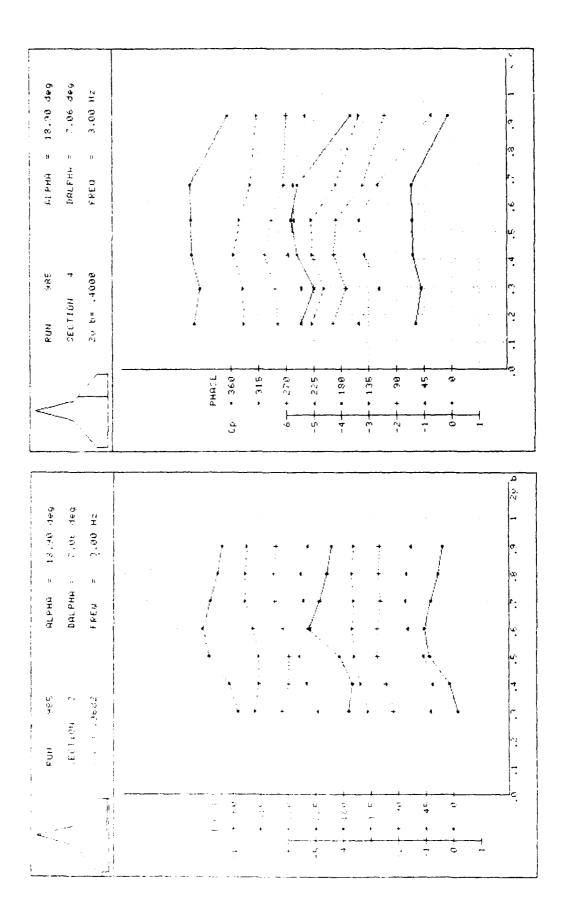


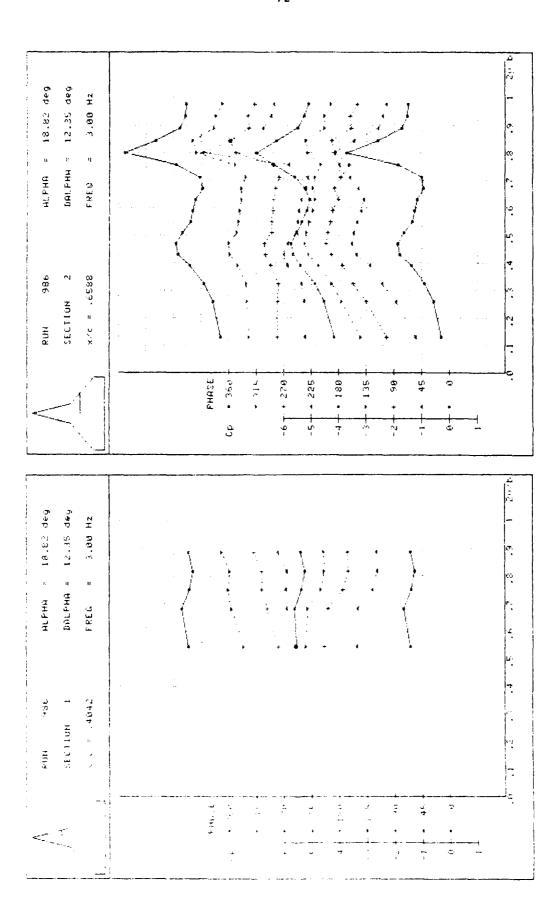
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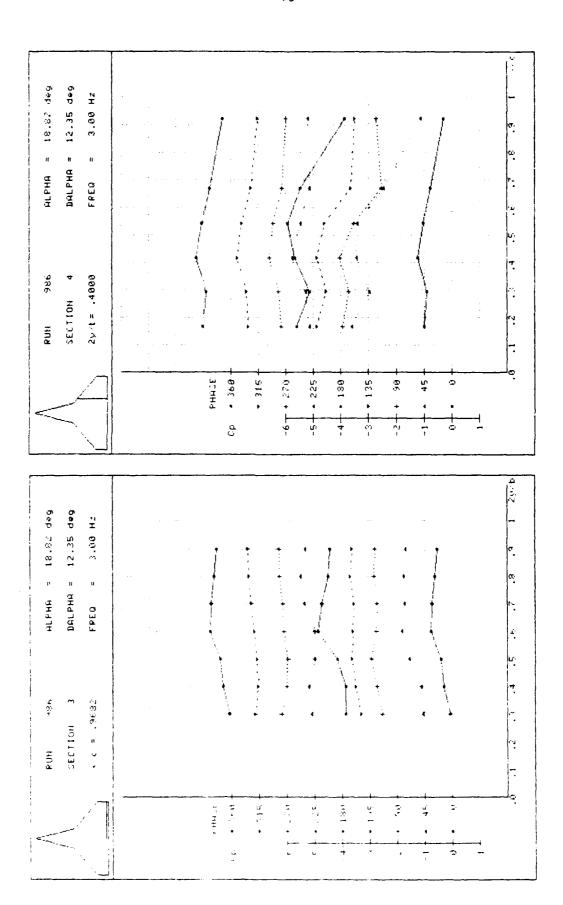


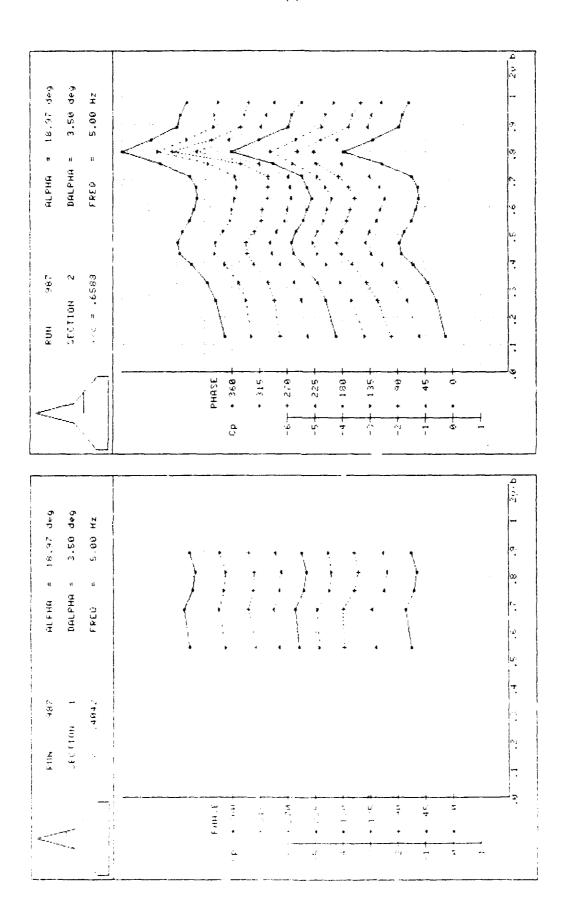


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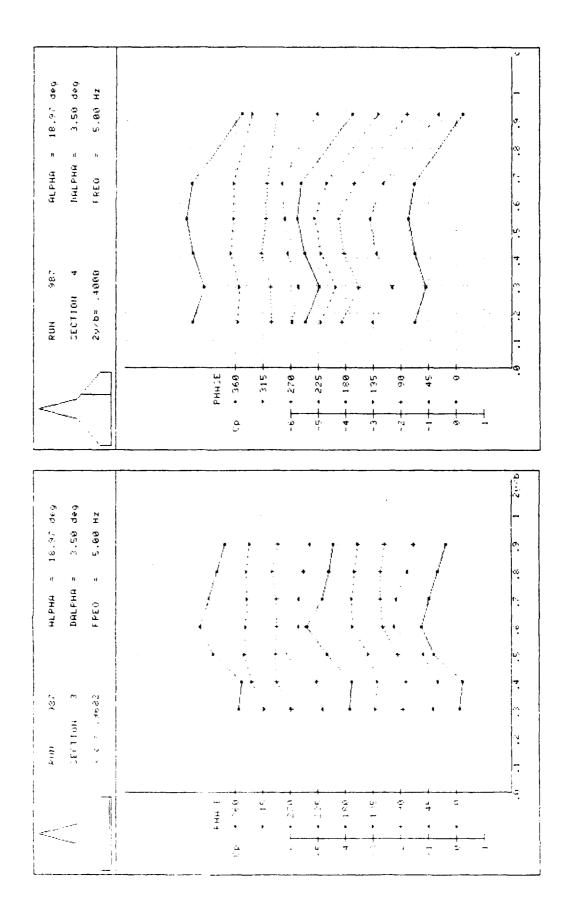




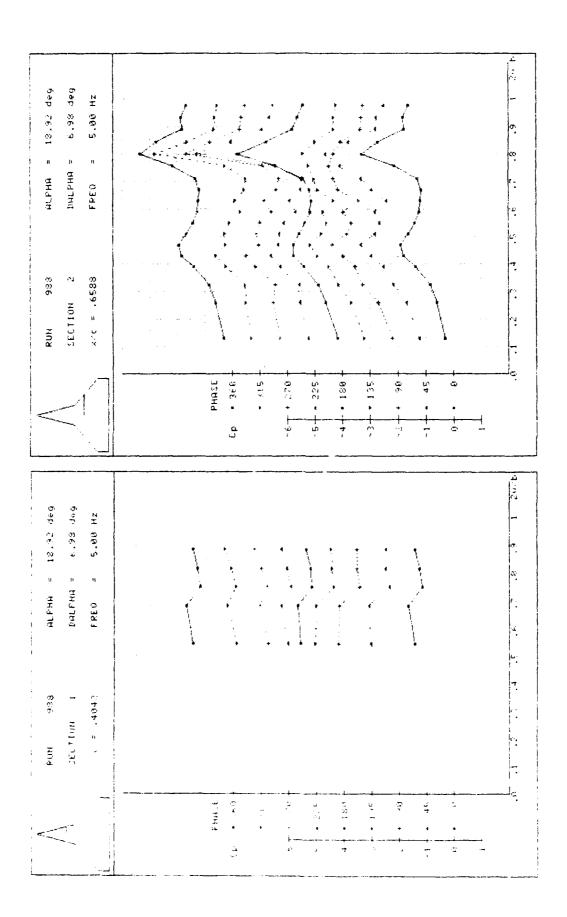


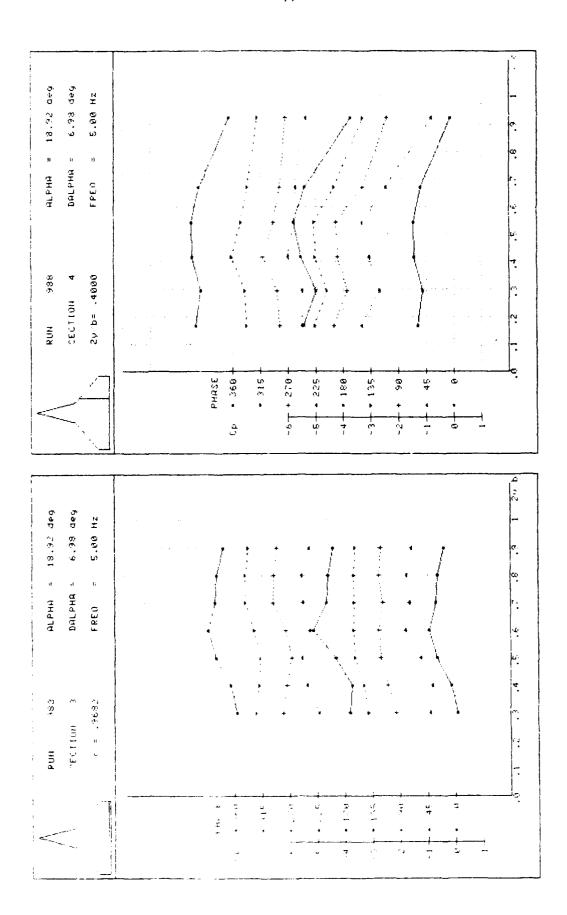
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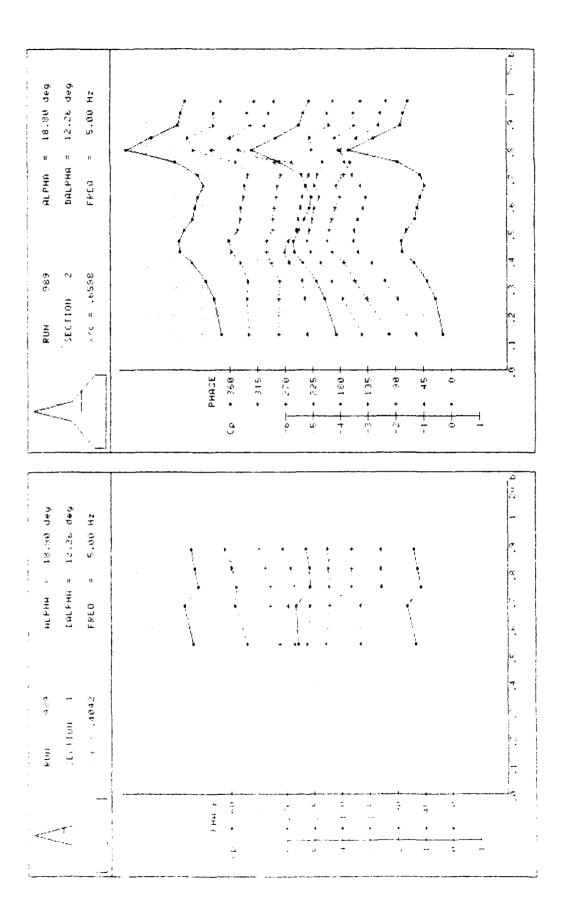


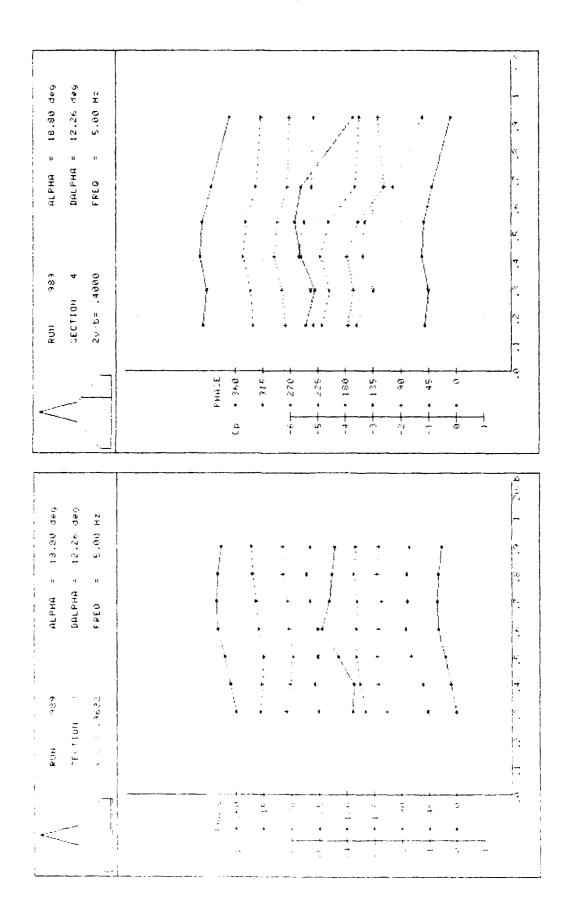
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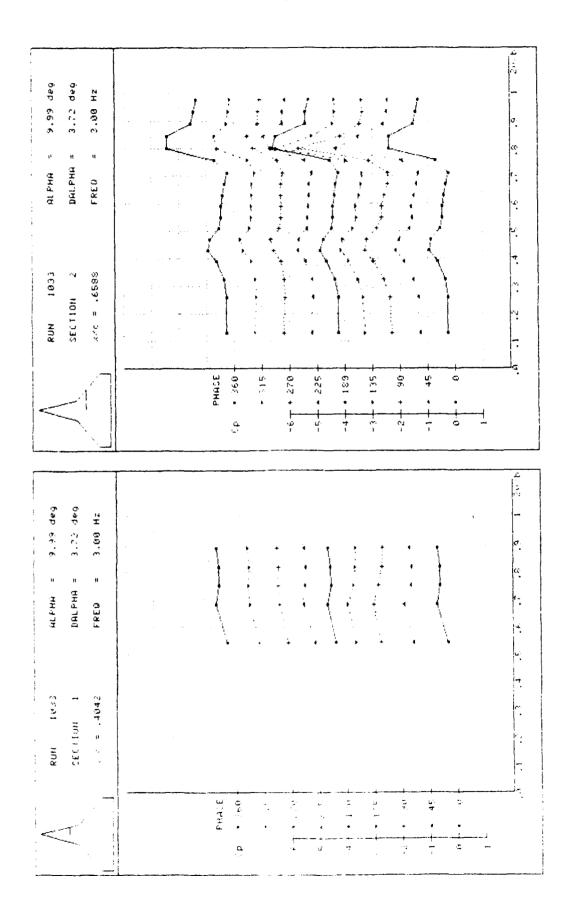




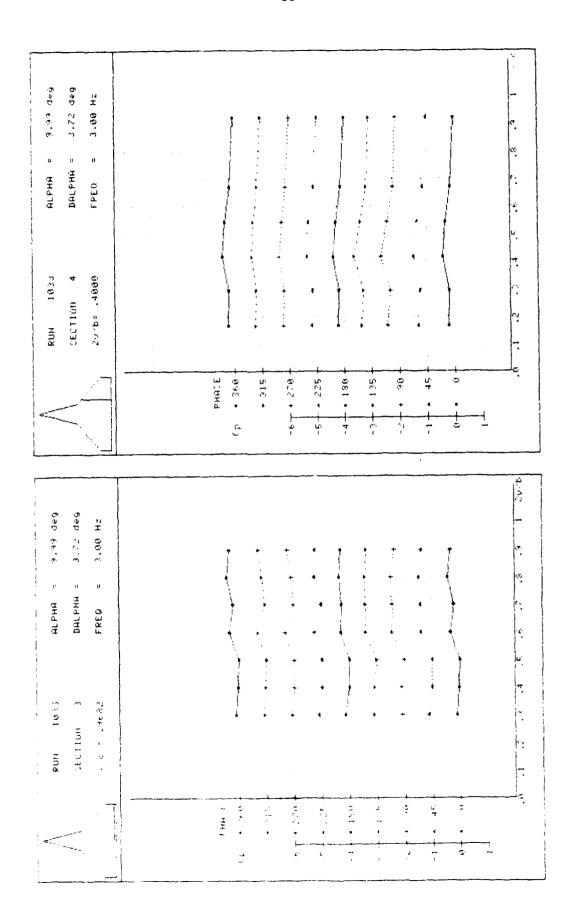
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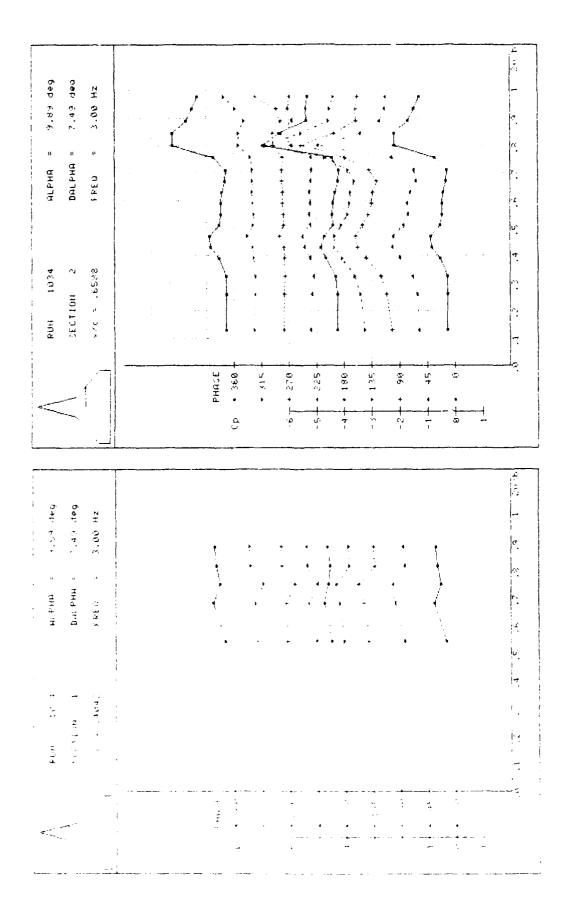


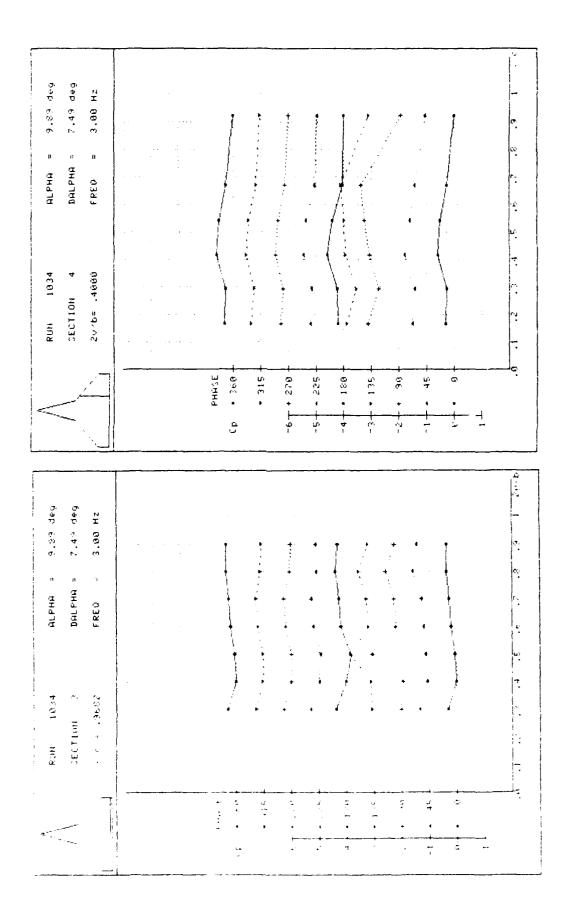


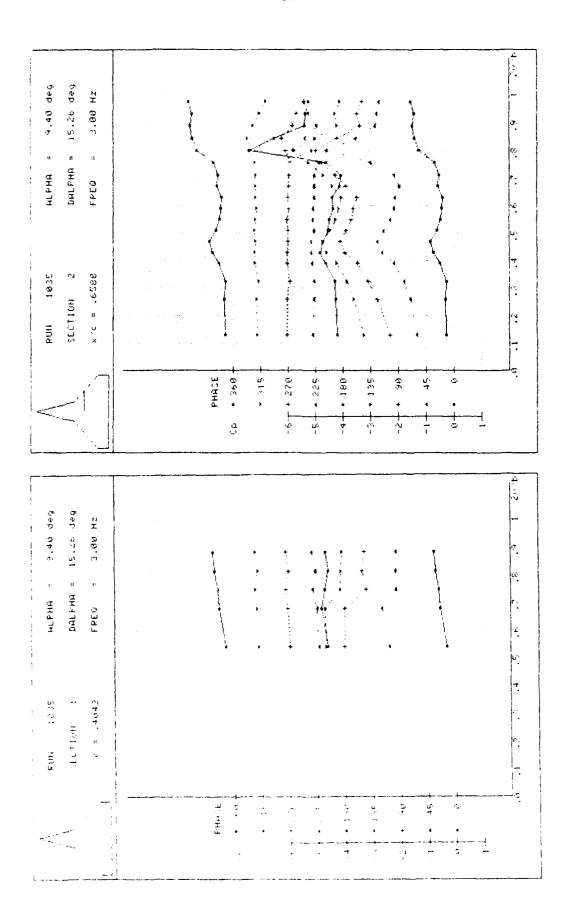


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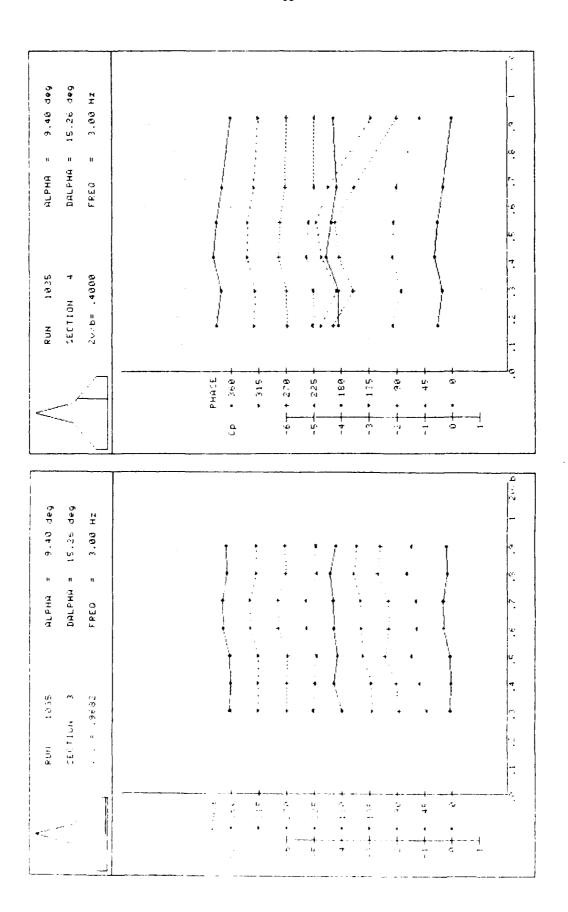


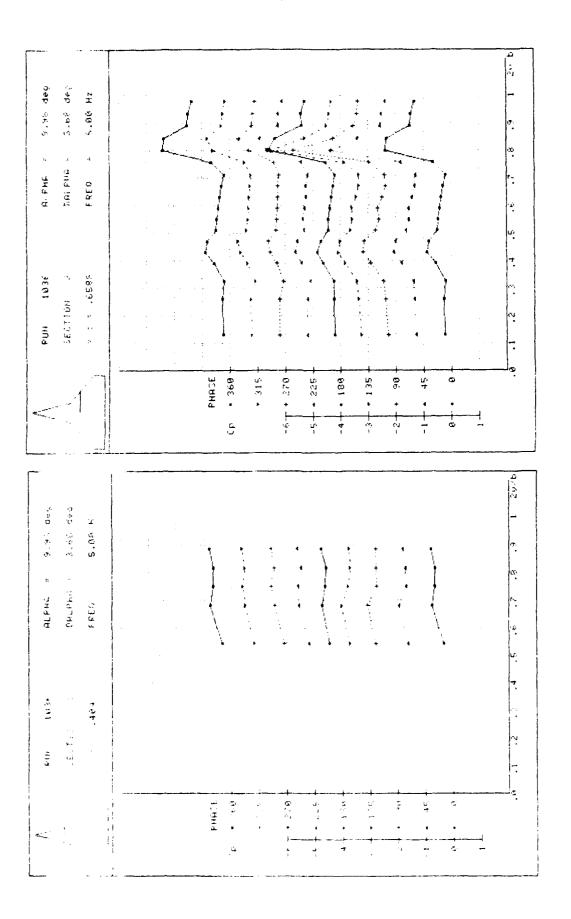


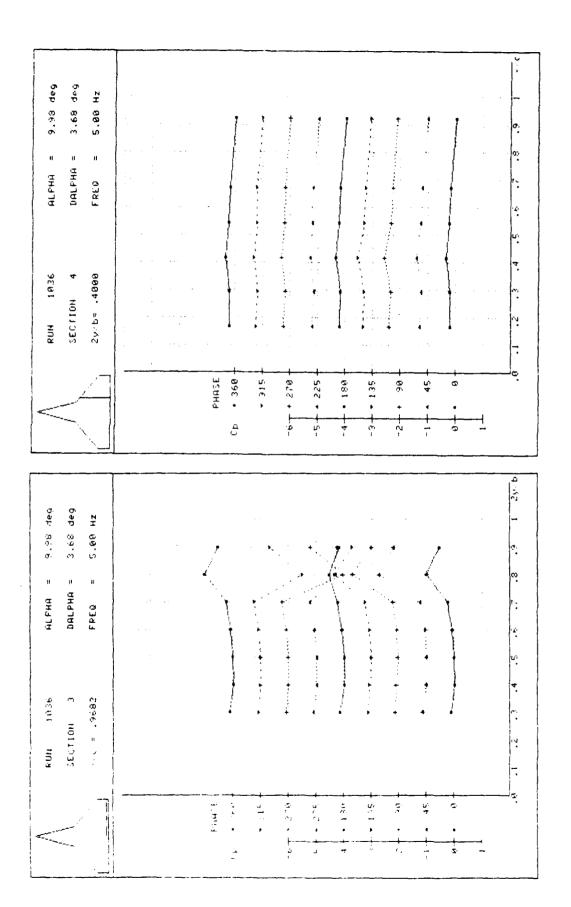


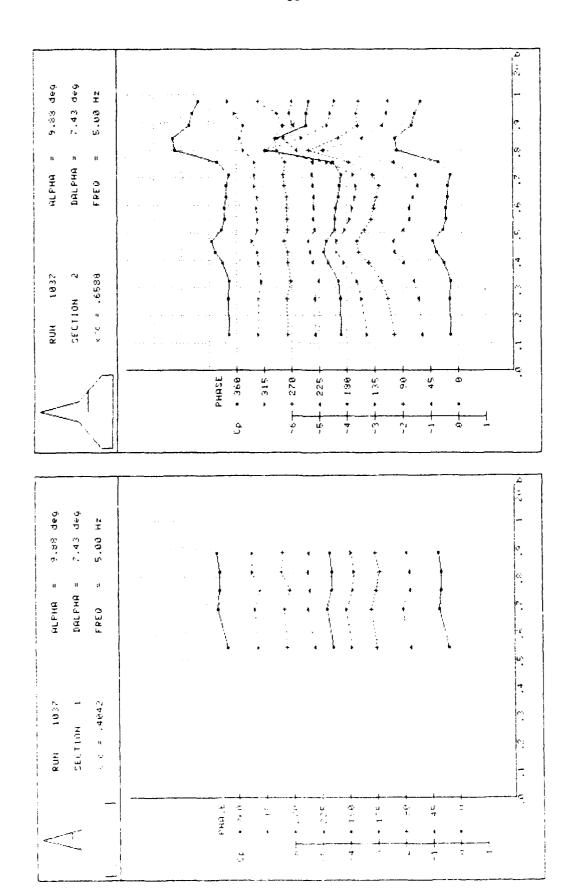


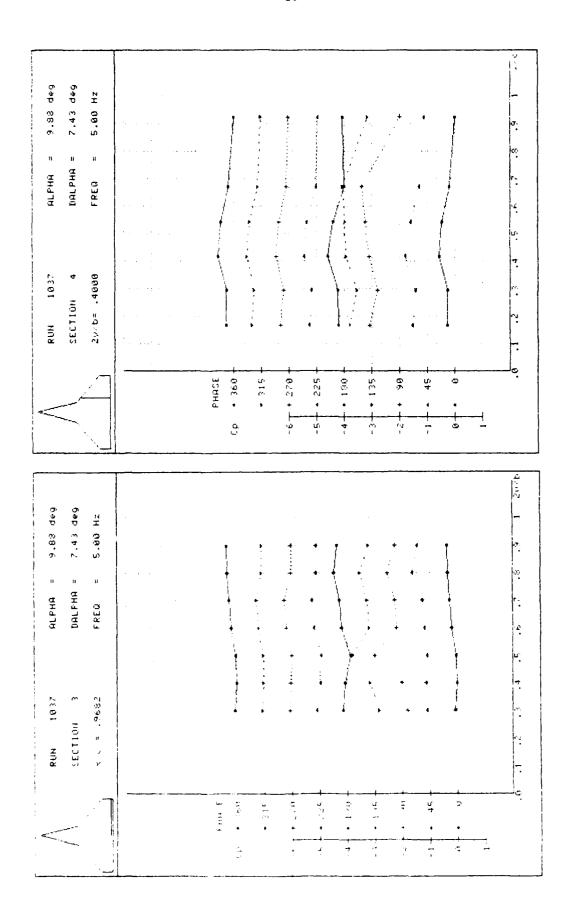
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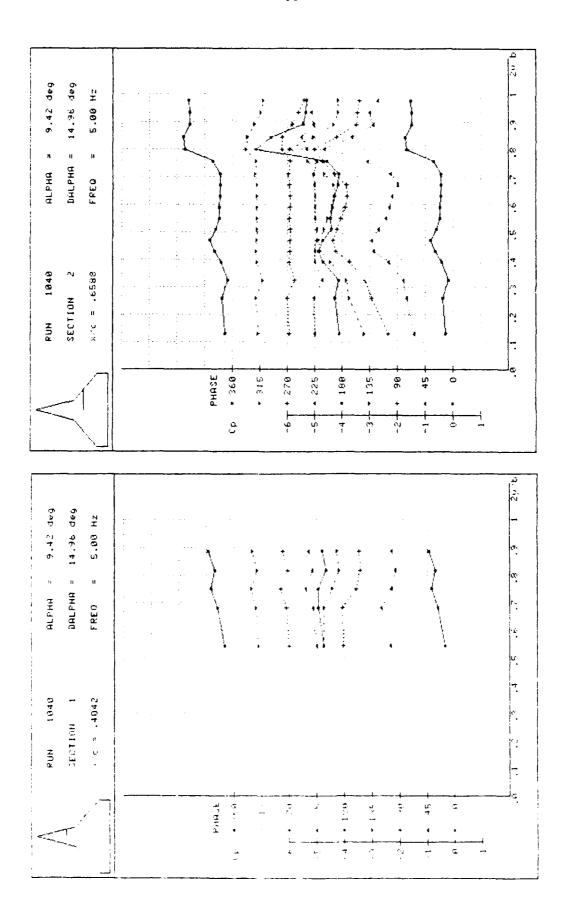


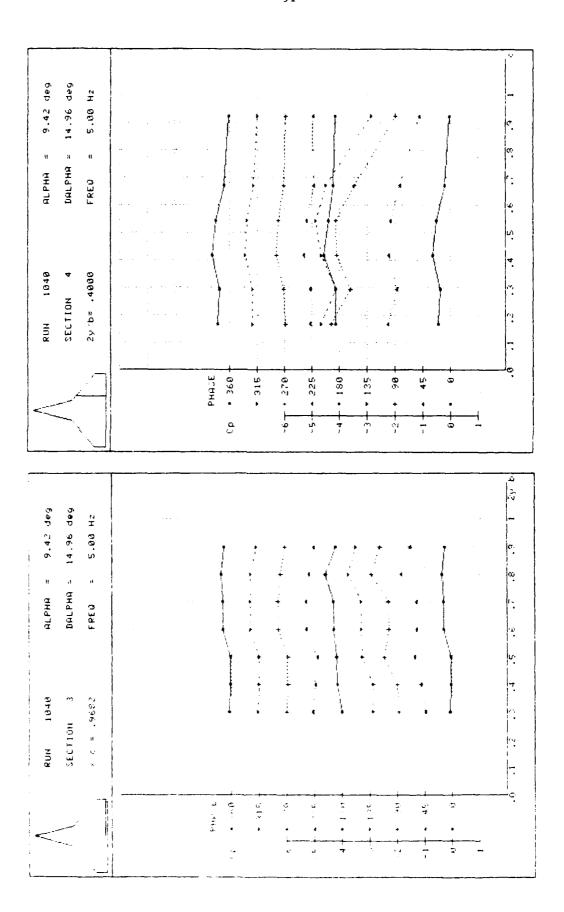


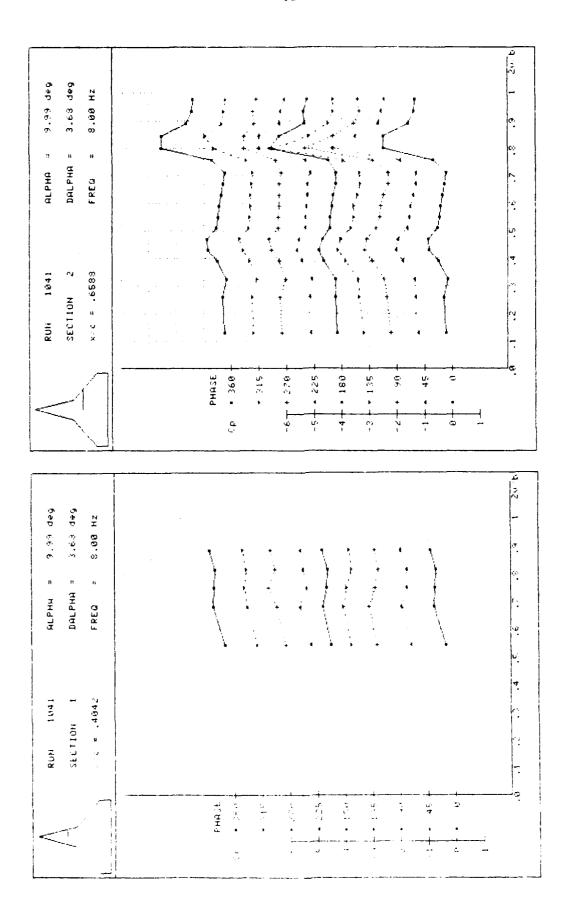




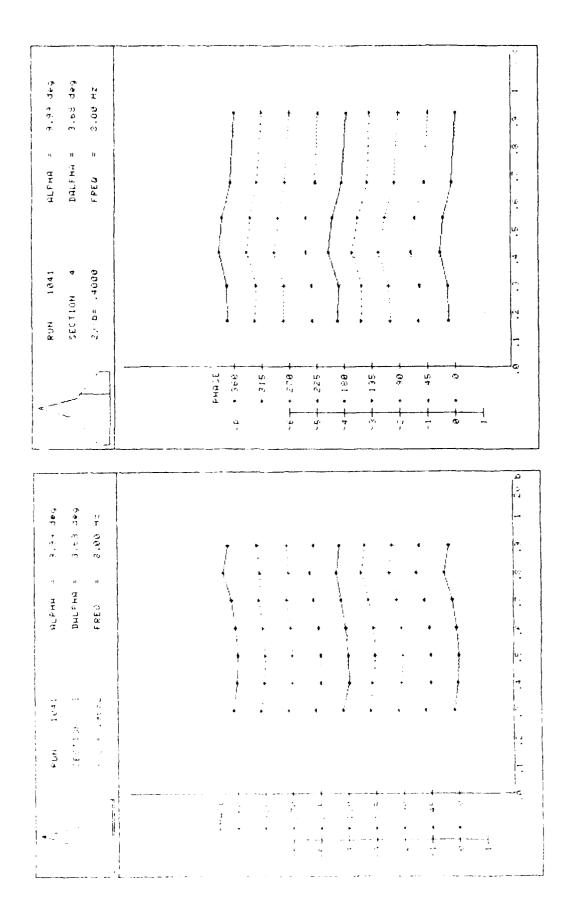
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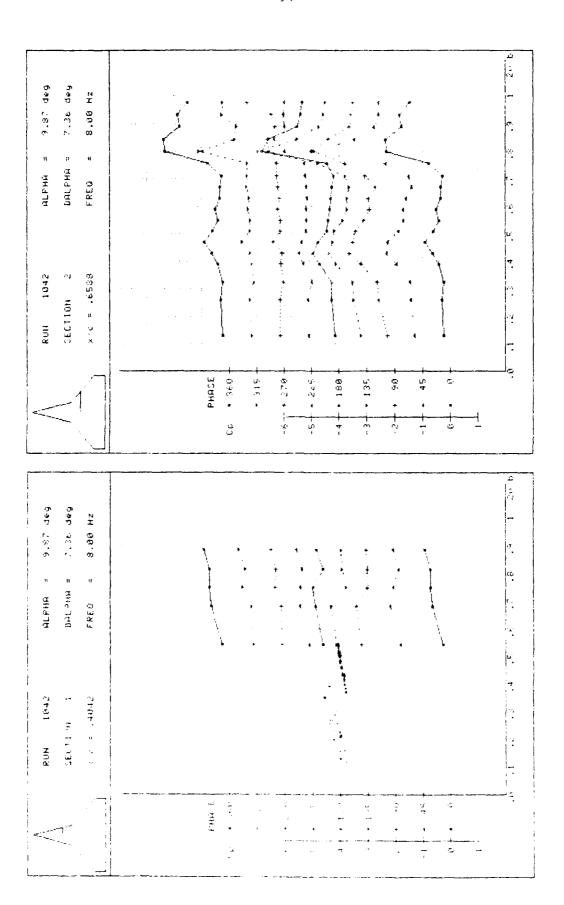


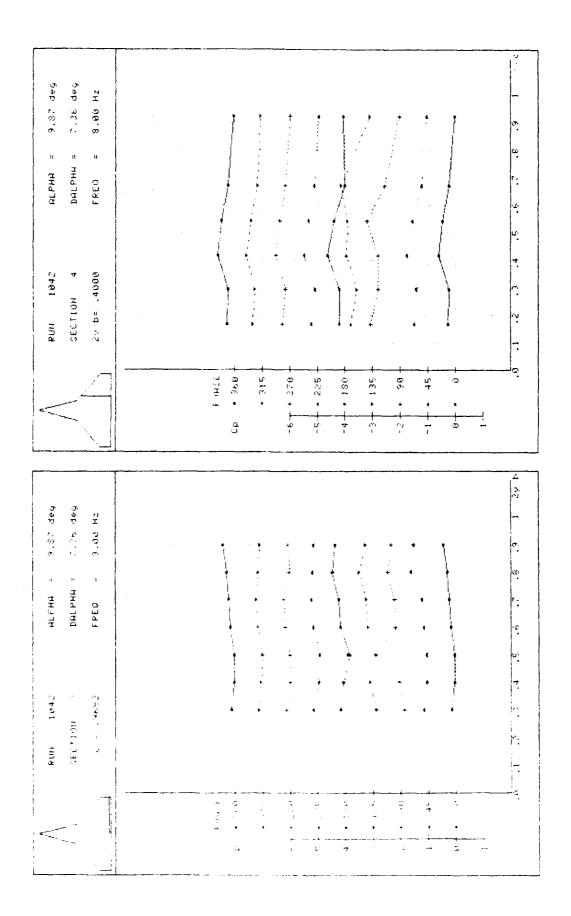


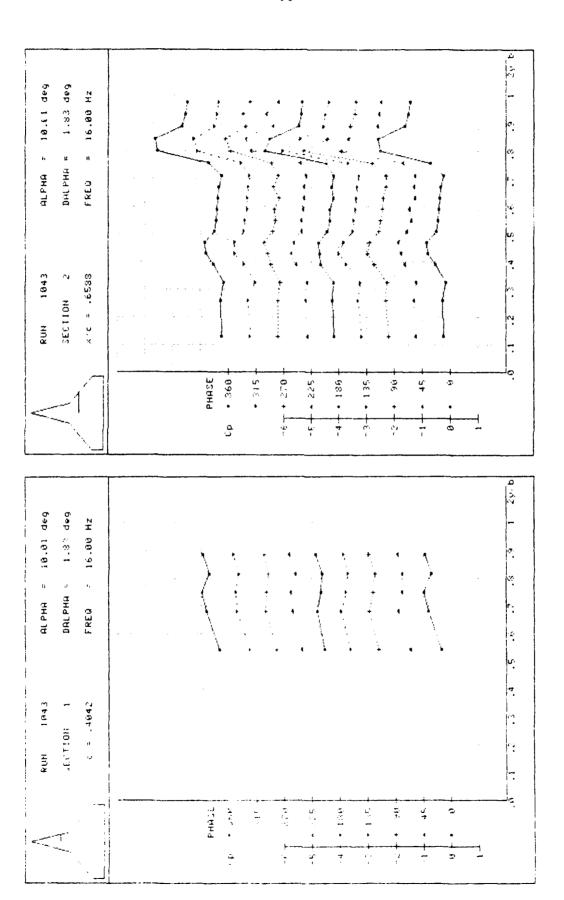


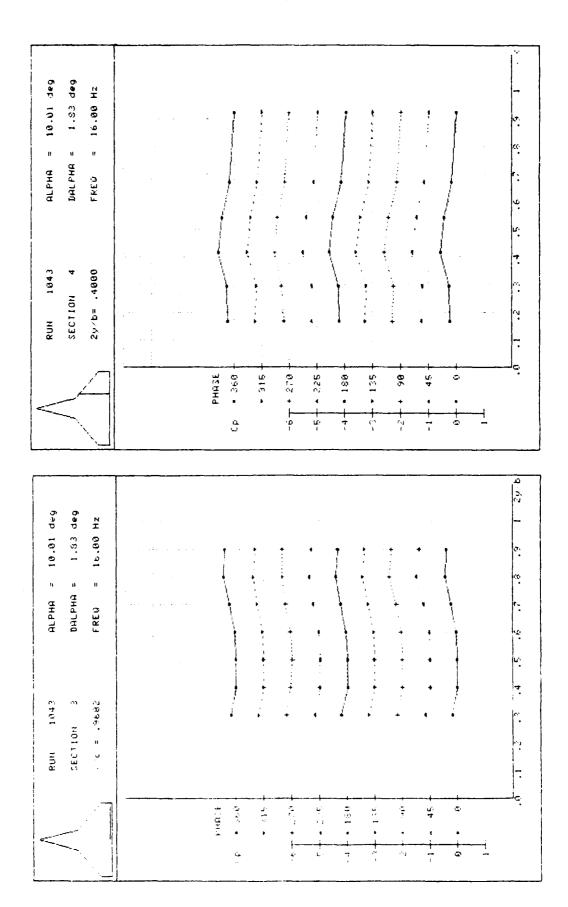
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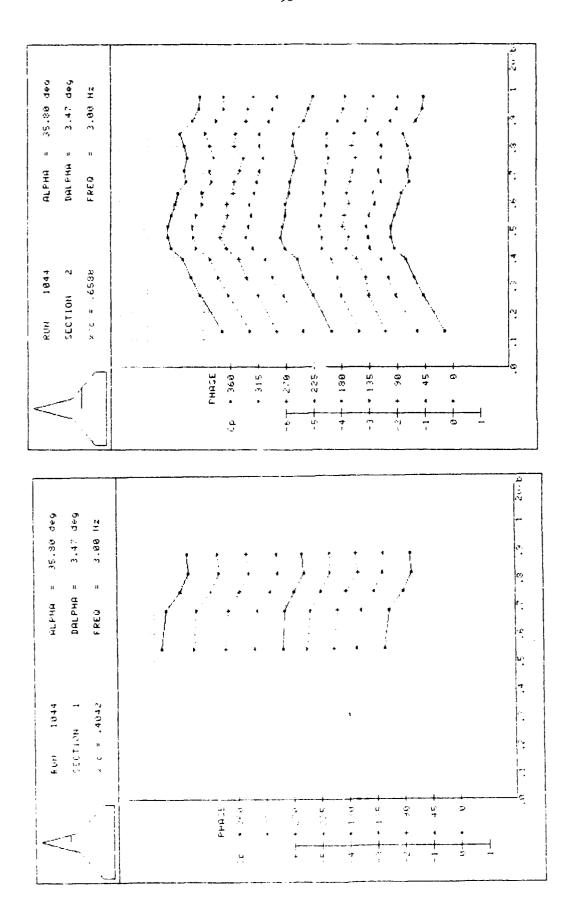


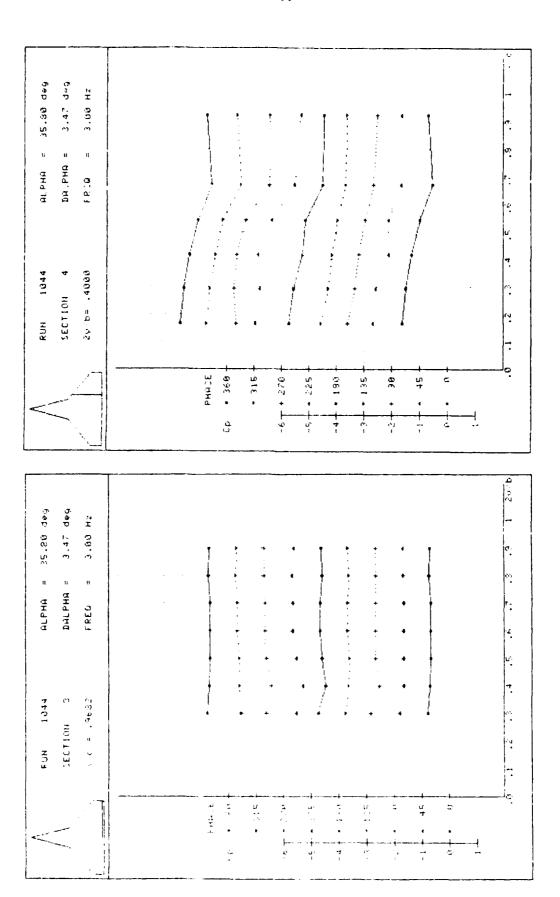


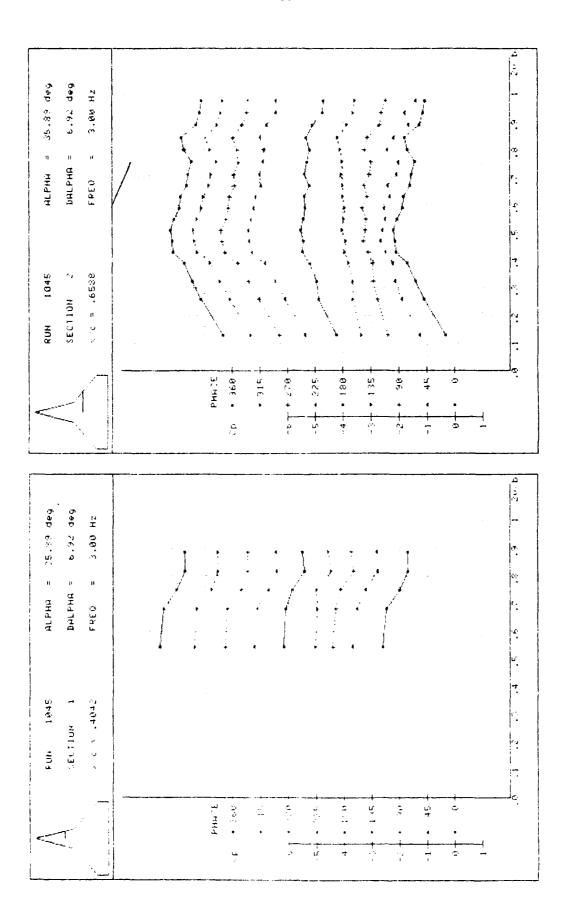




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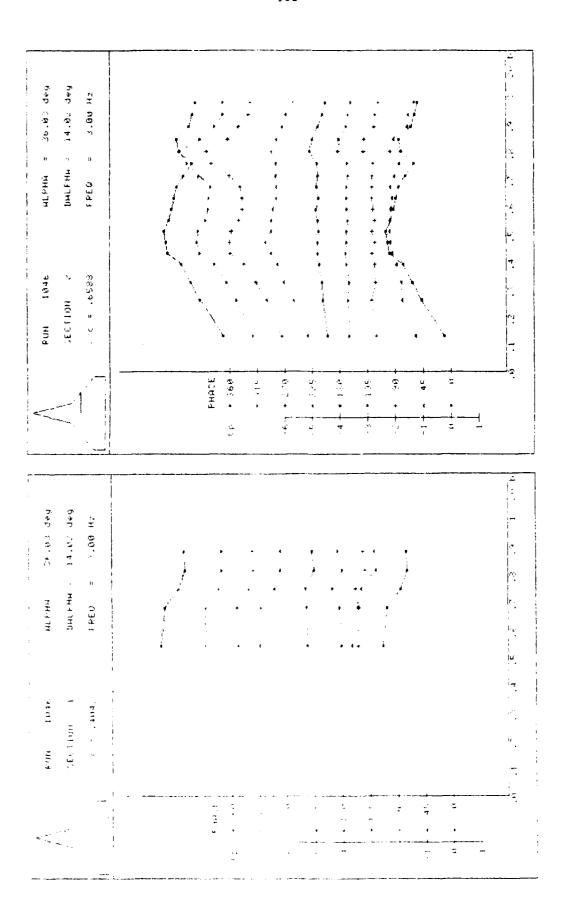


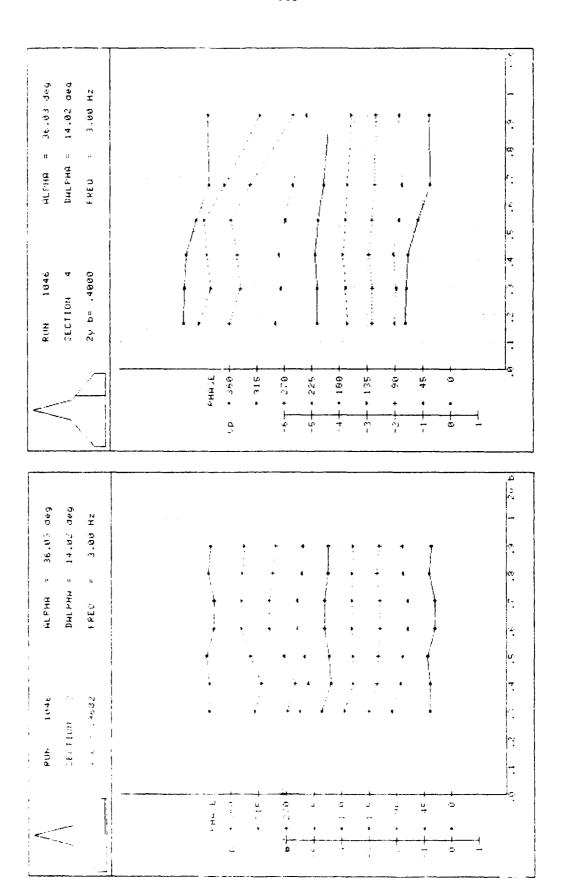


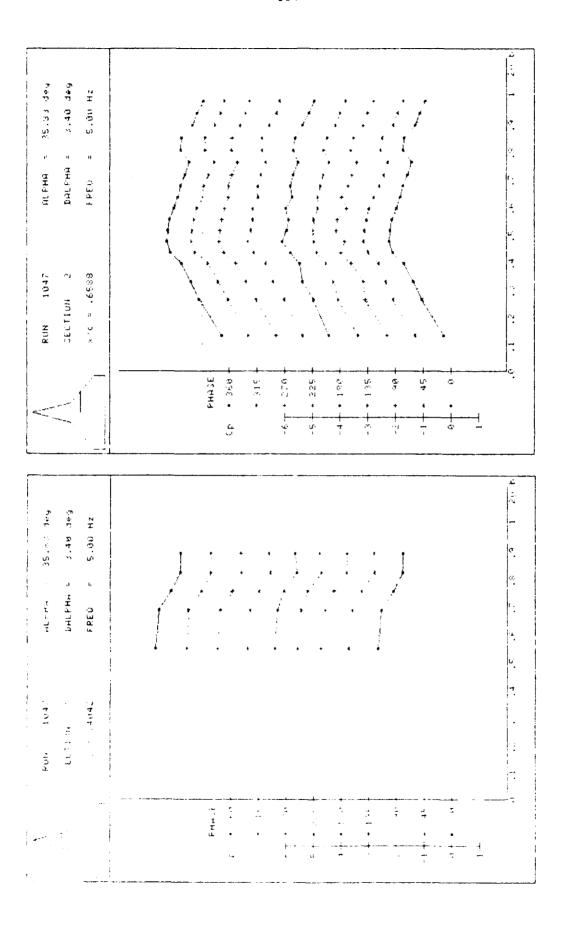


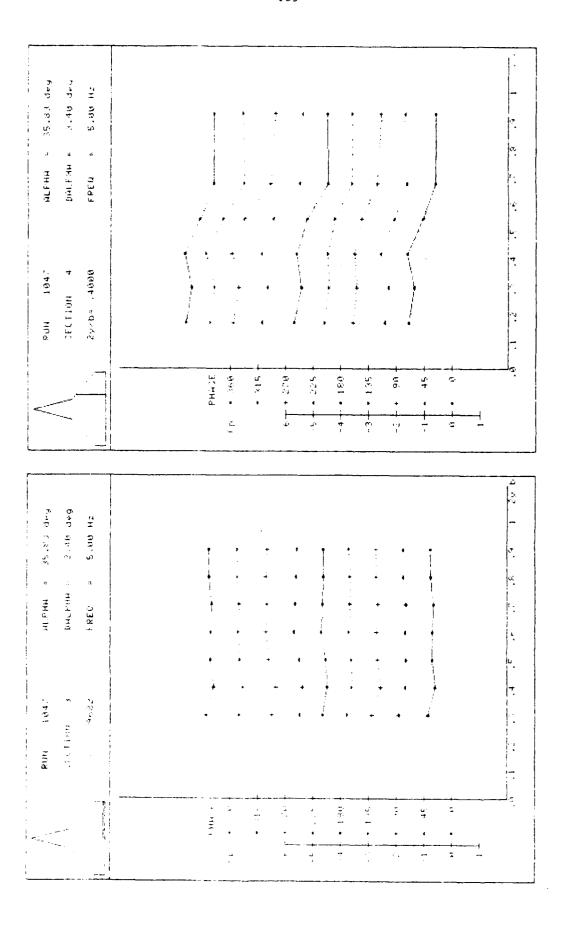
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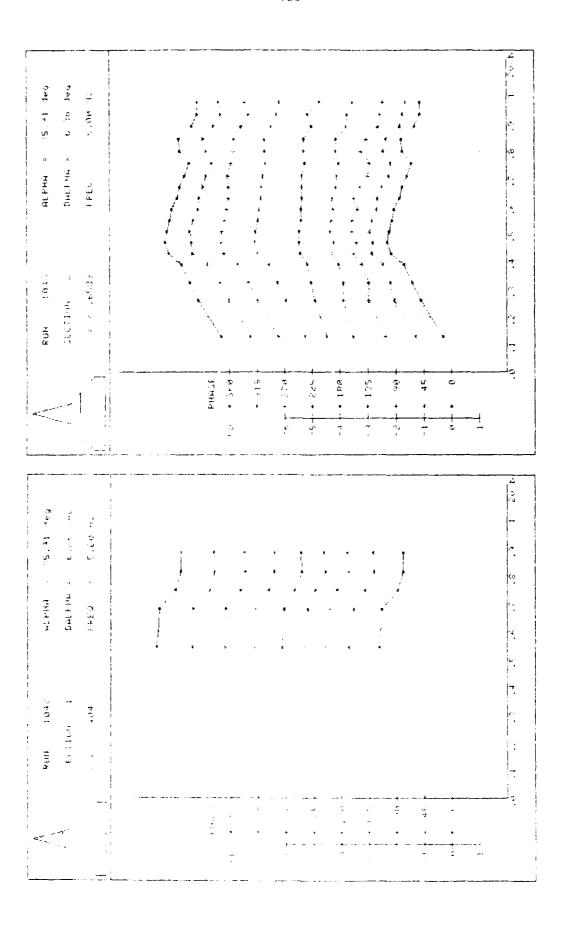


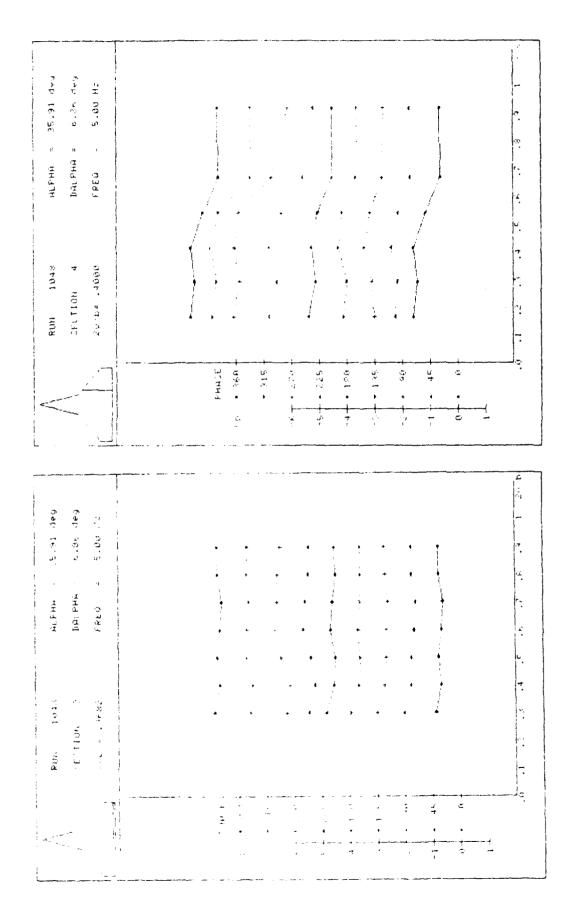


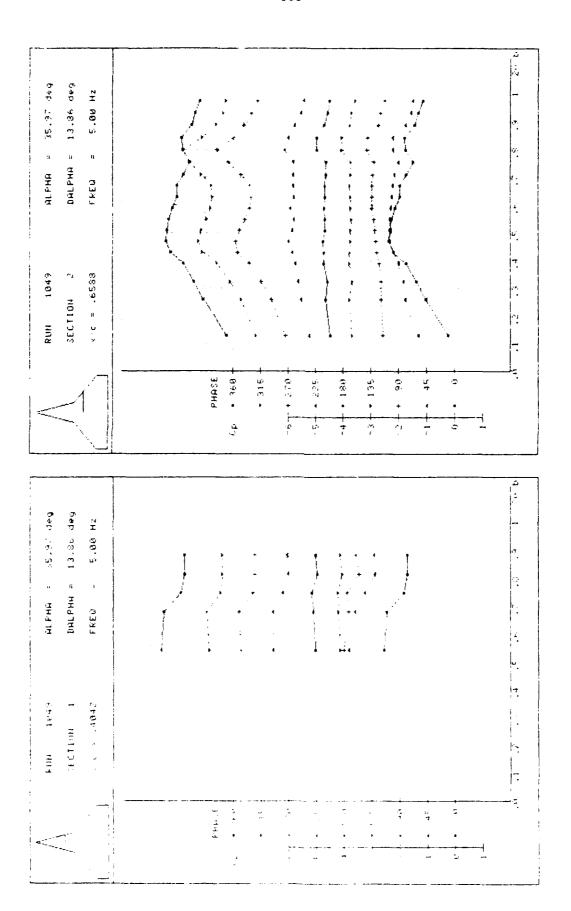


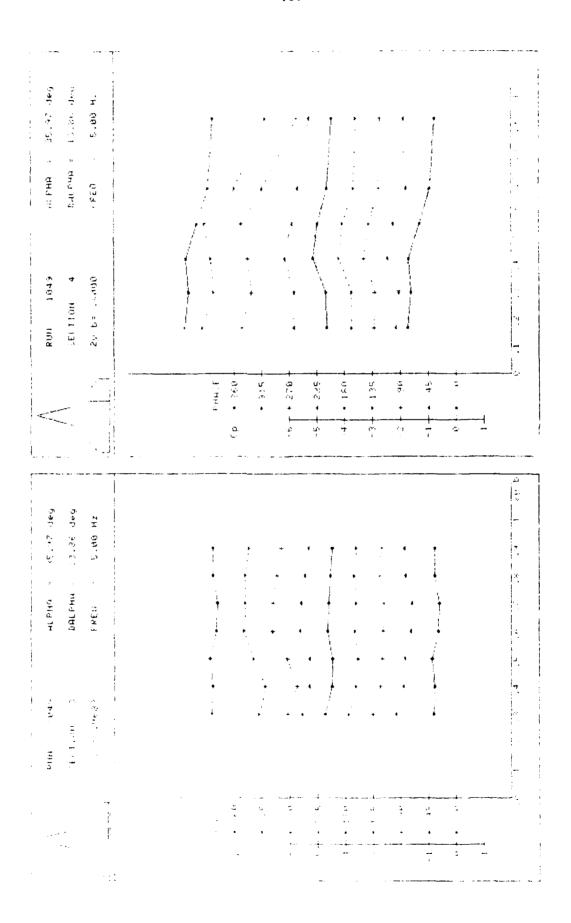


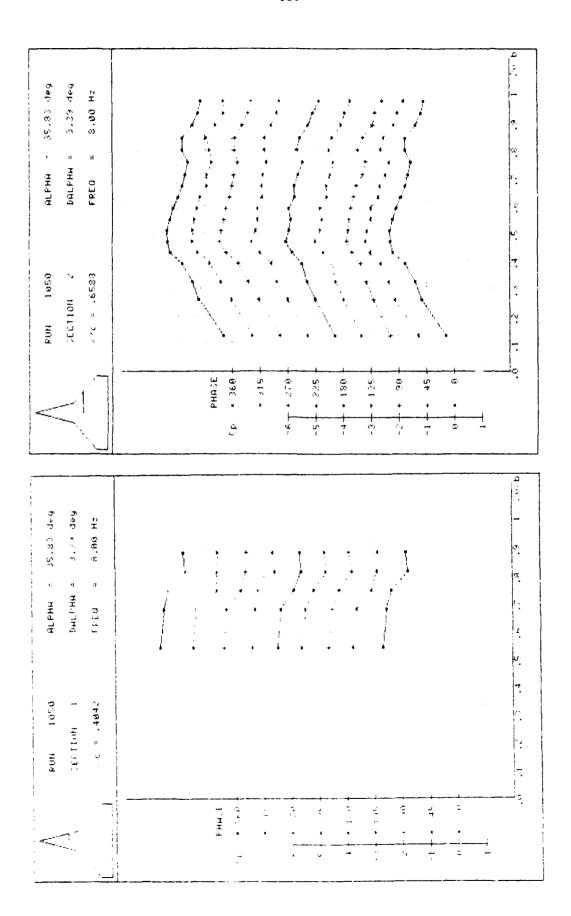
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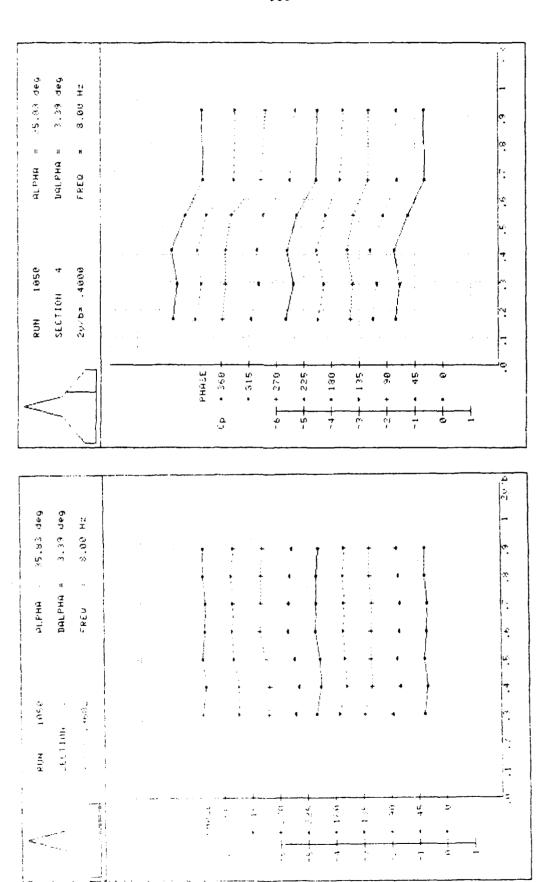


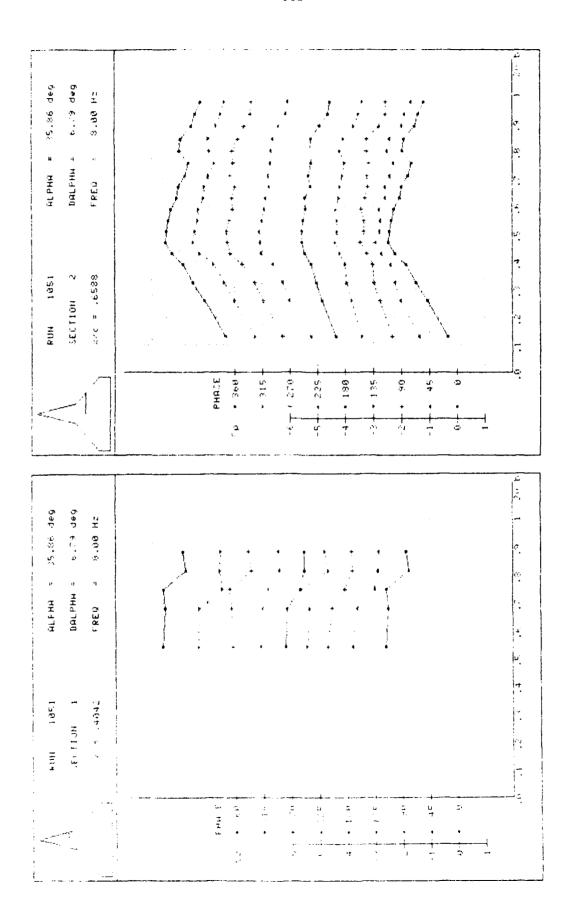




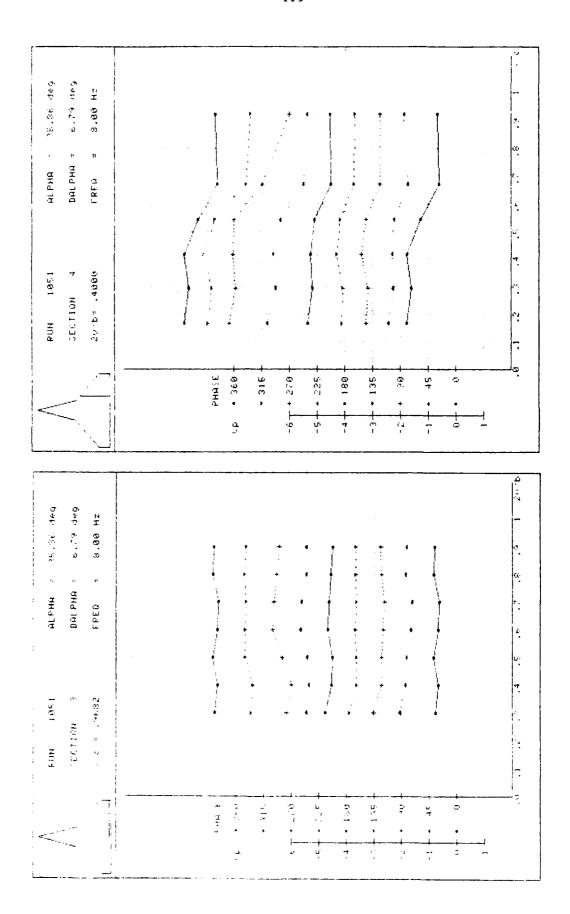


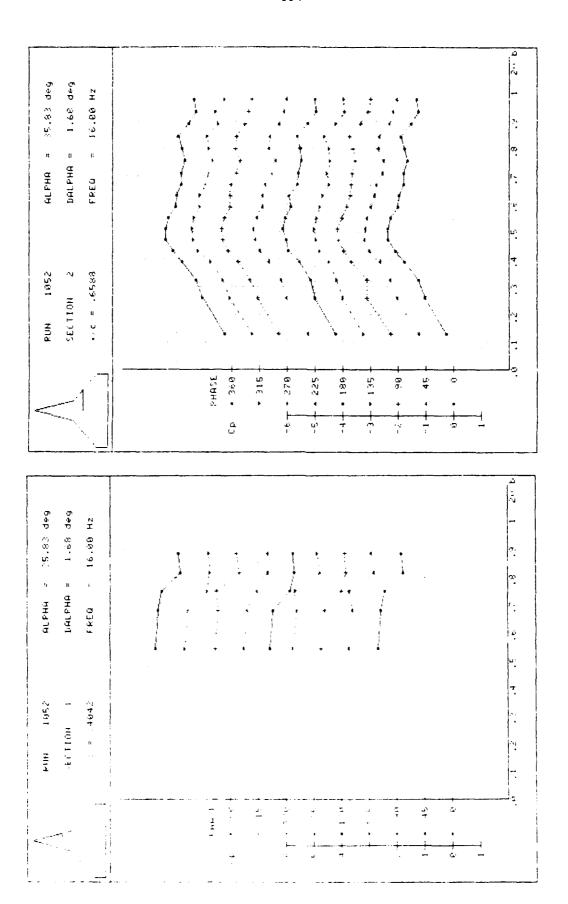


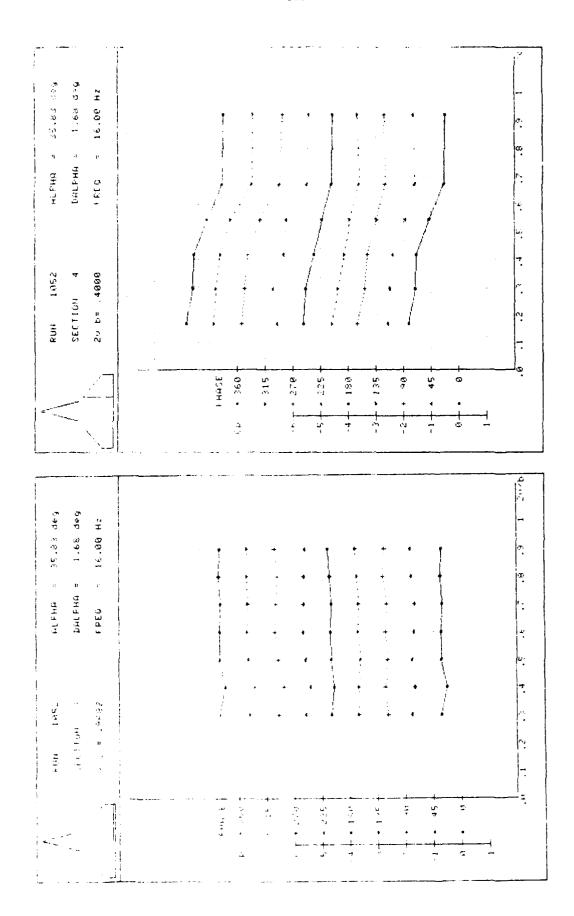


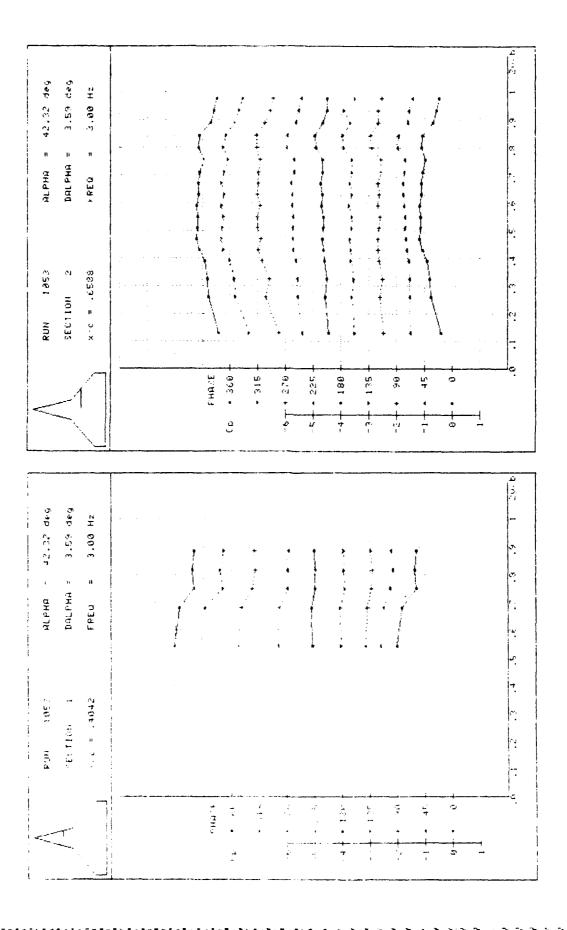


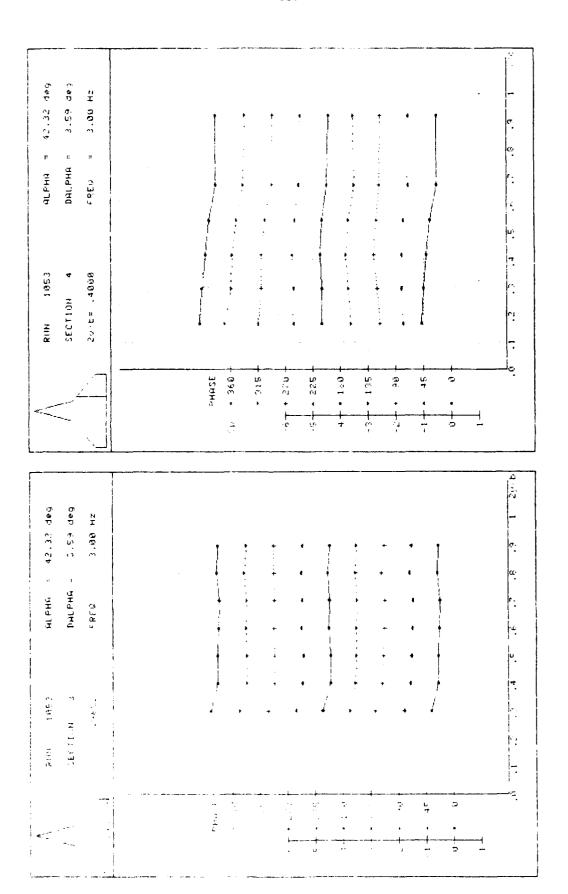
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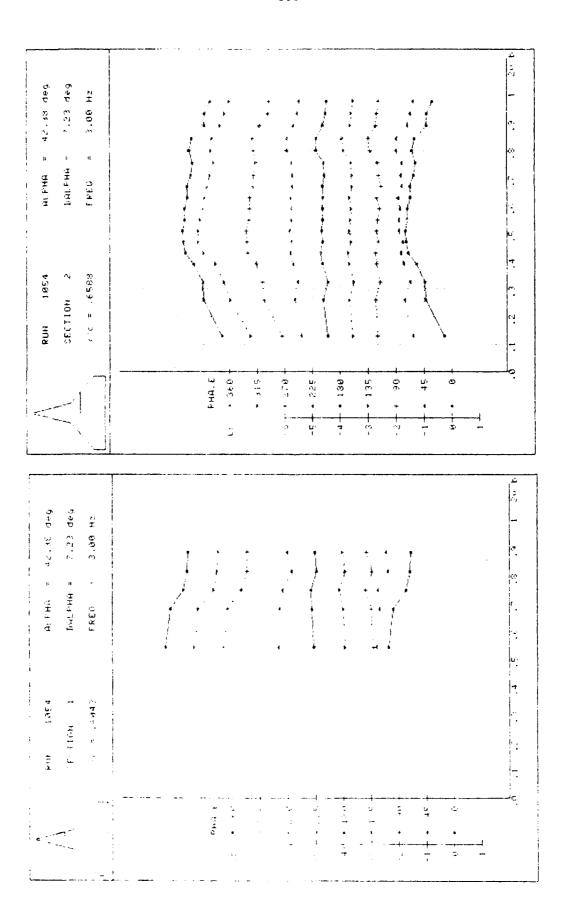


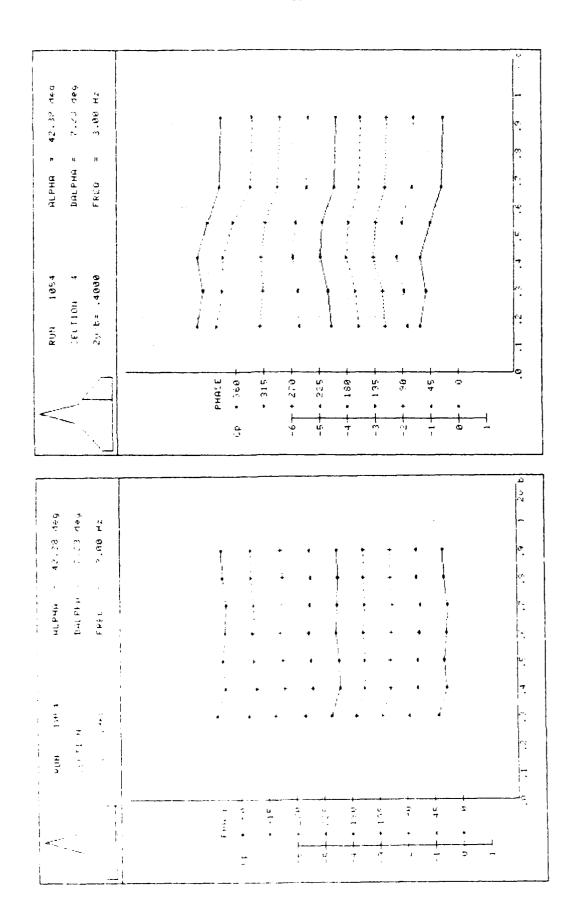


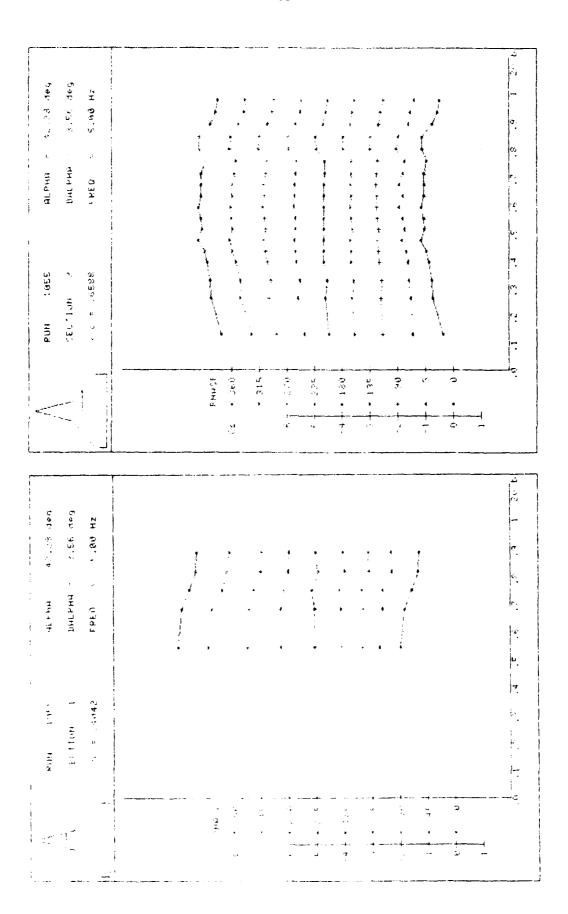


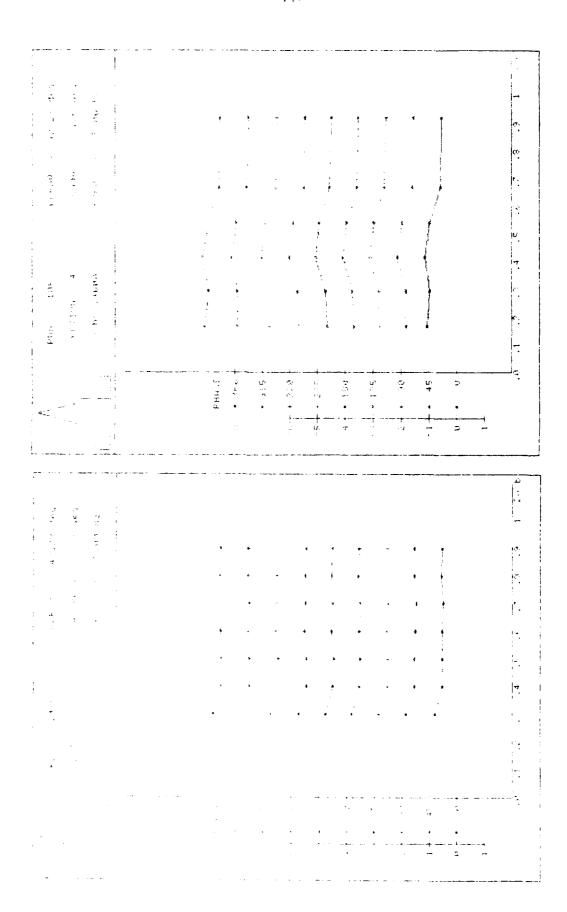


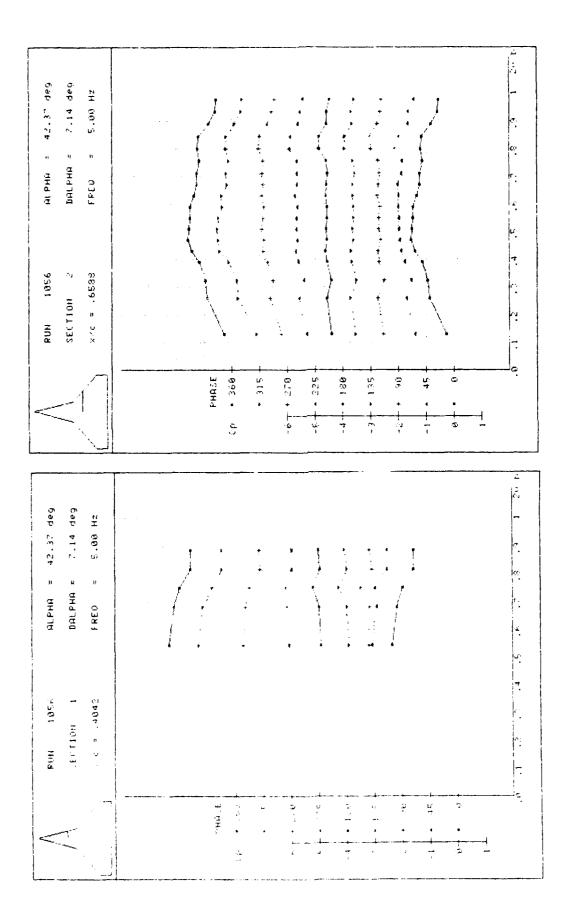


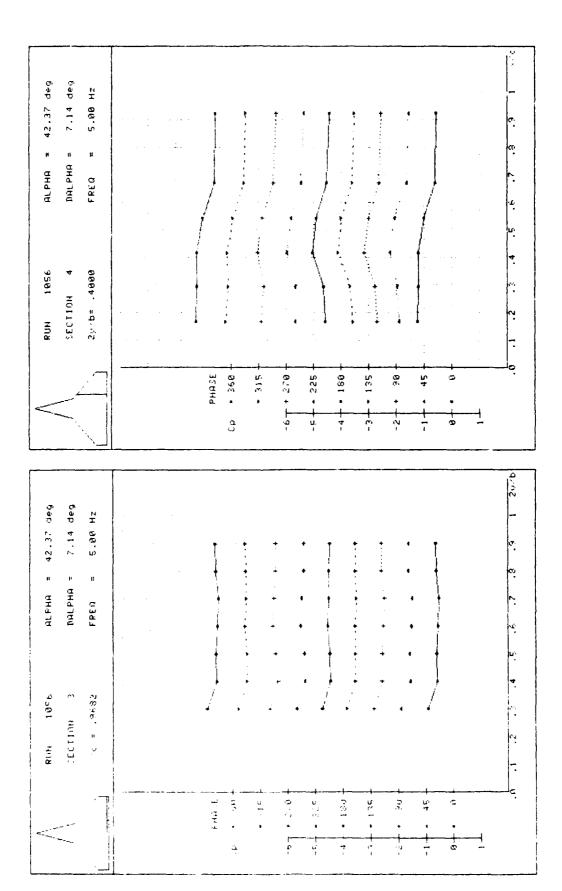




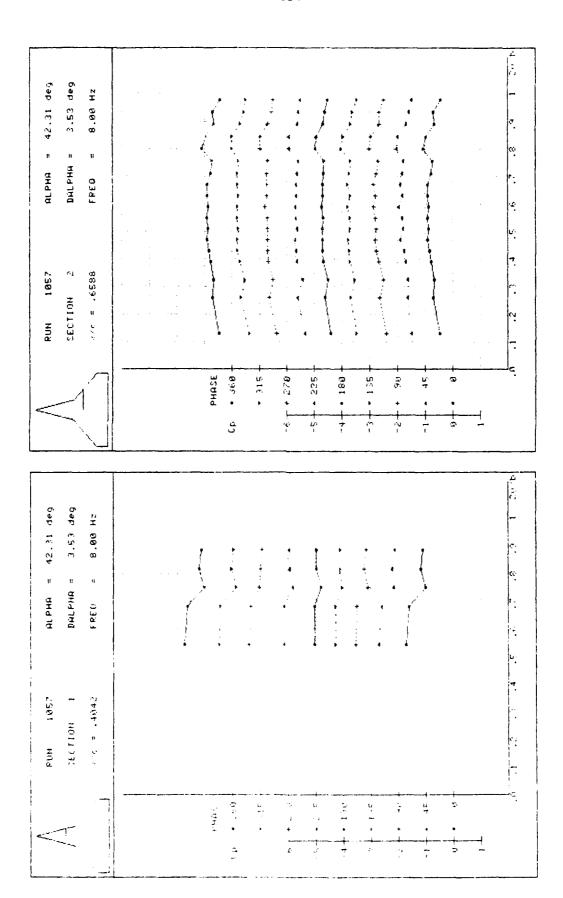


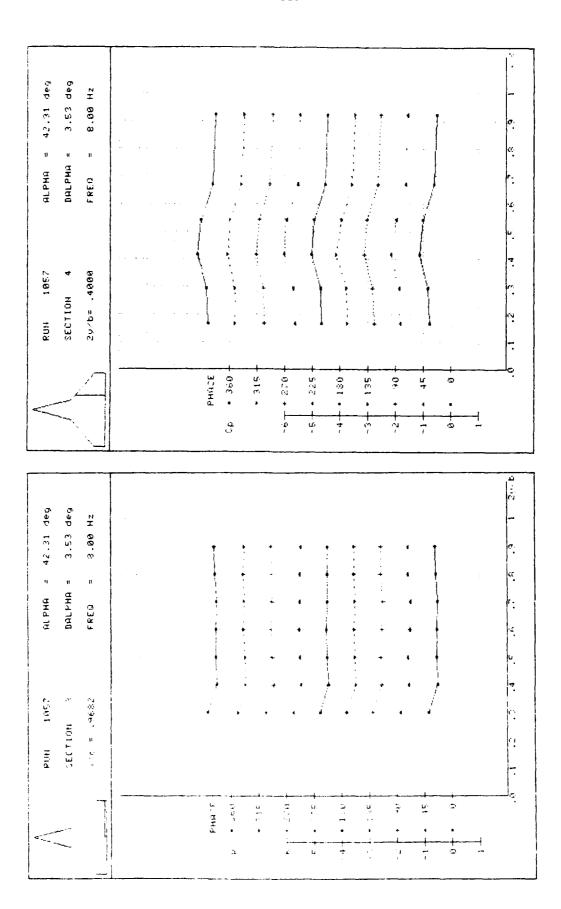


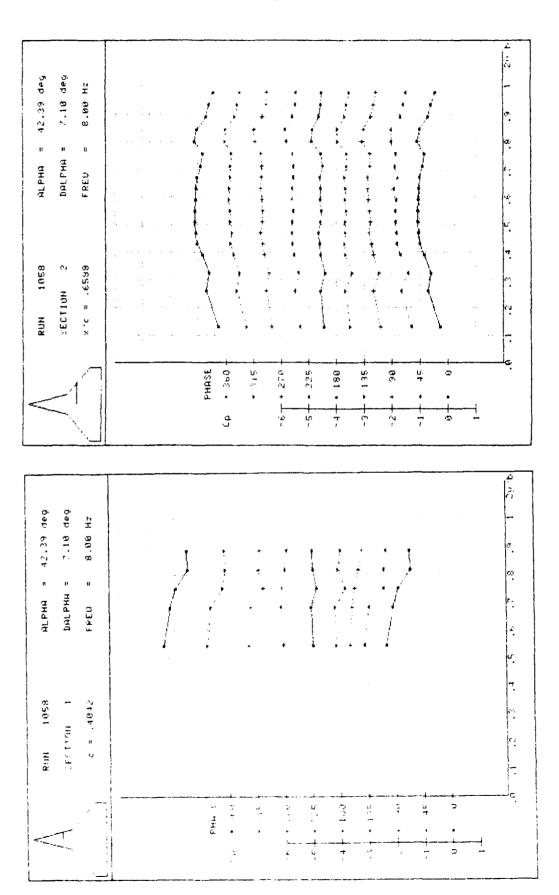


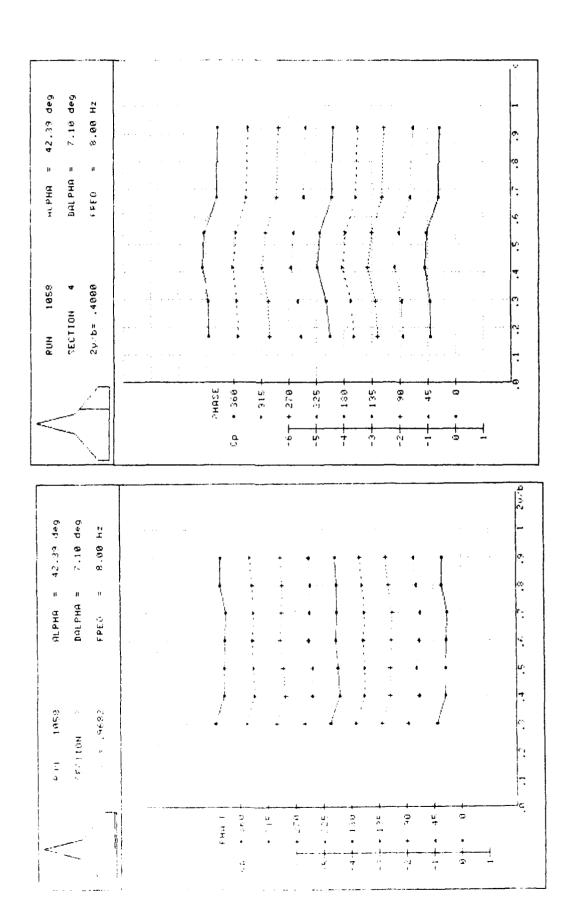


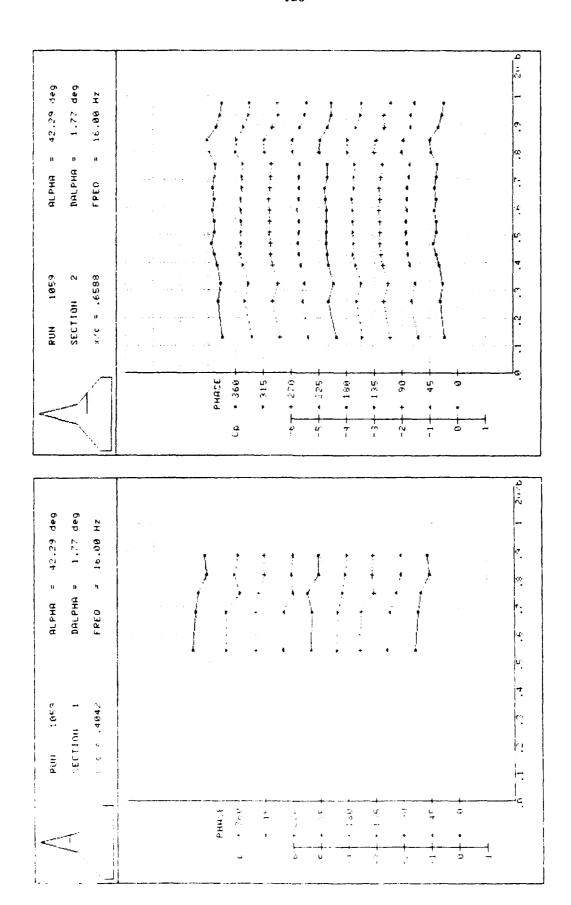
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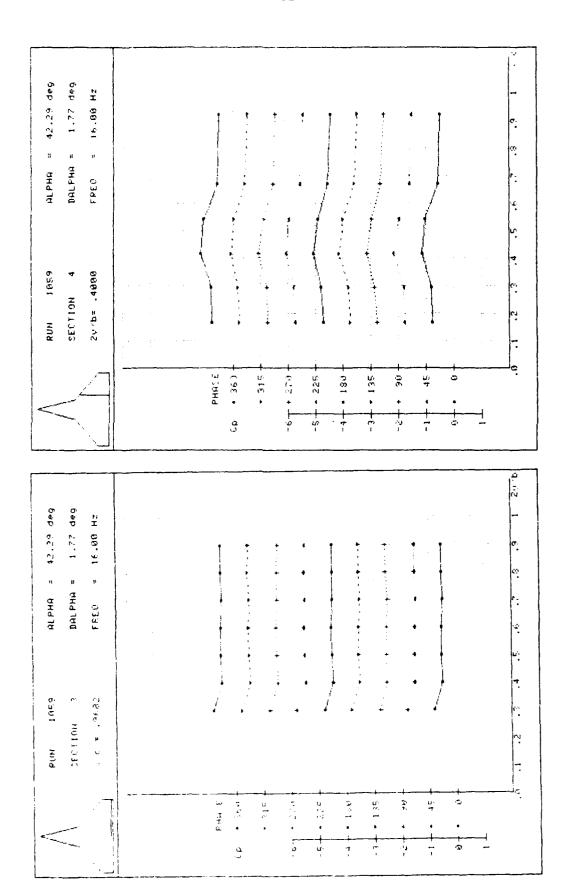








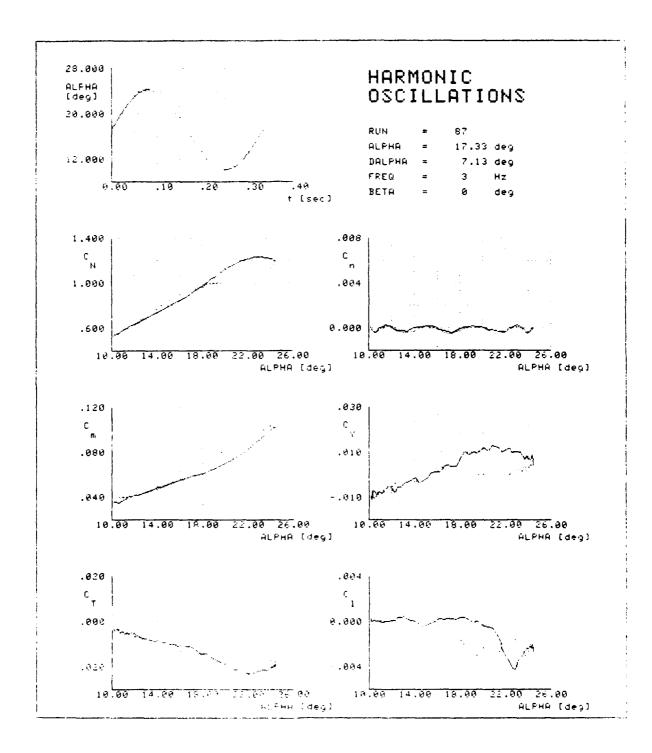


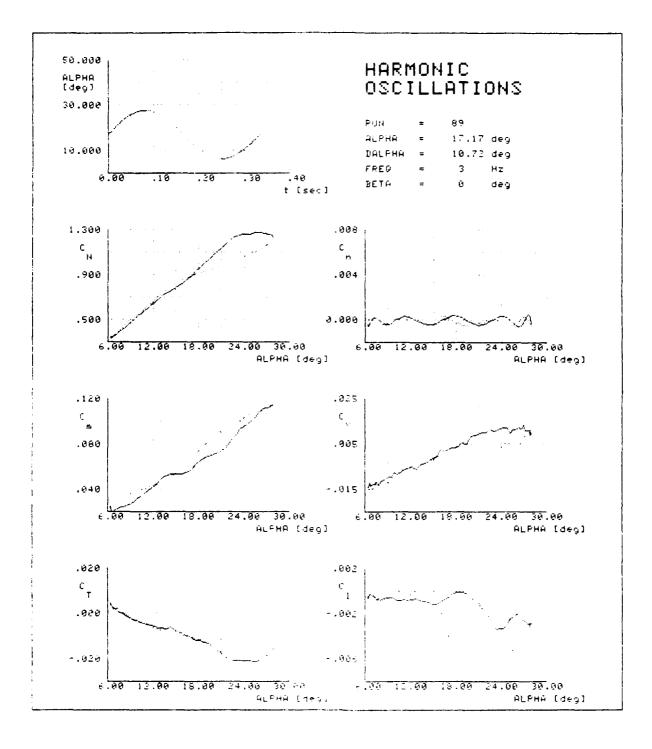


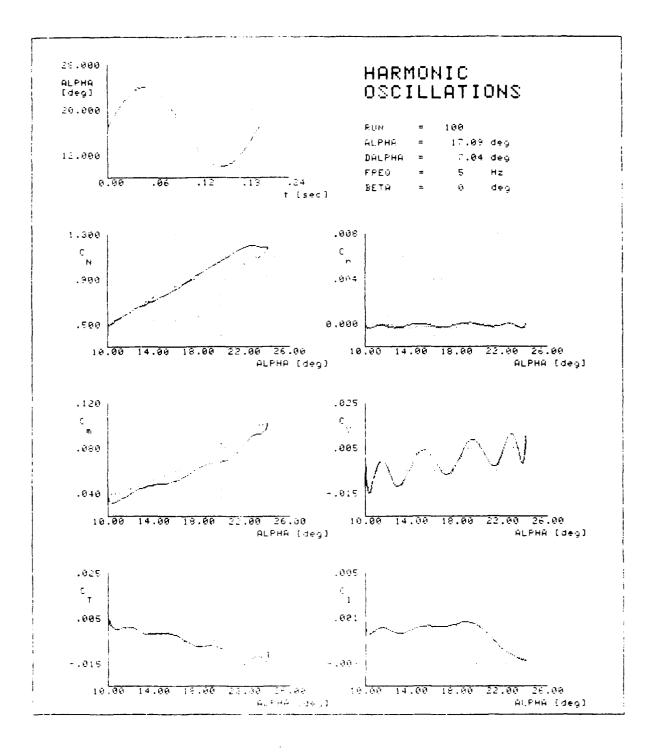
APPENDIX B

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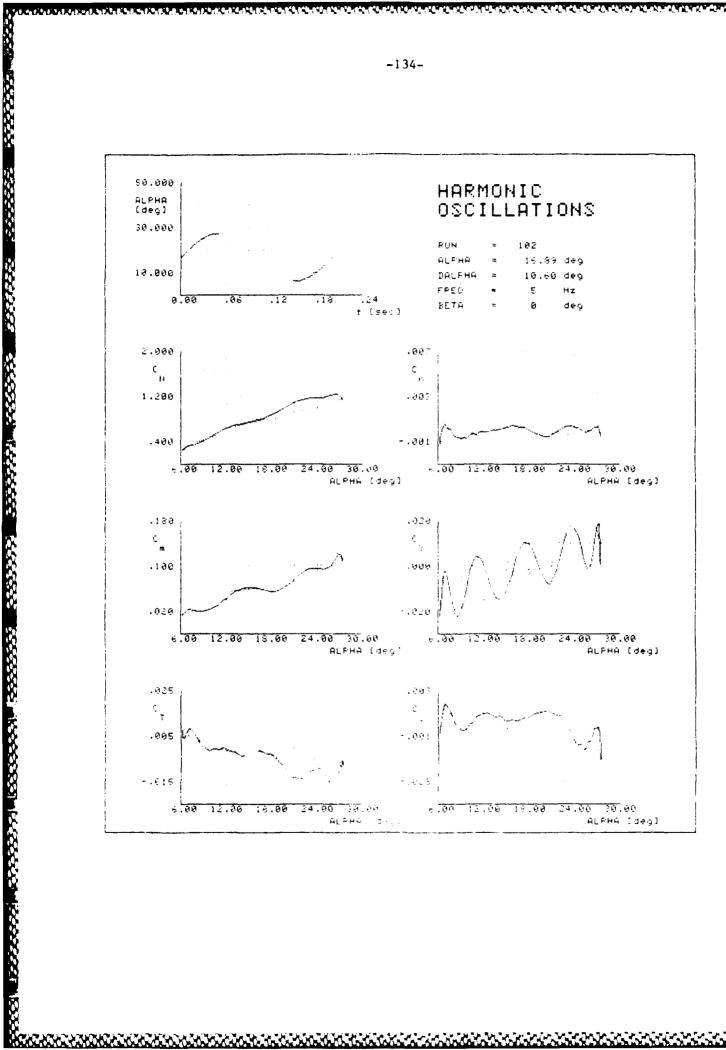
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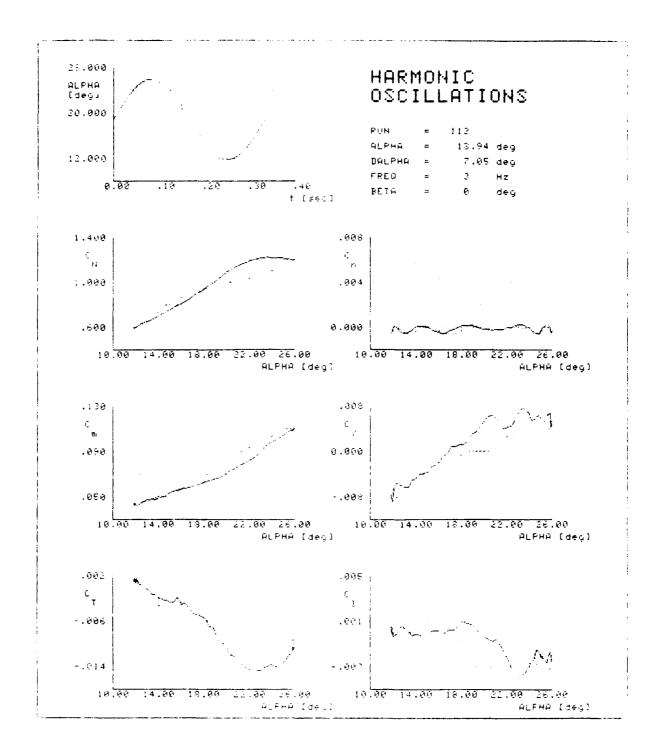


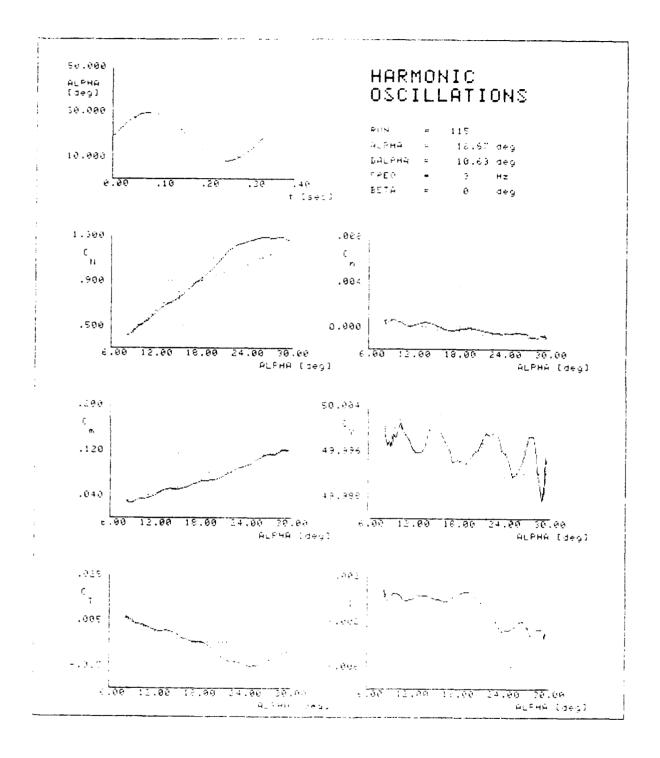




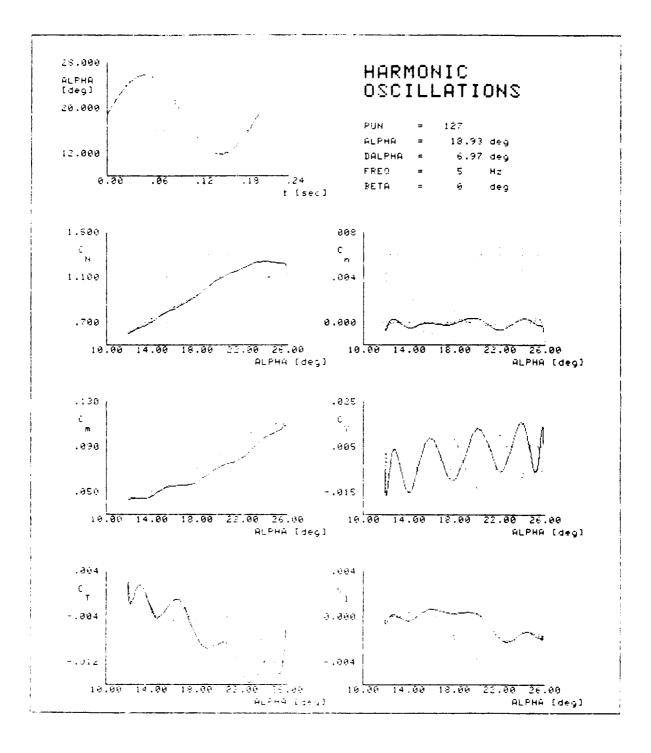
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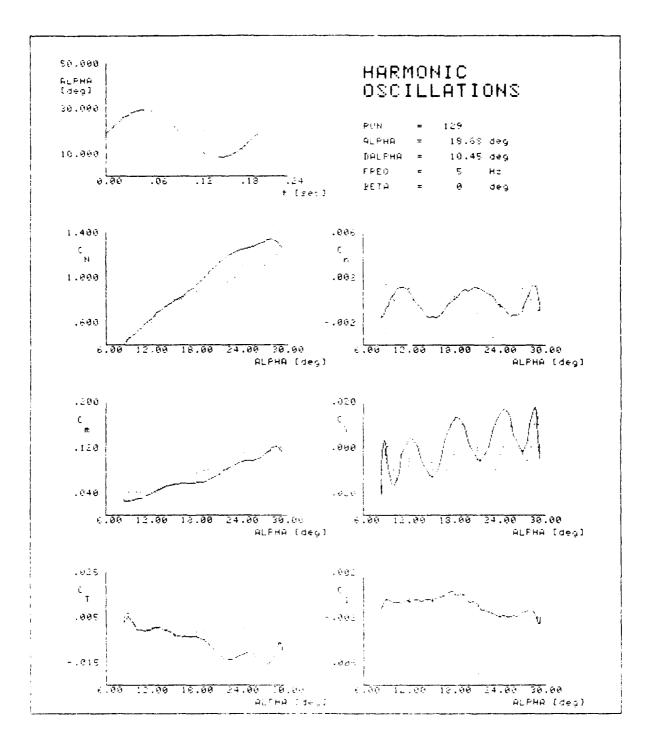


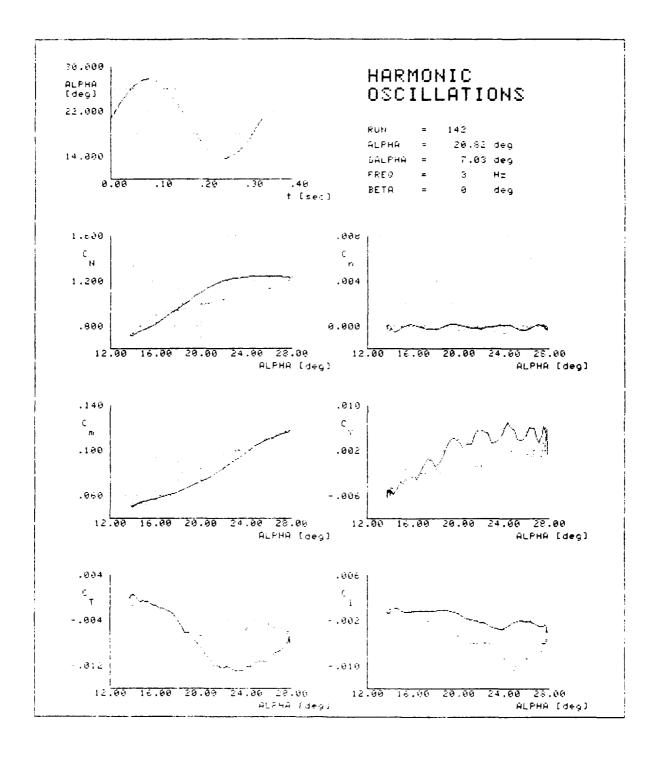


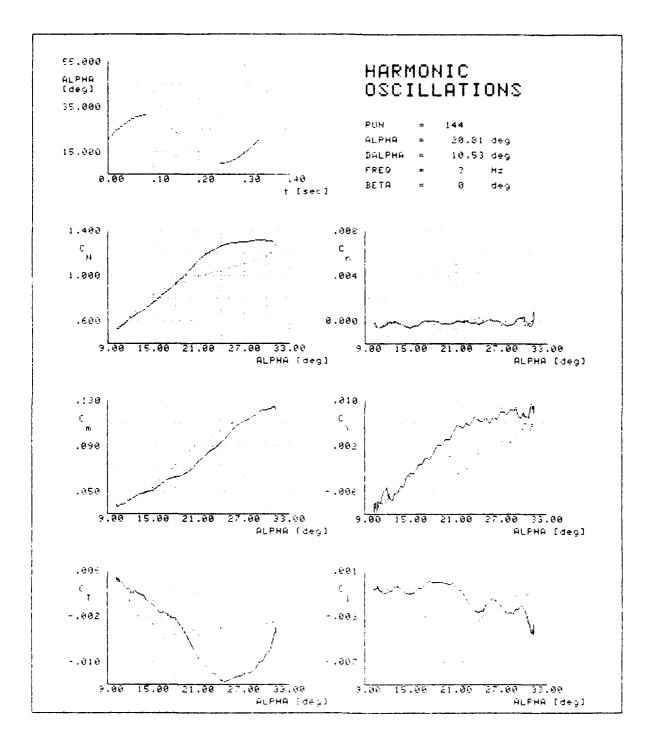


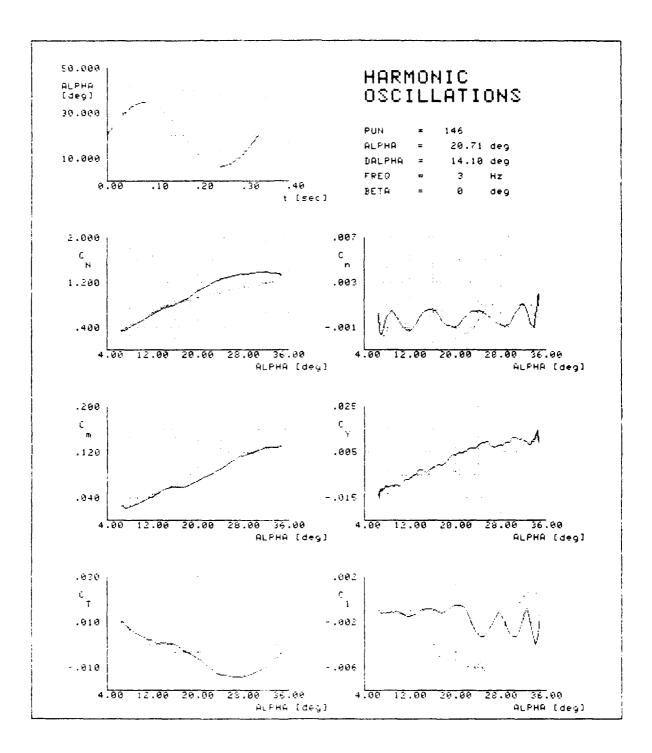
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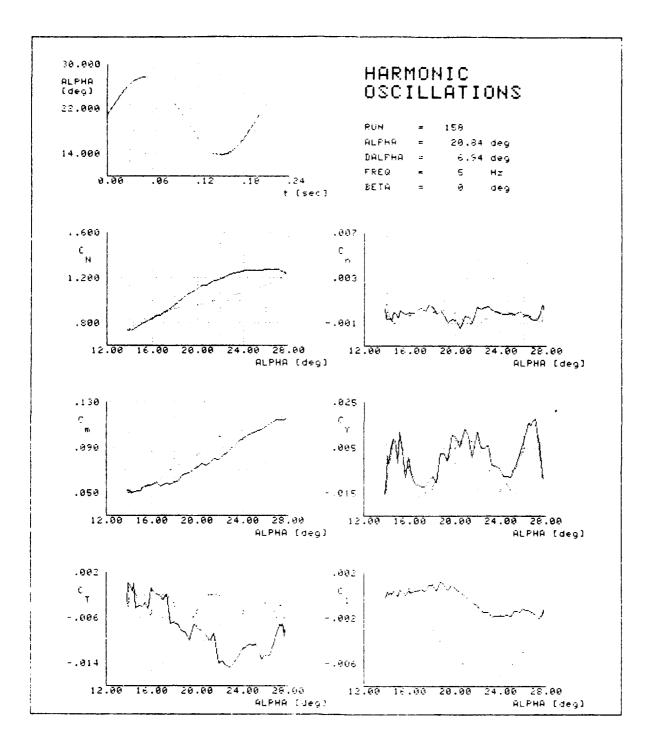


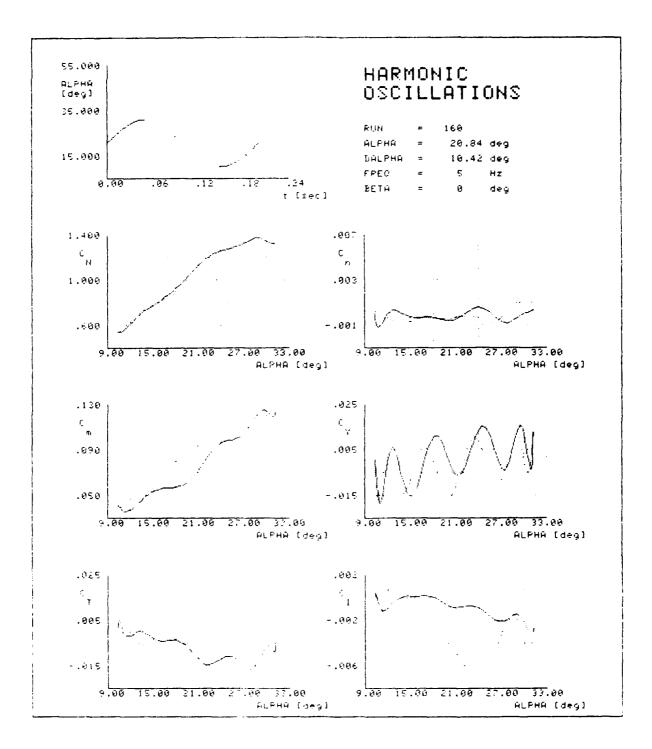


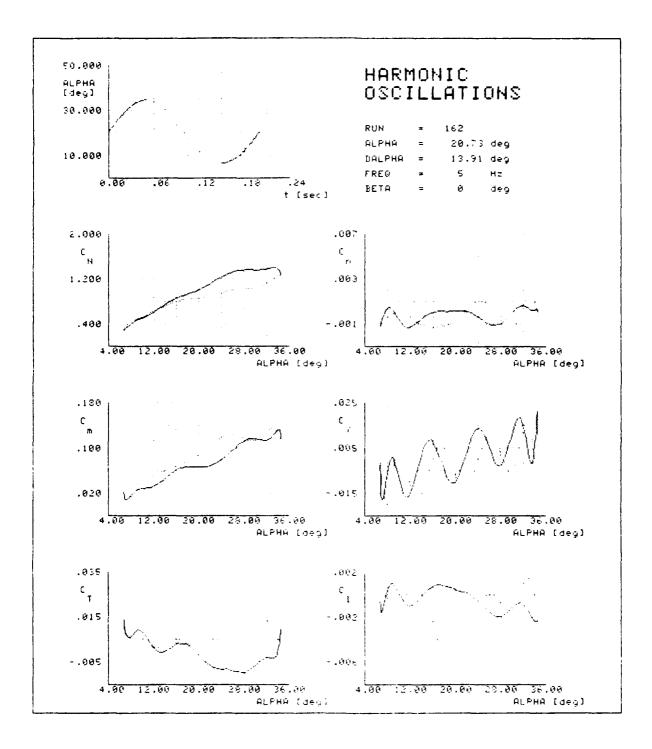


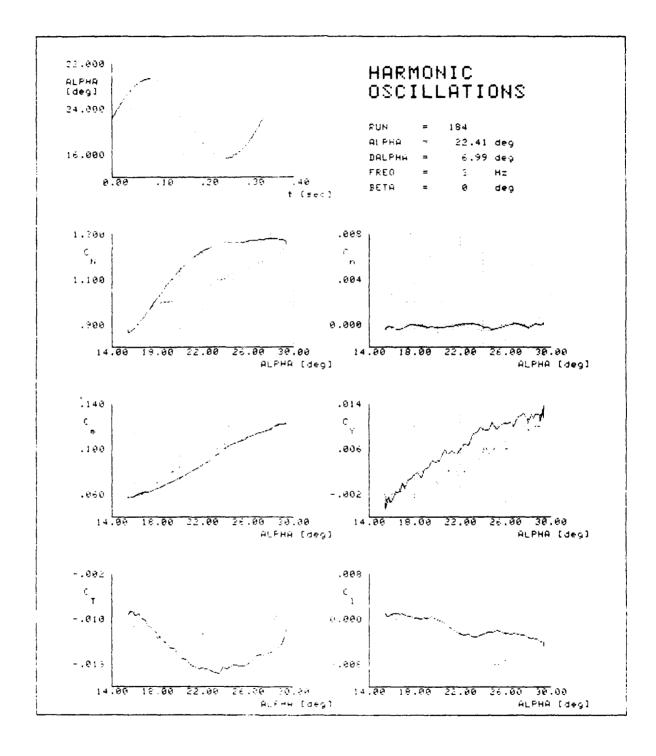


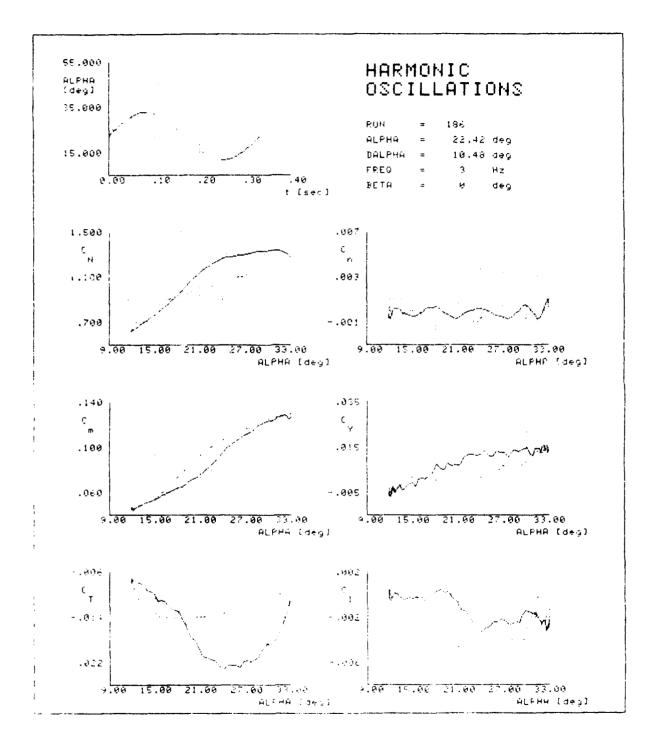


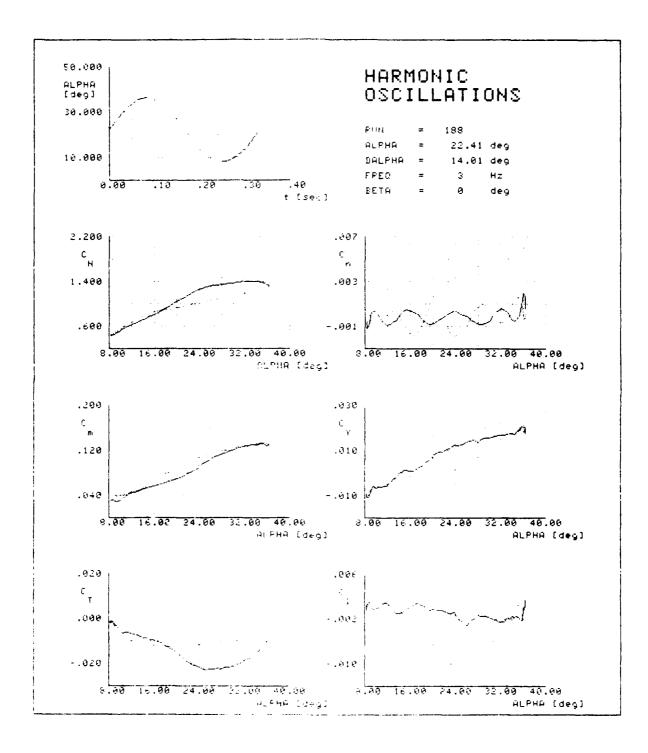


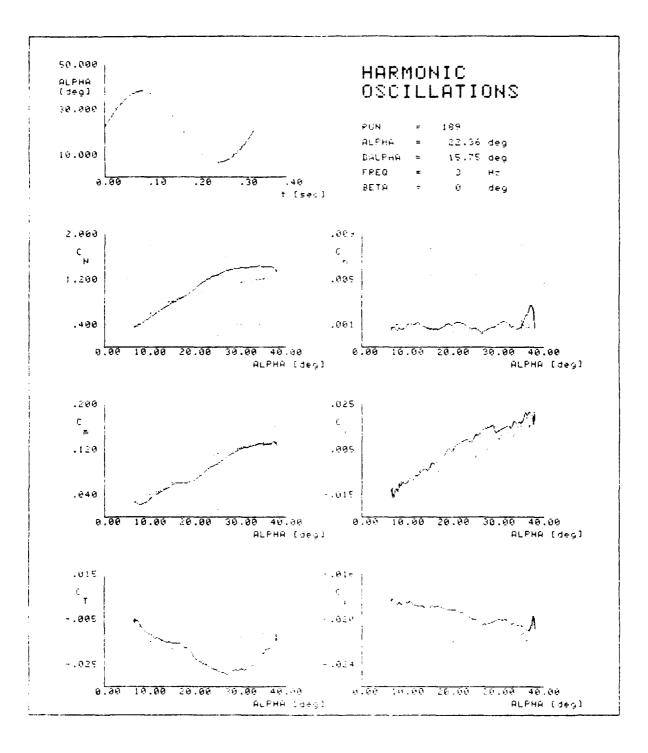


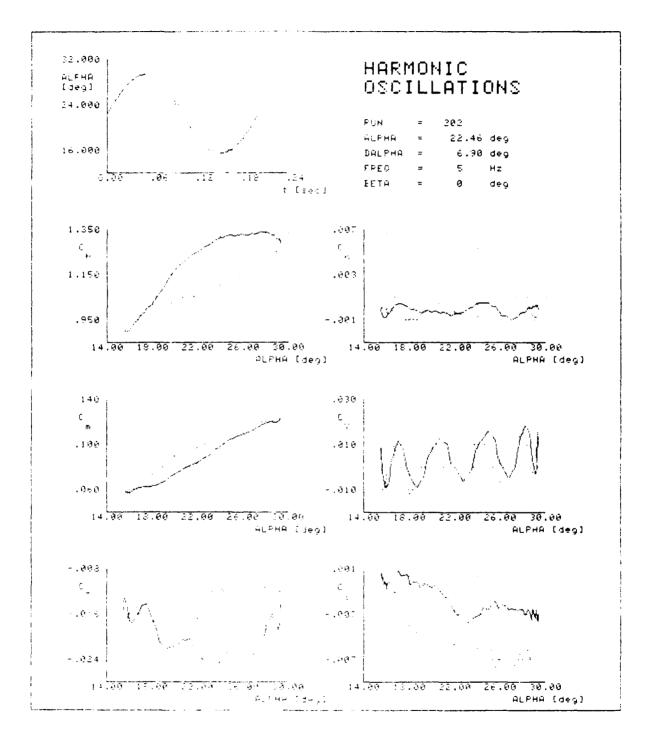




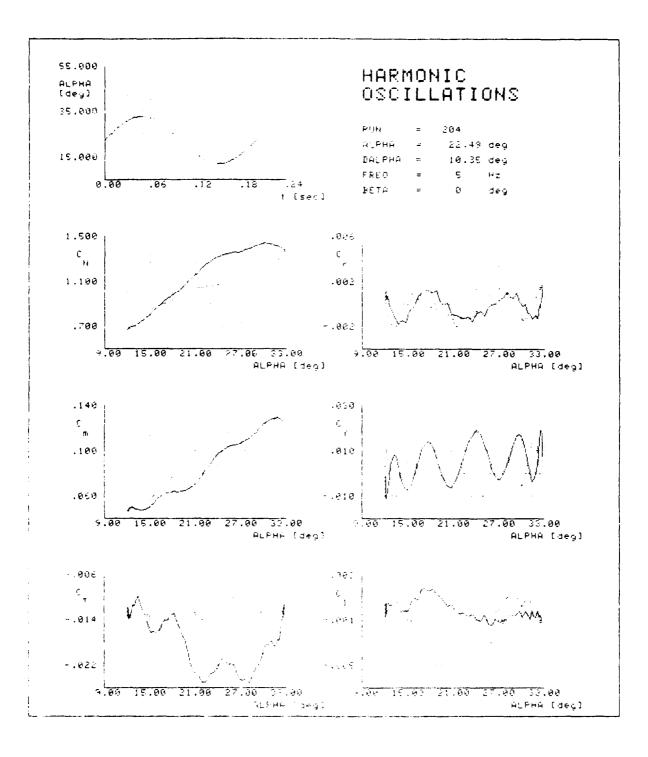


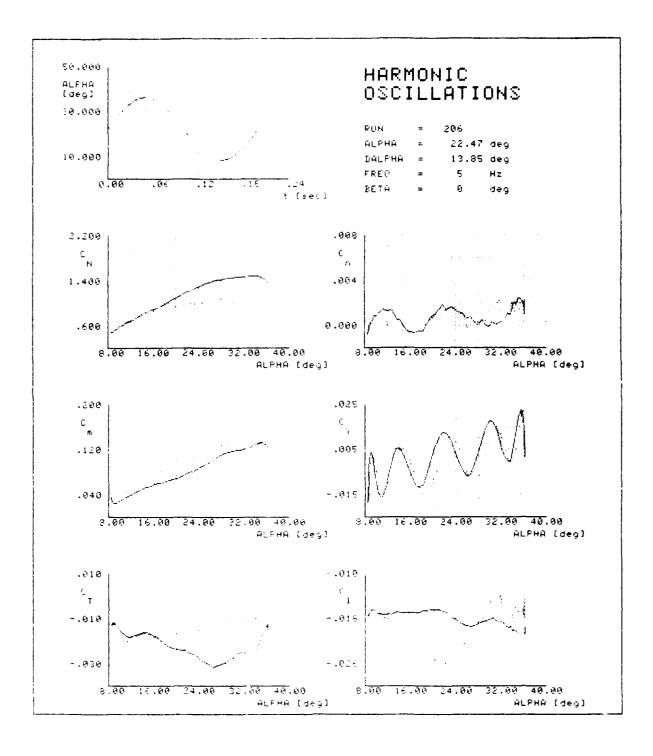


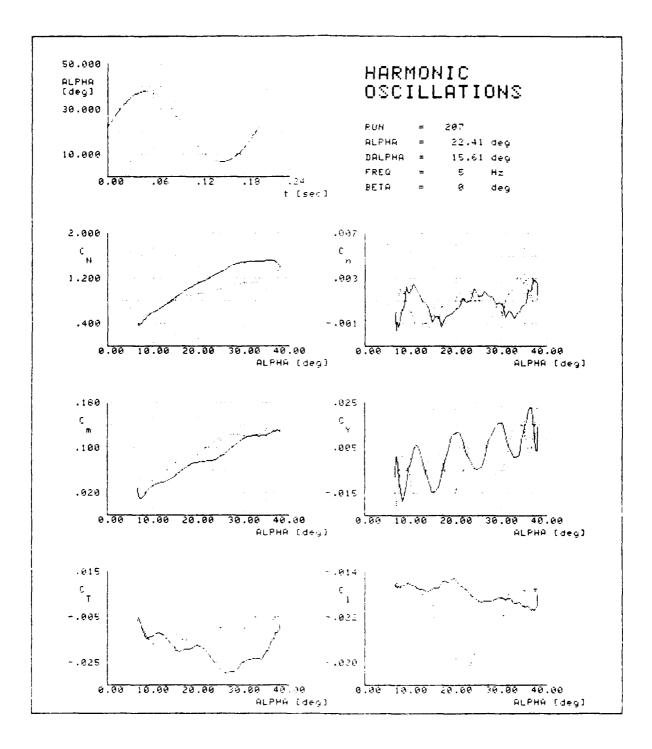


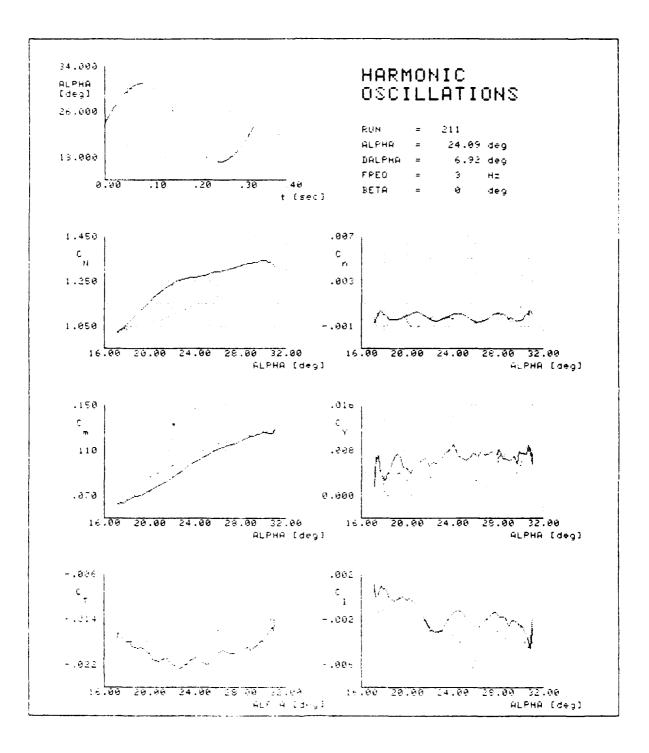


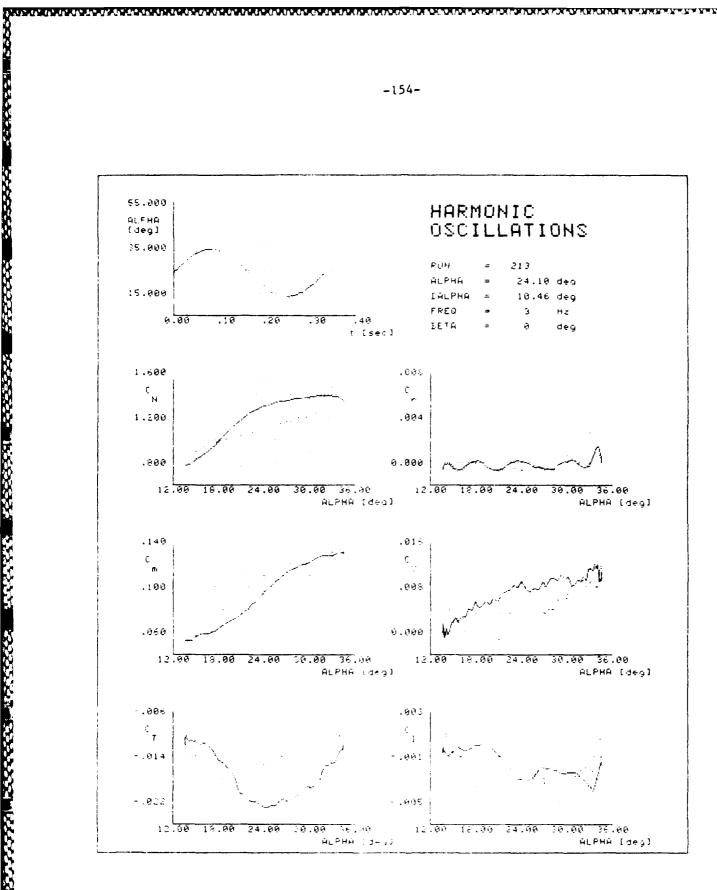
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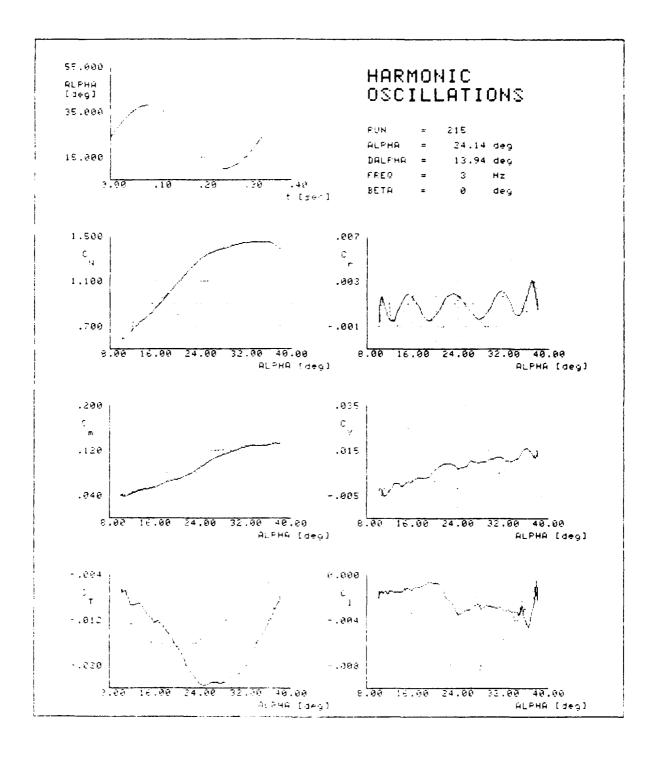


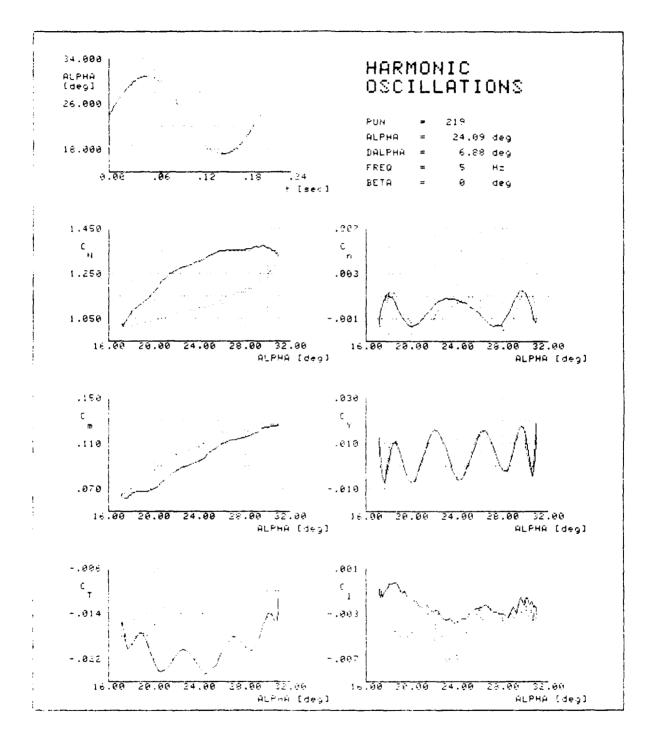




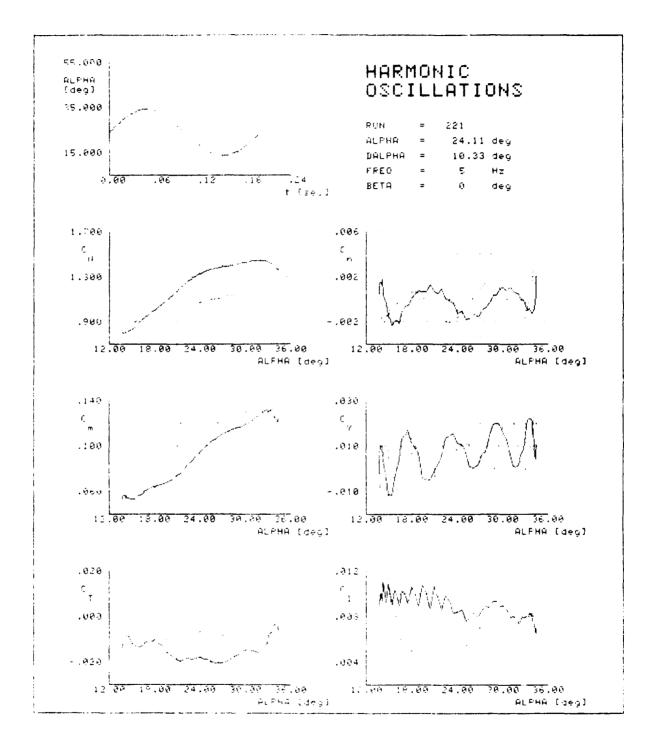


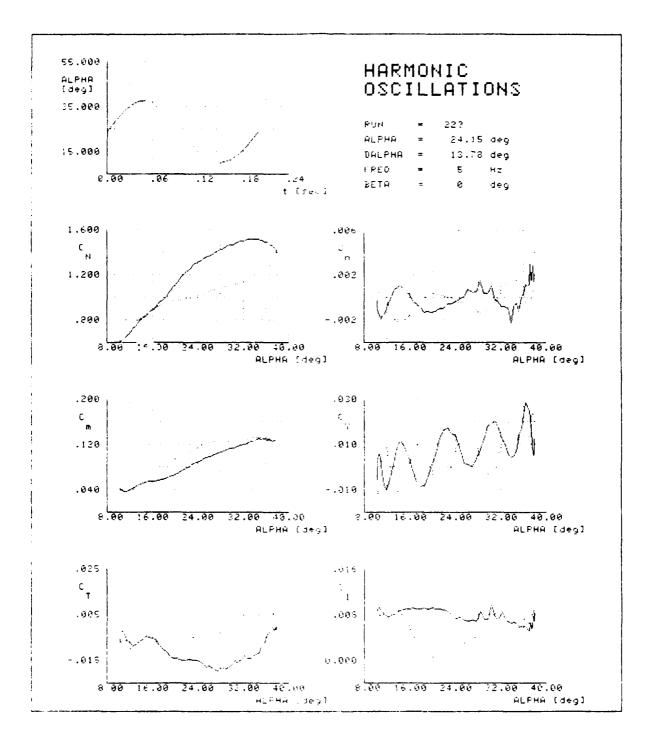


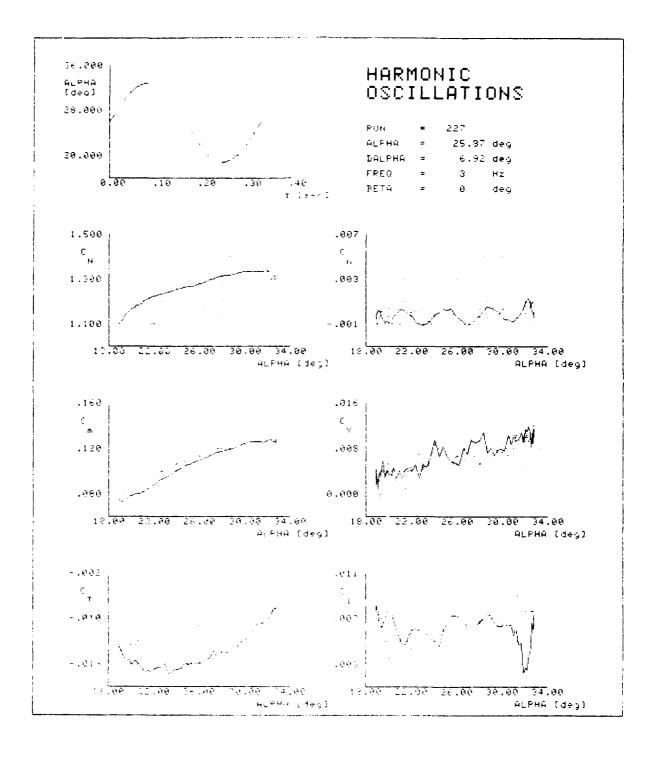




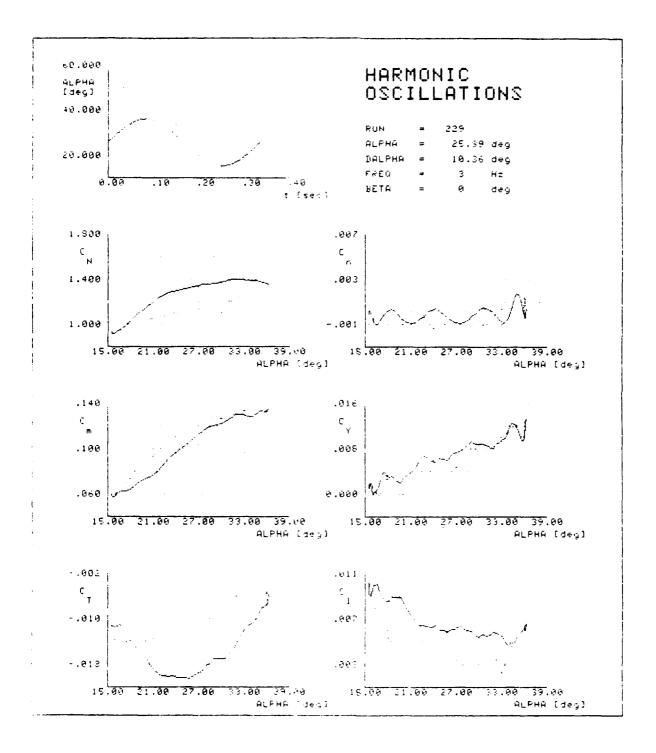
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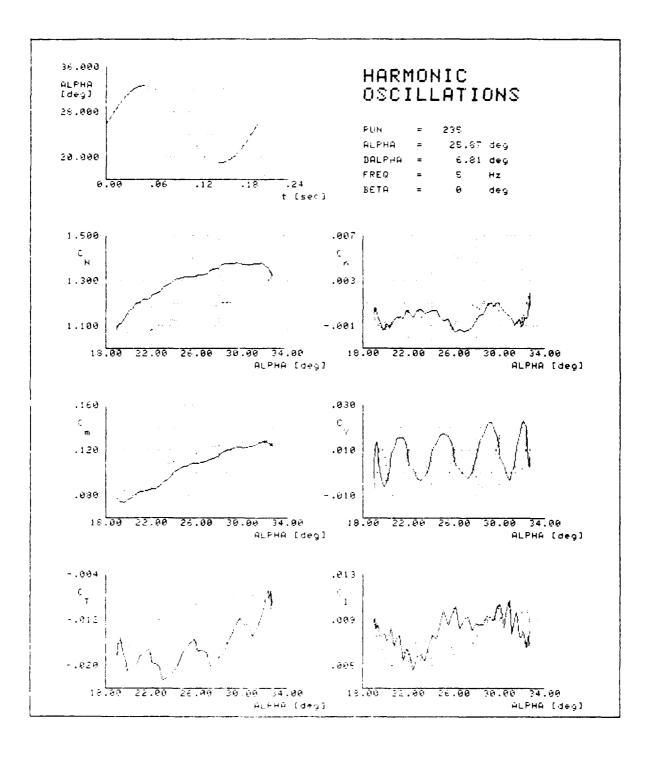


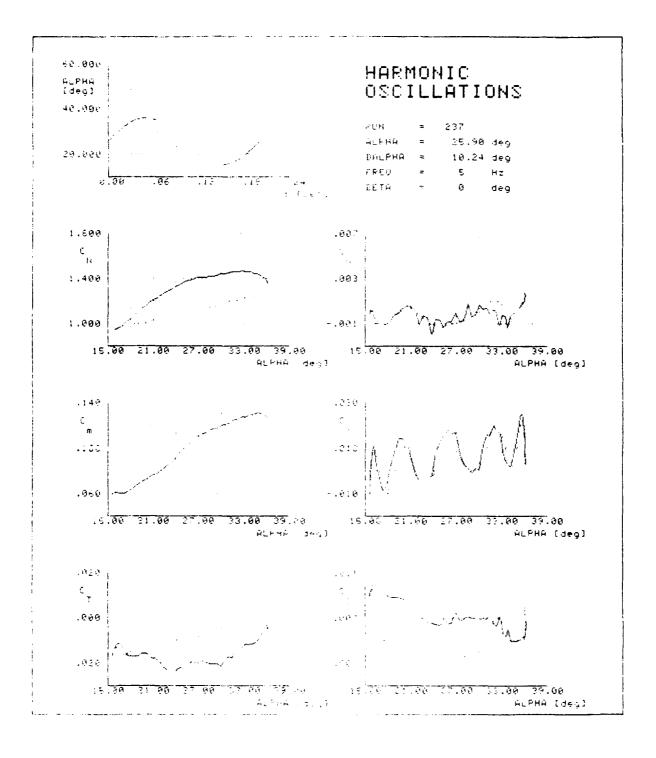


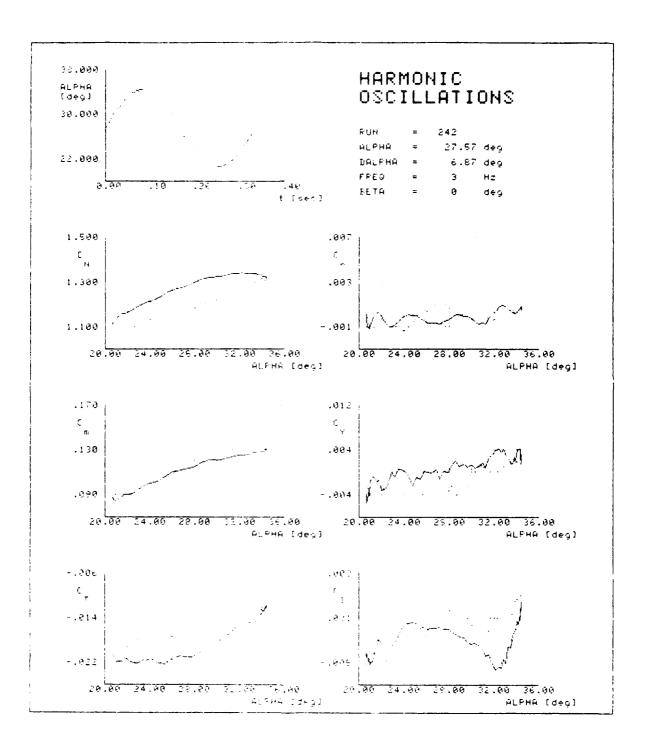


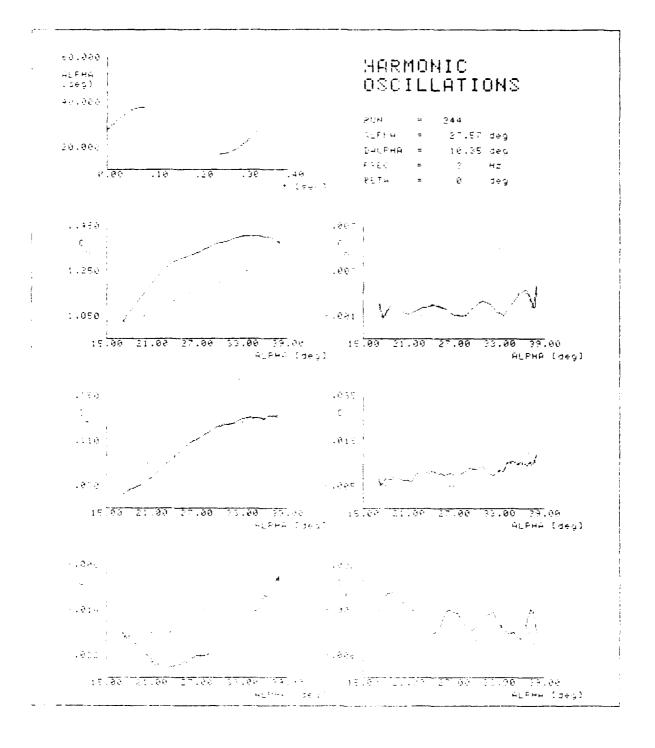
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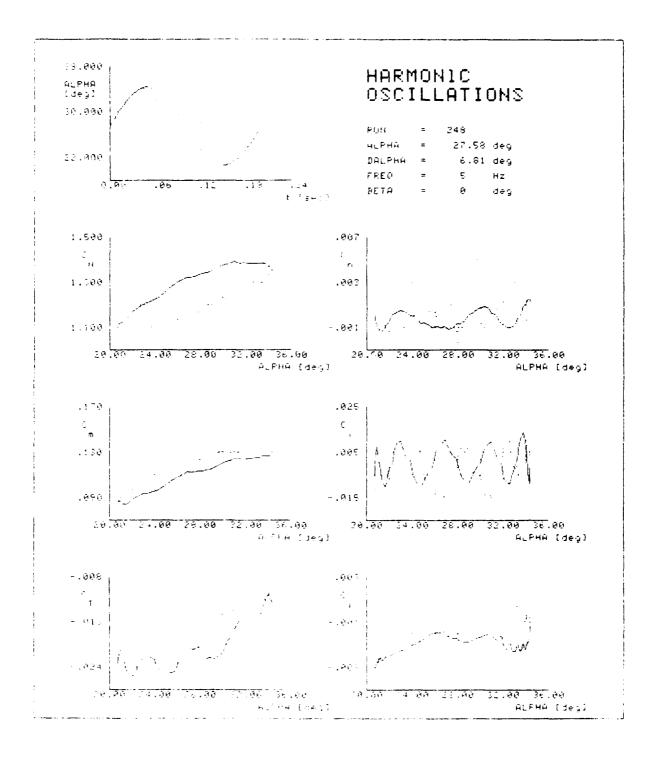


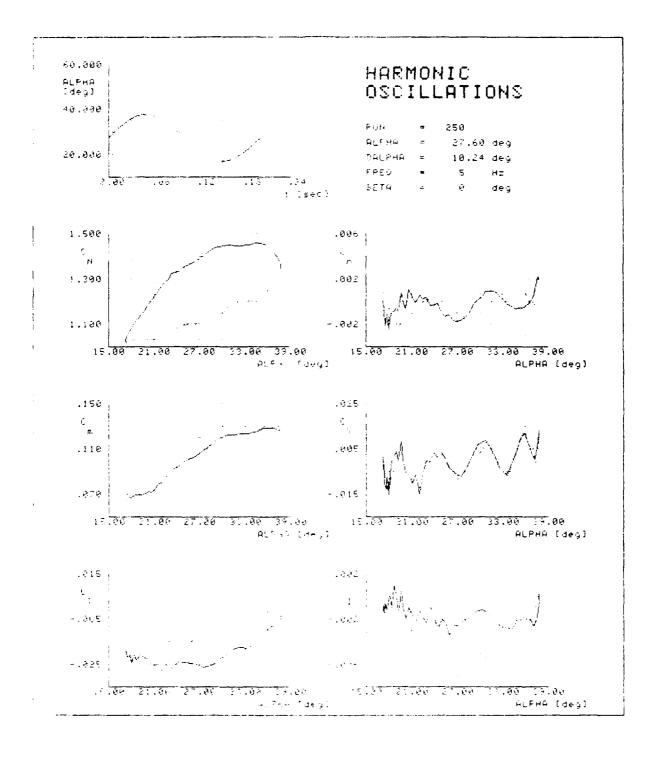






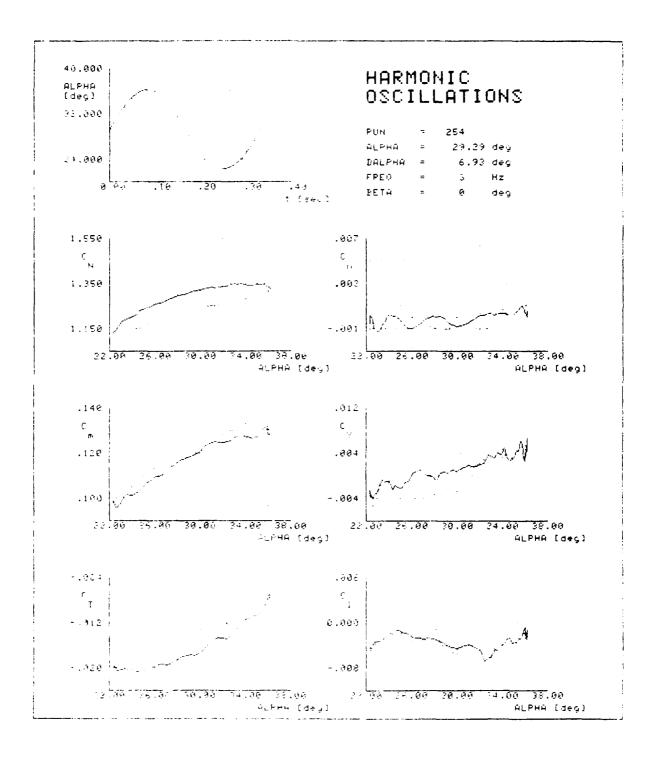


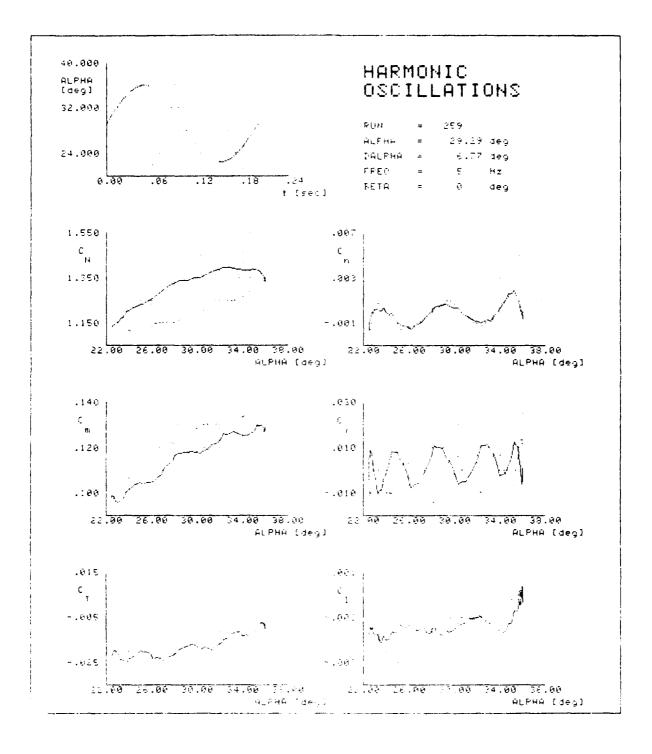


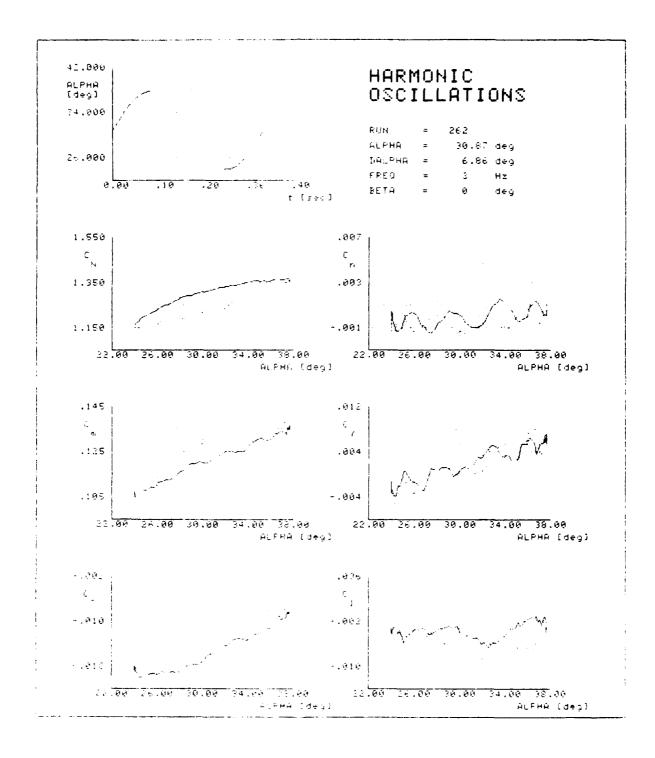


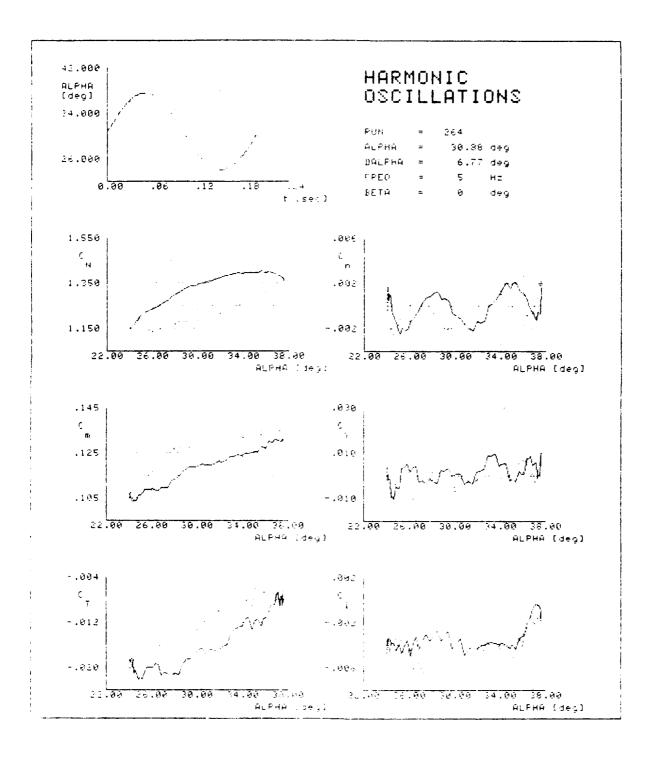
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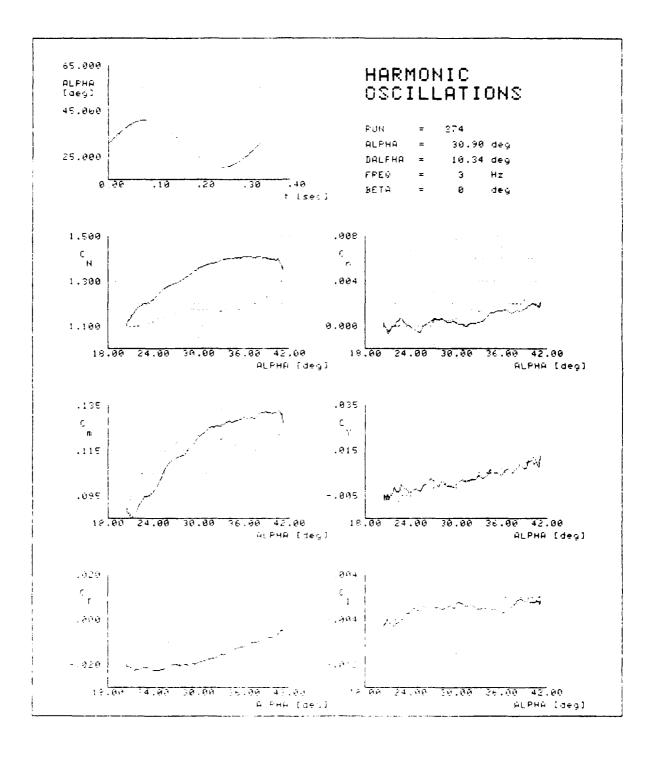


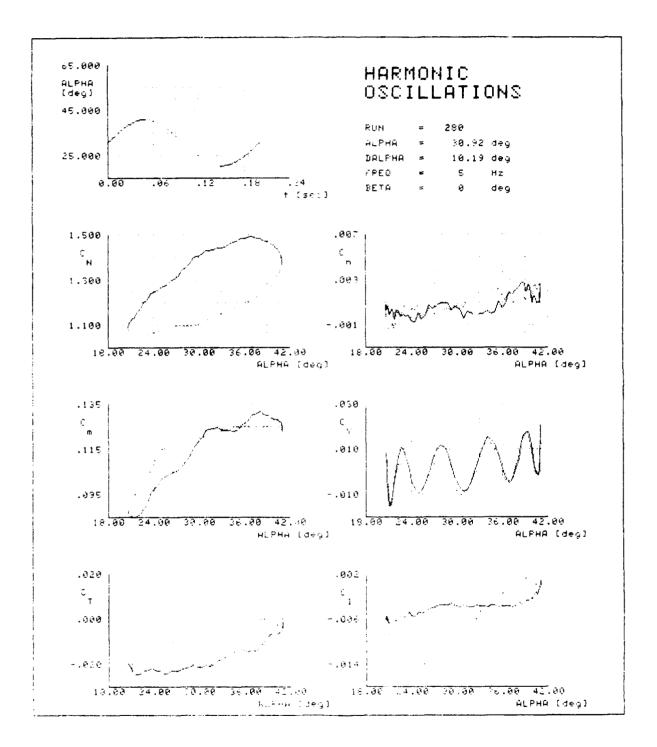






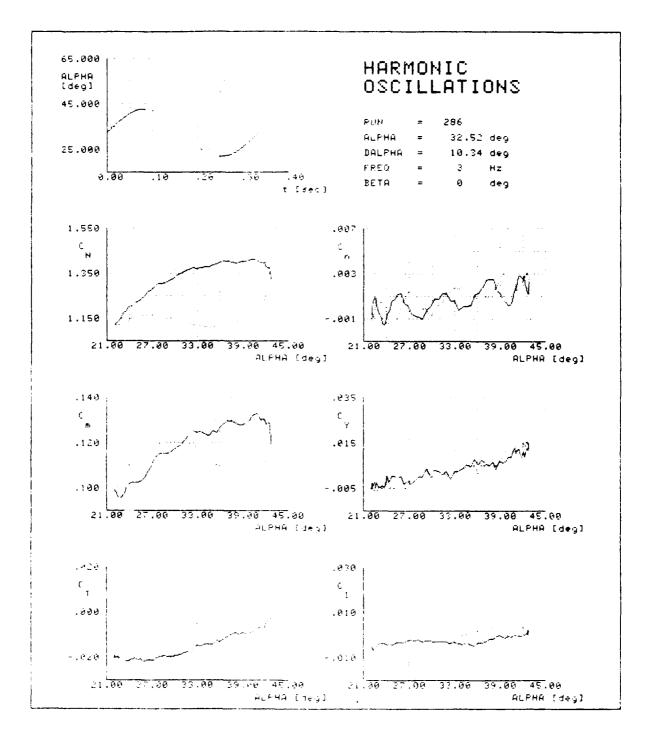
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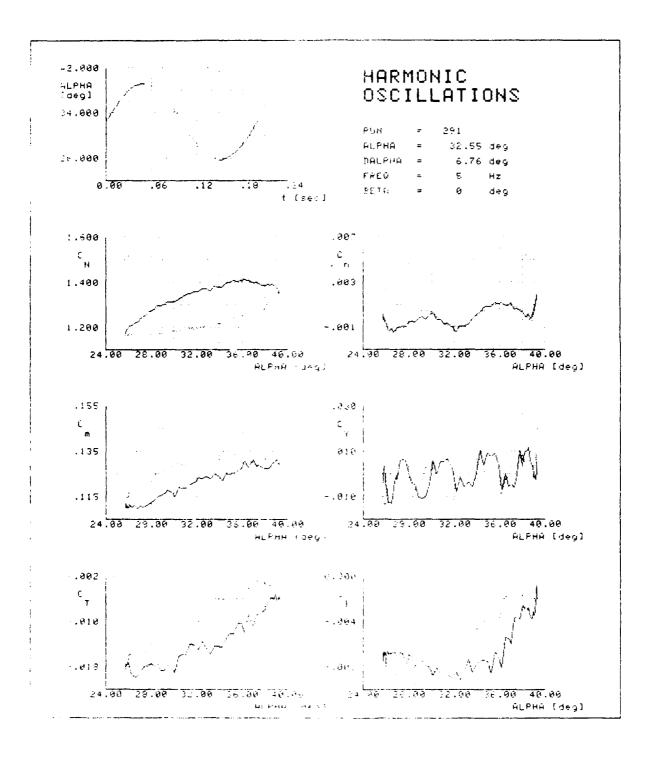


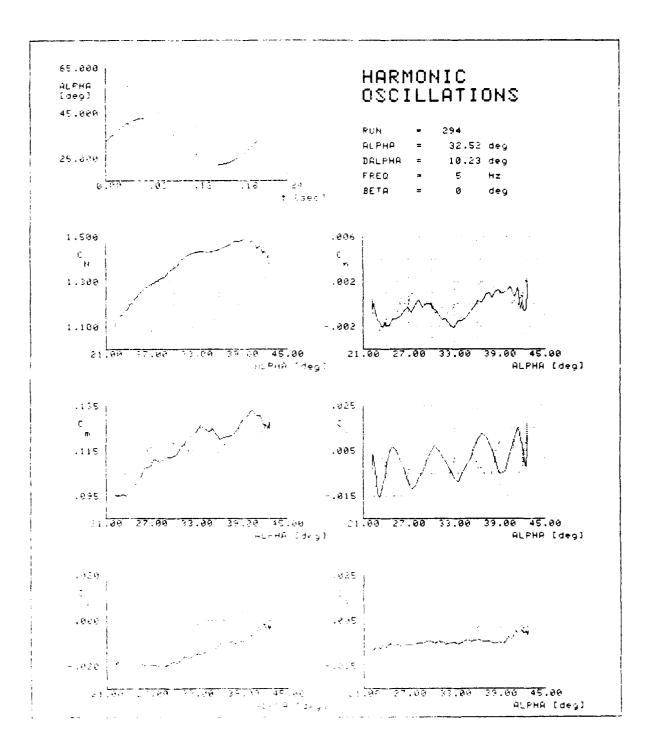


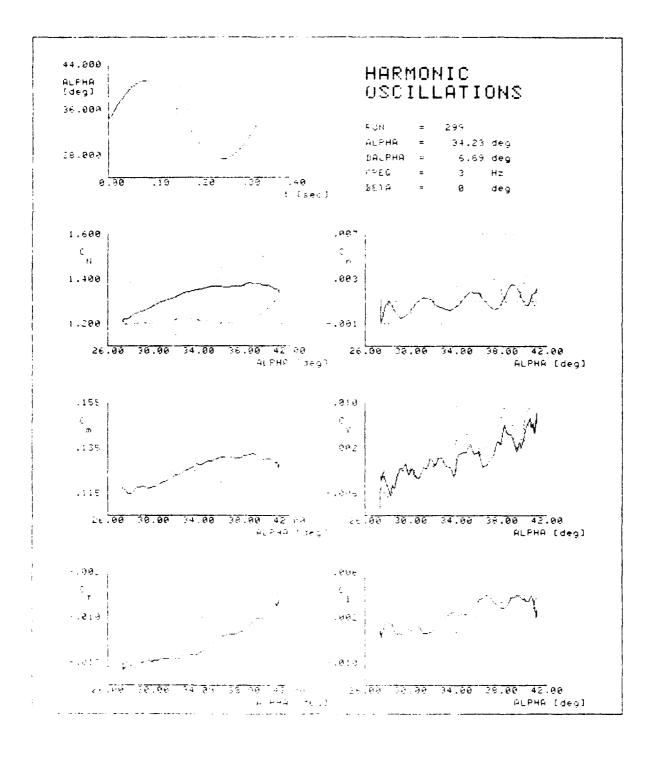
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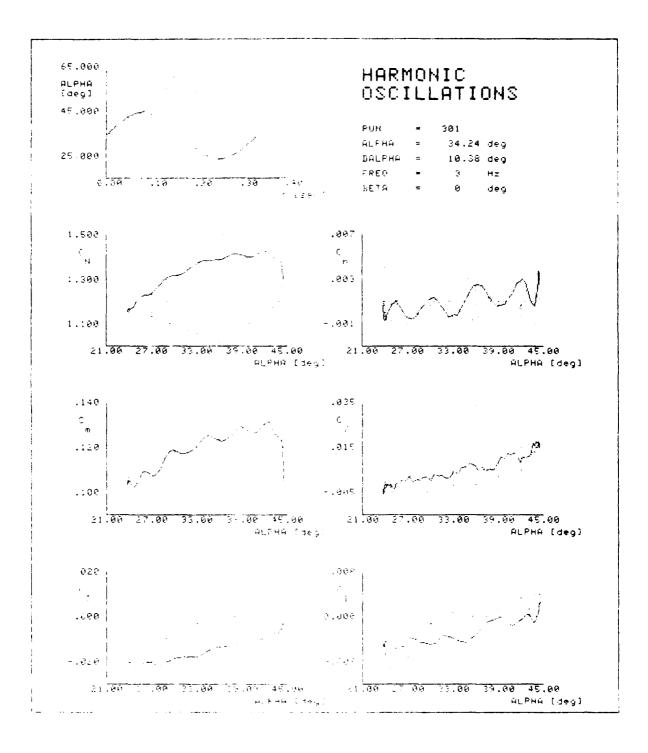
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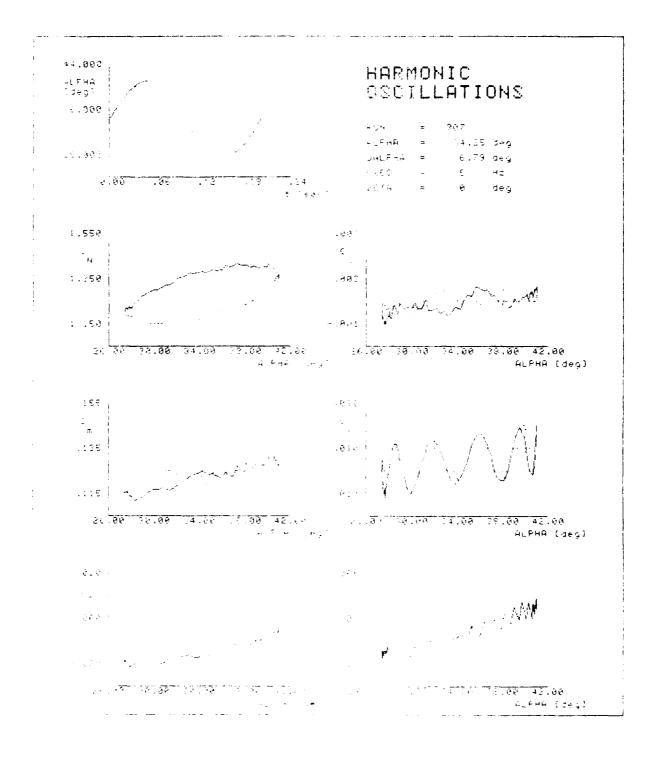


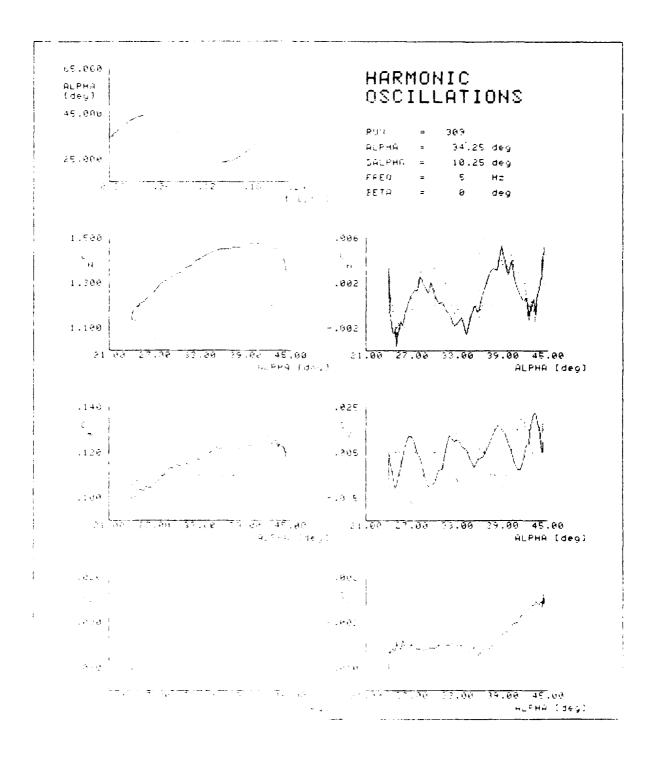


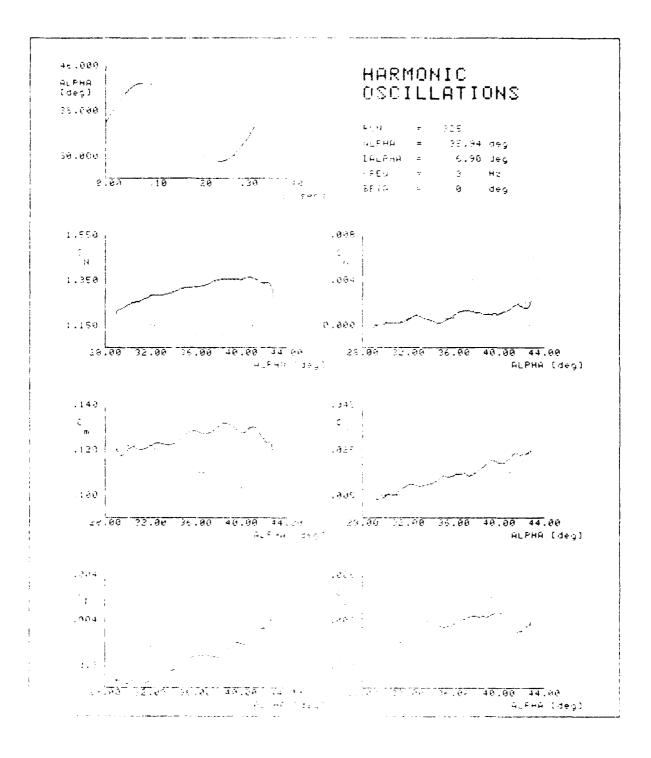


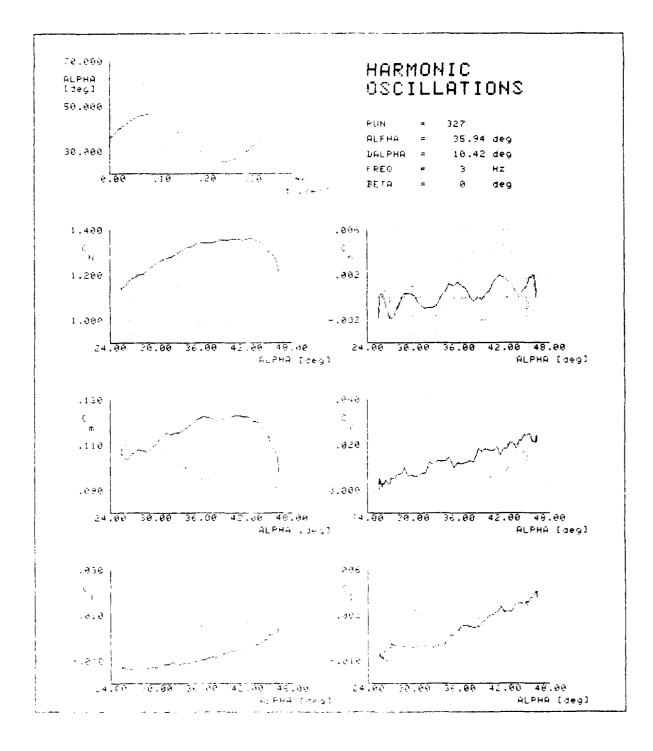


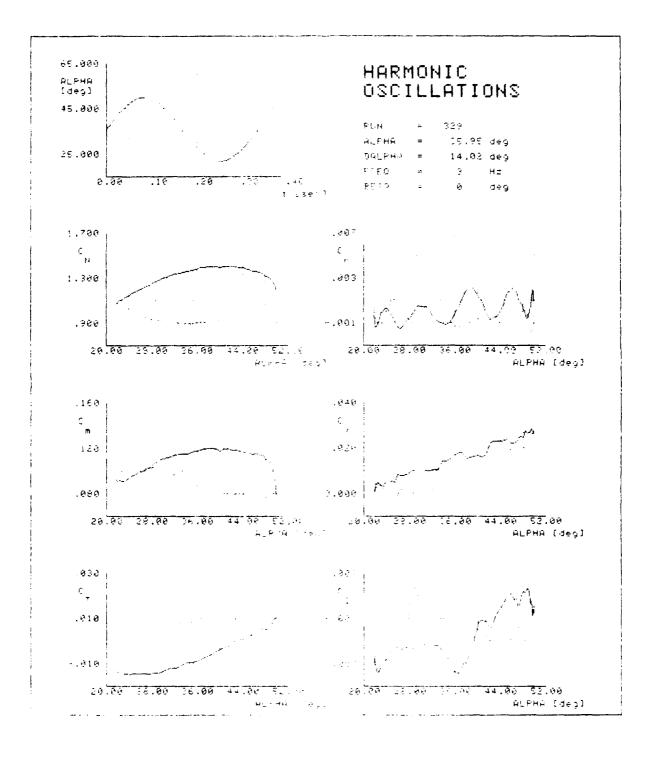


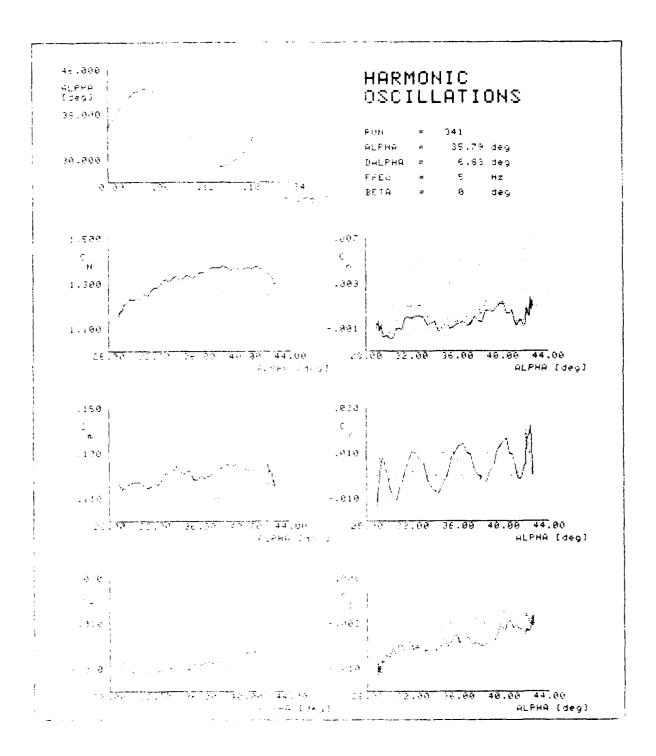


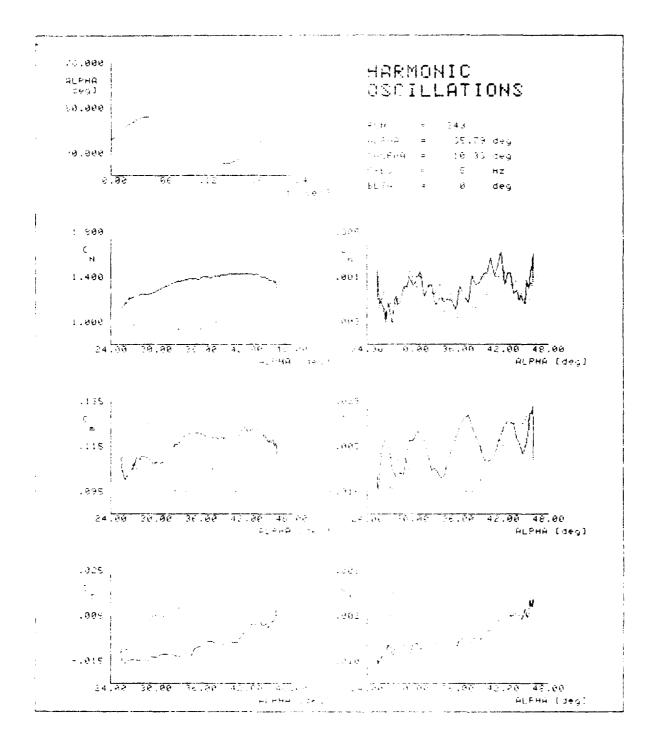


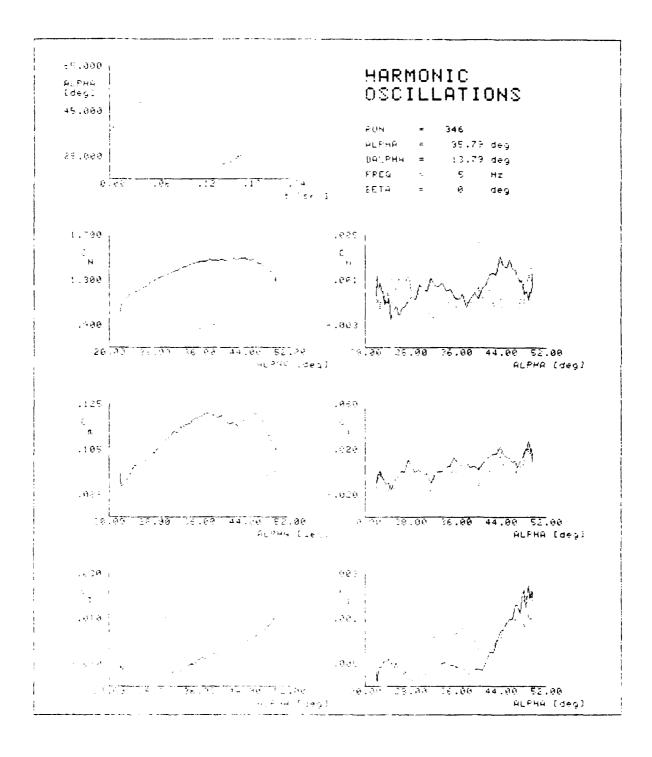


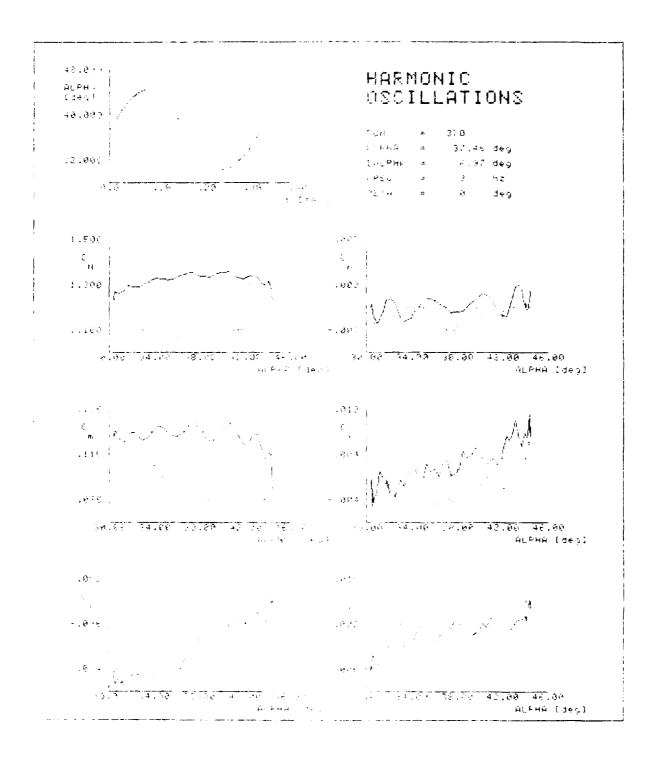


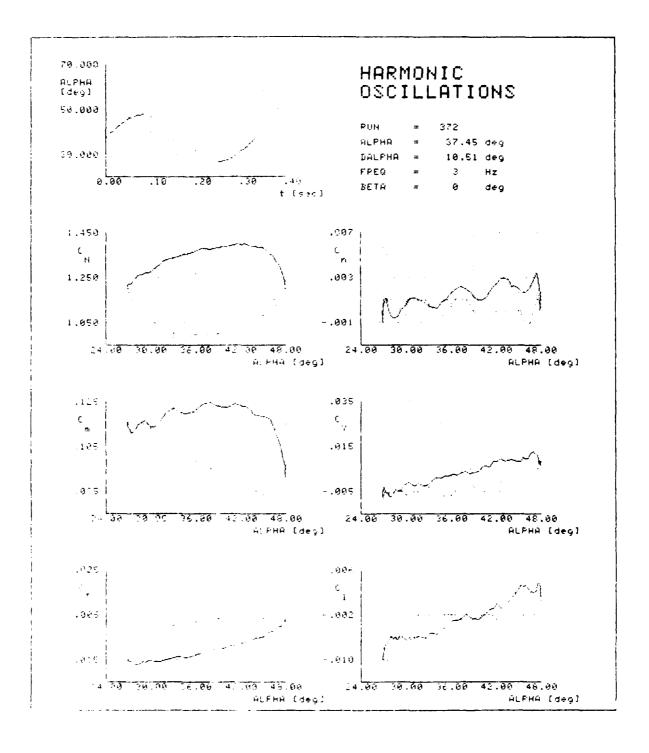


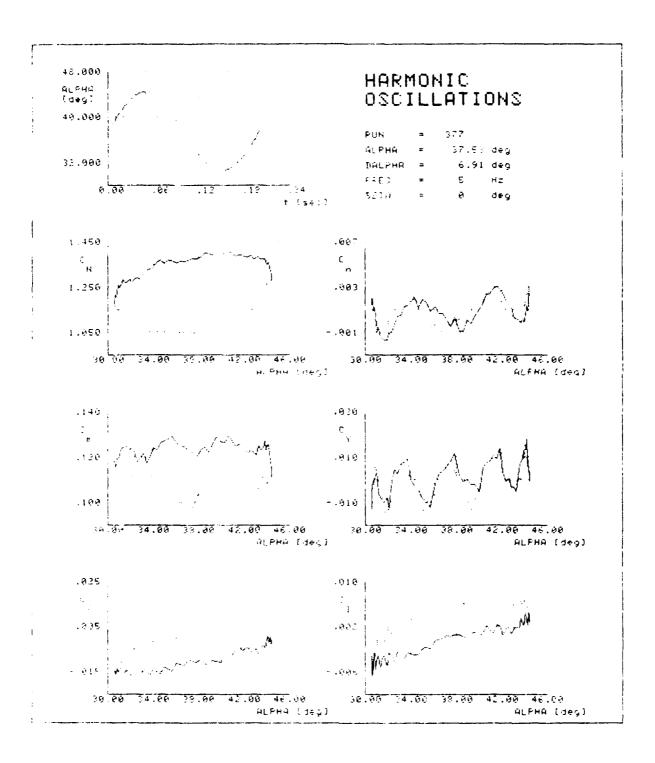


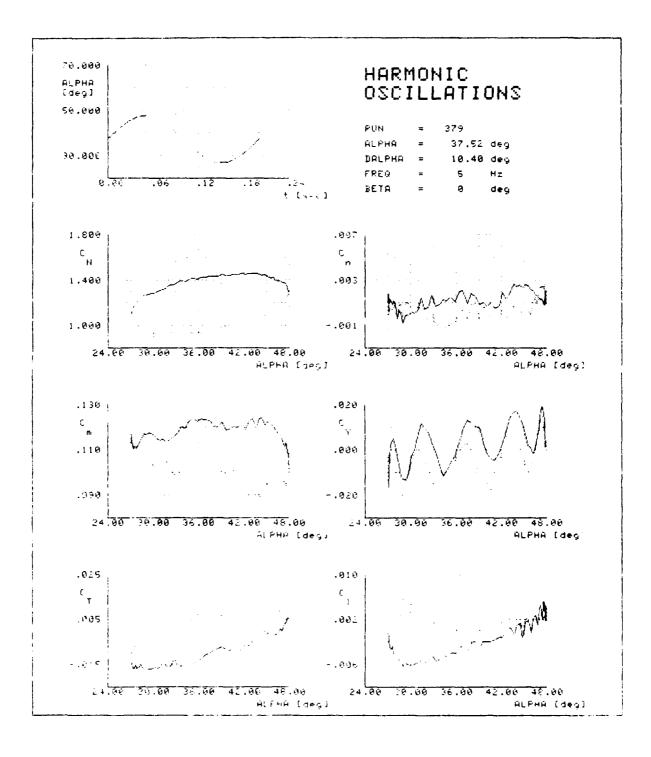


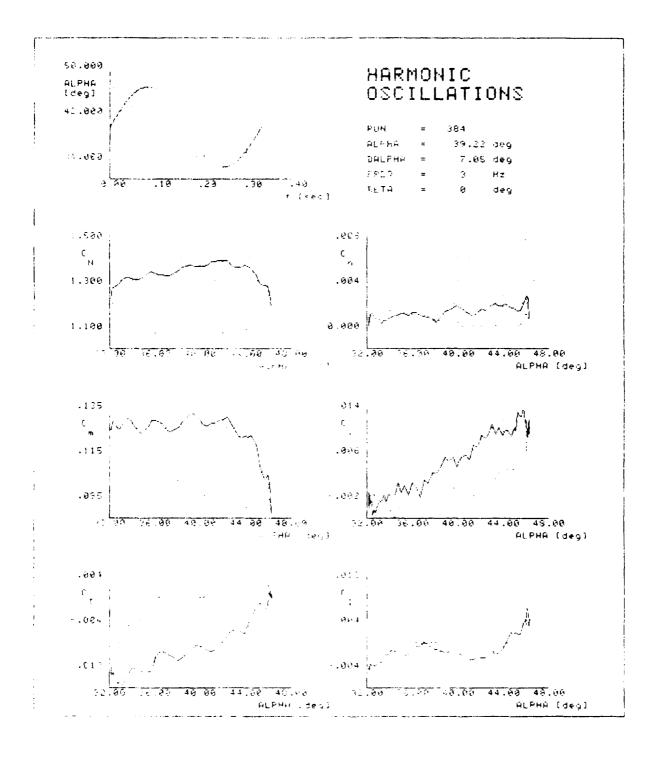


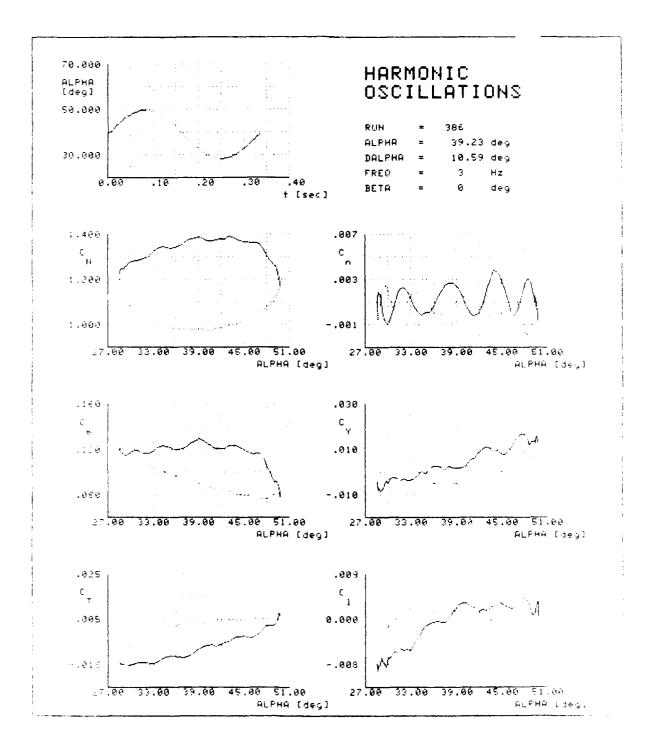


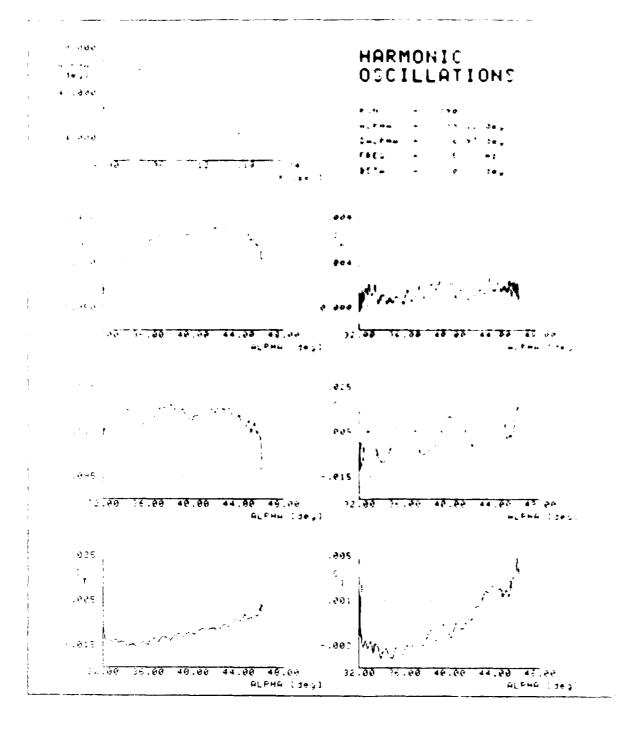


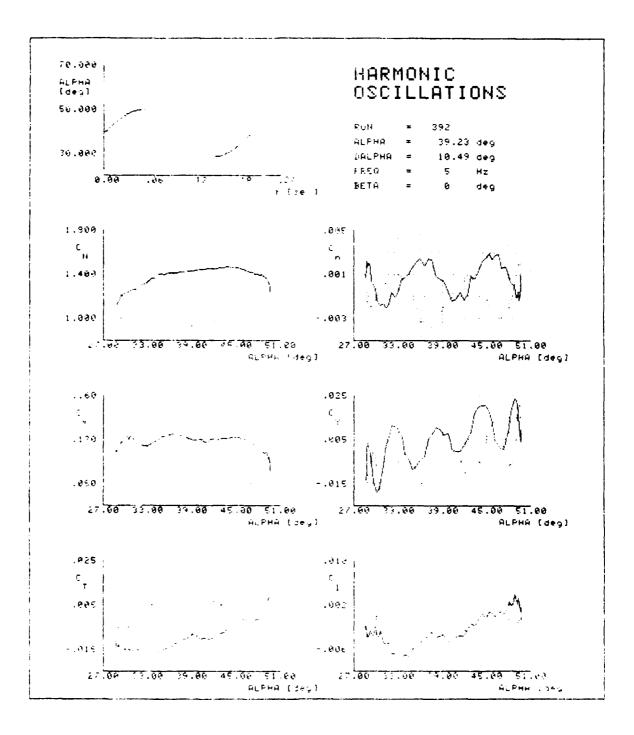


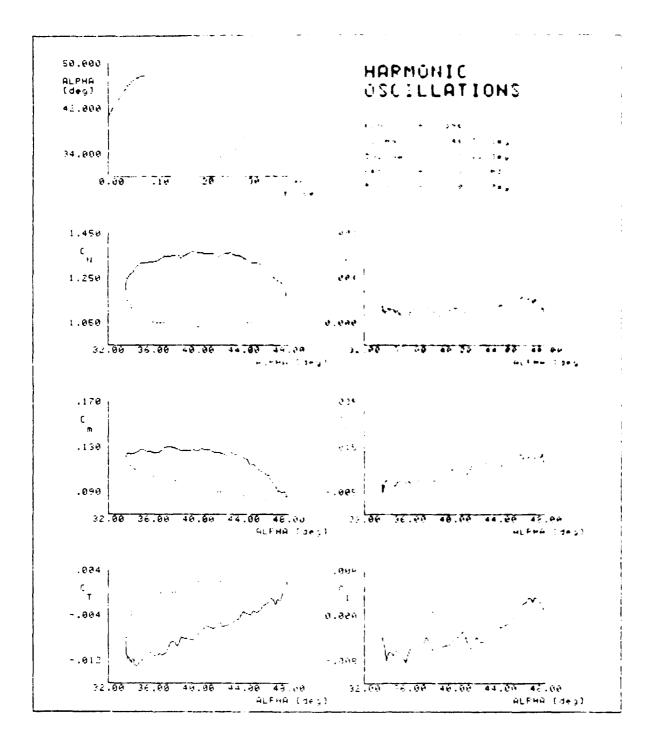


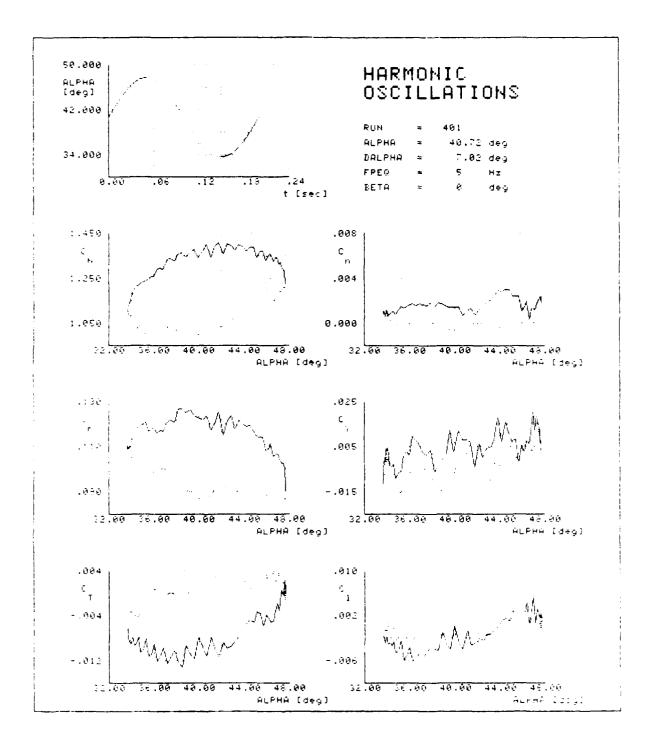


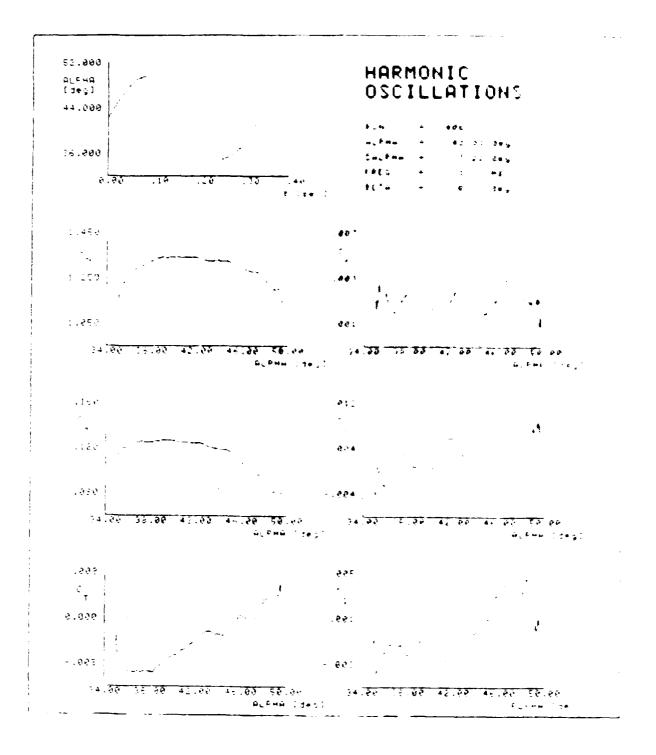




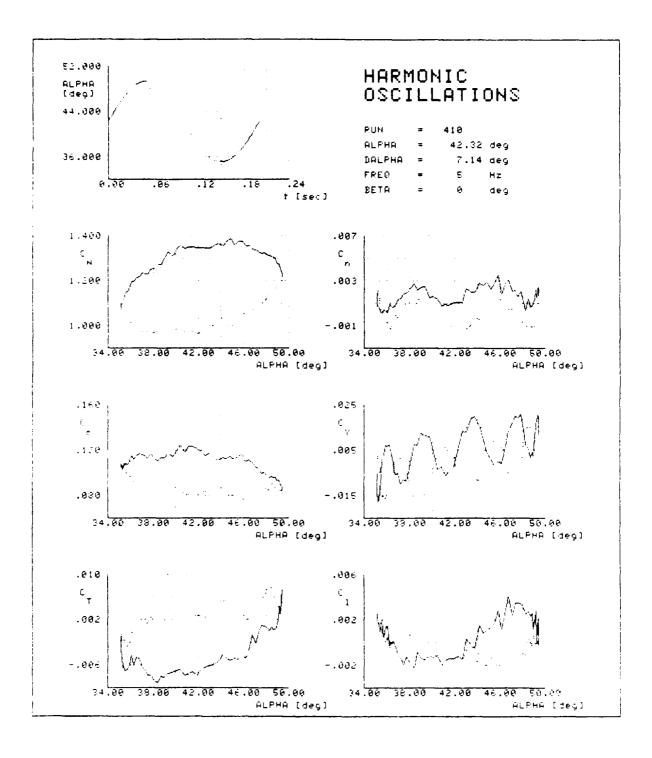




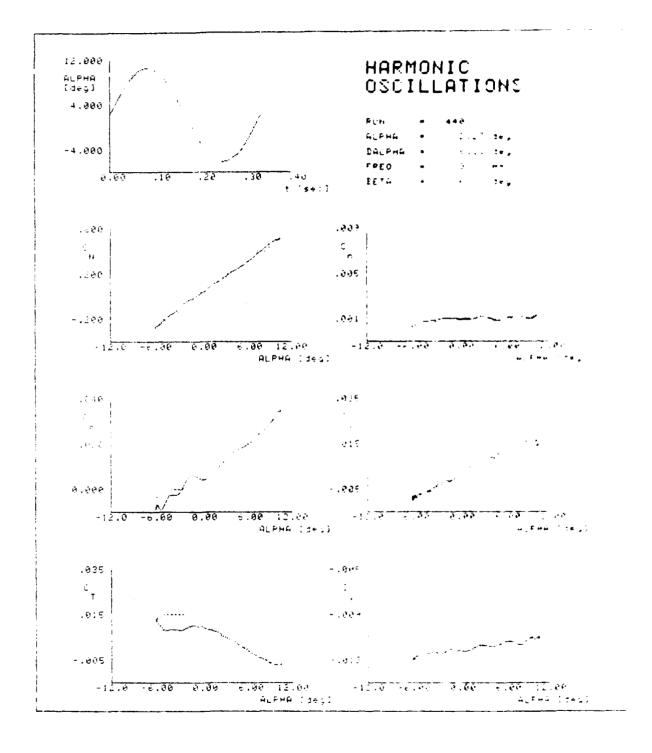




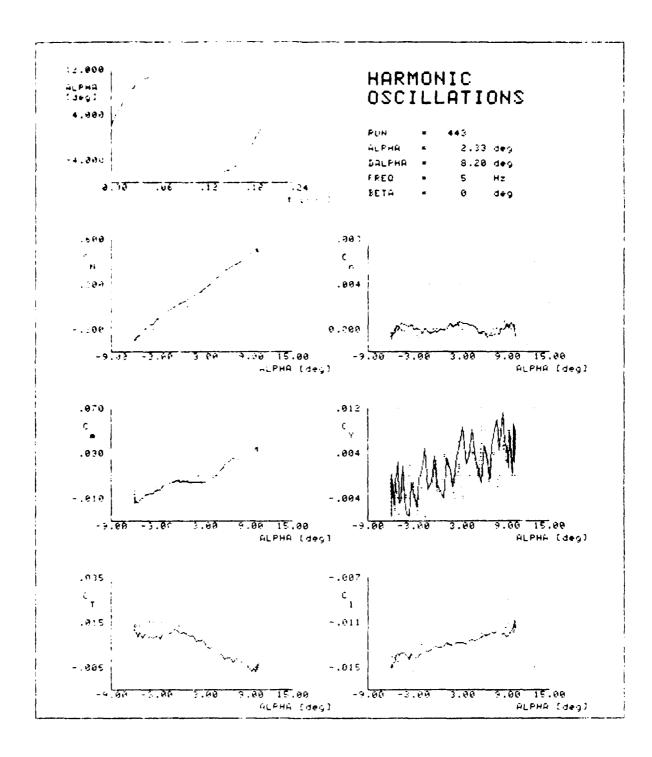
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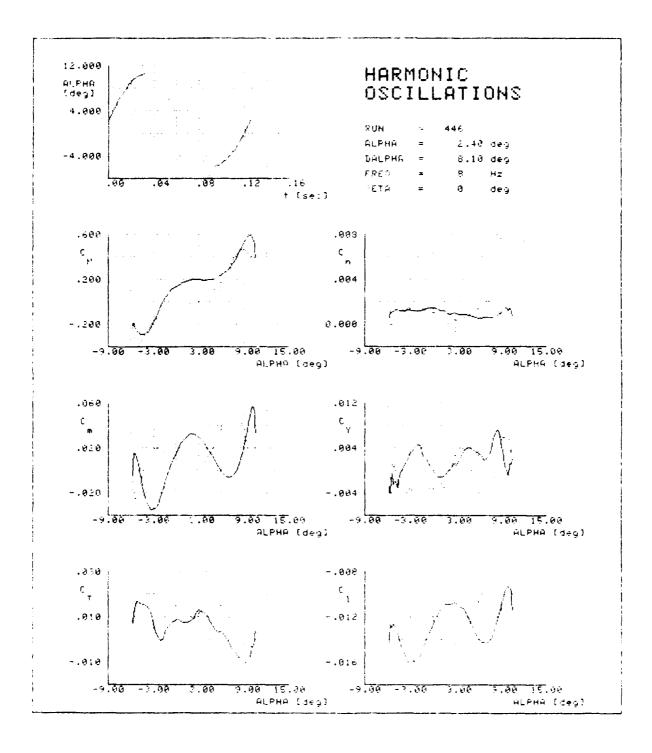


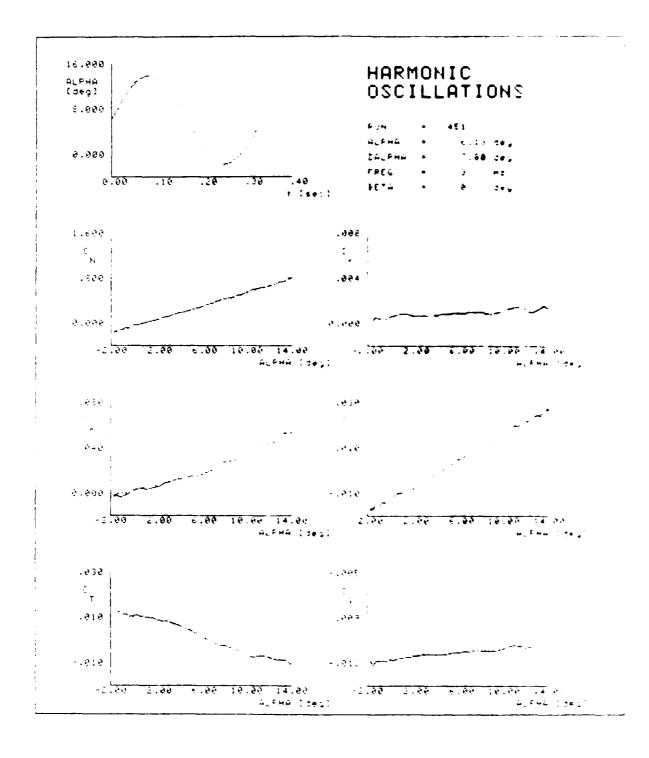
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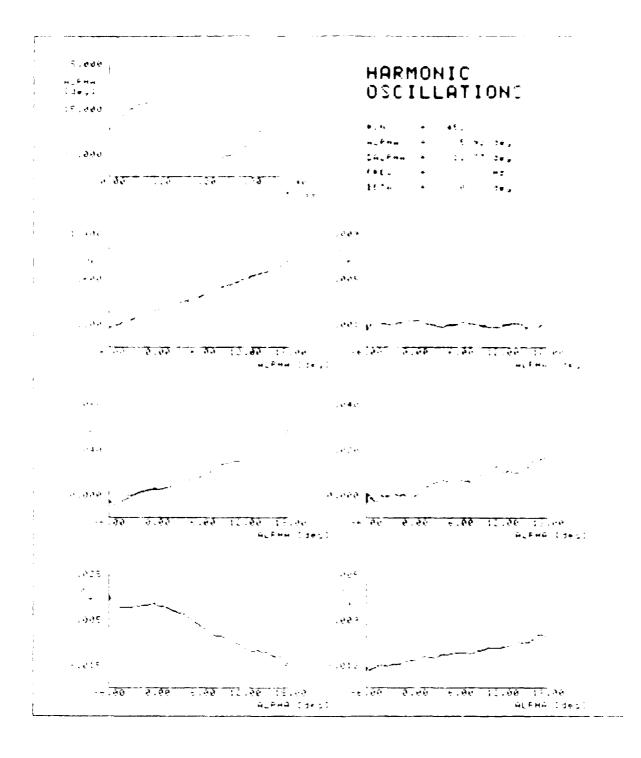


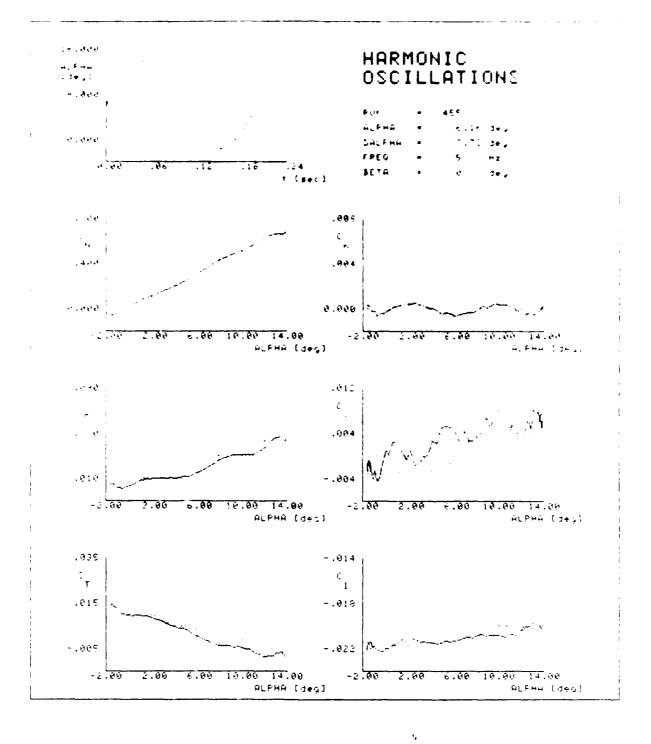
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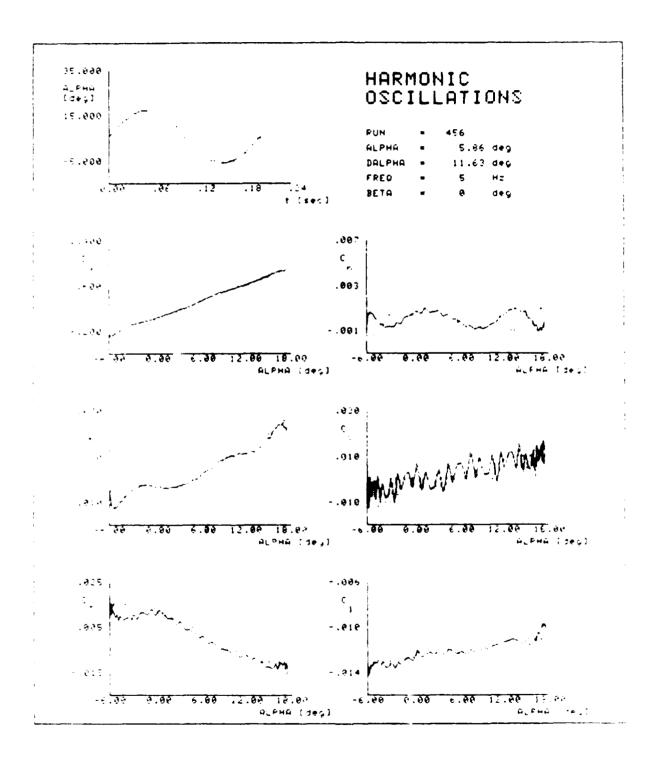




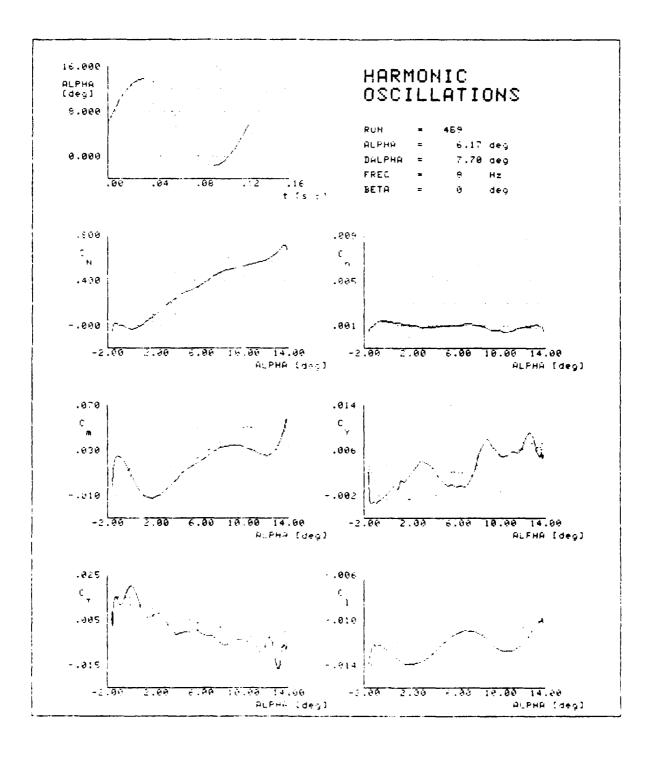


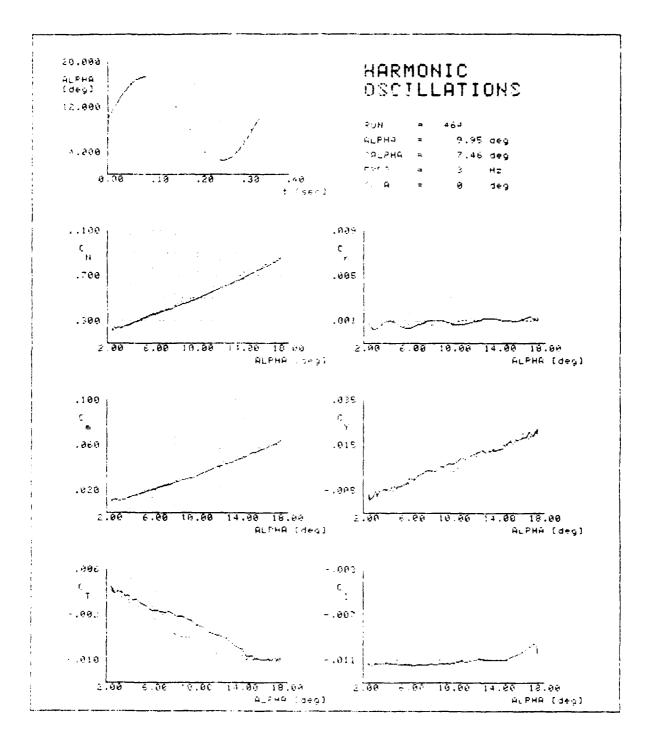


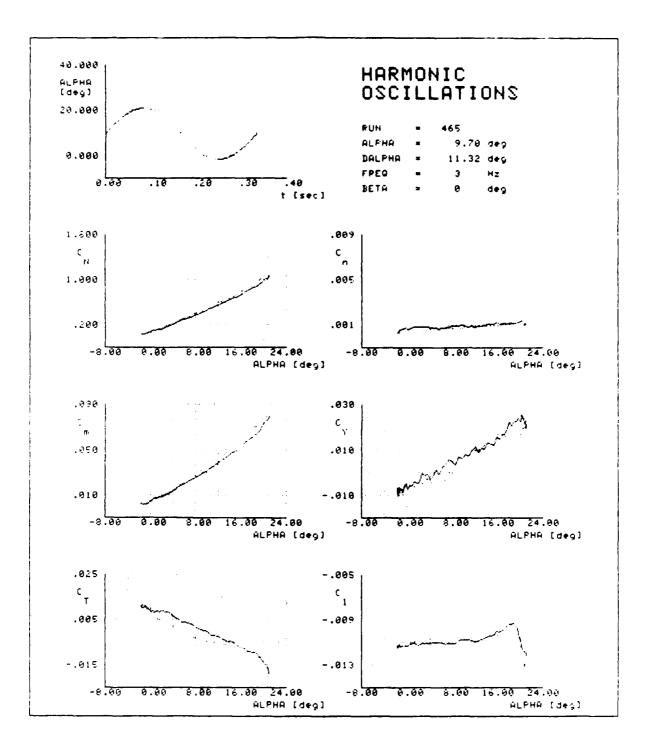


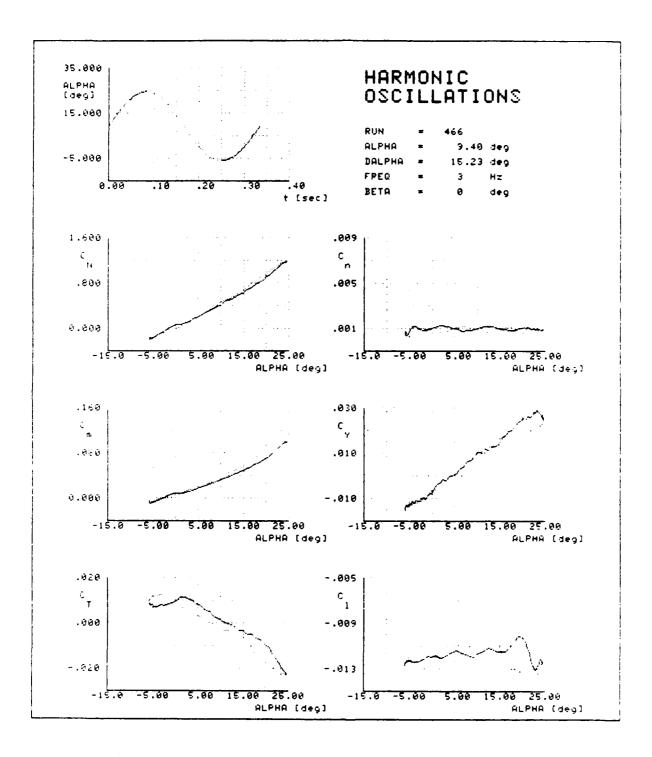


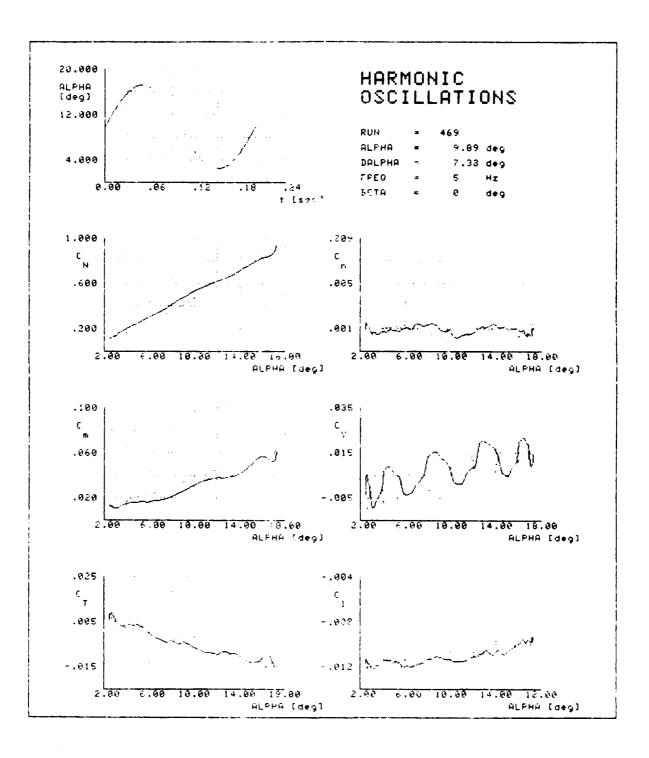
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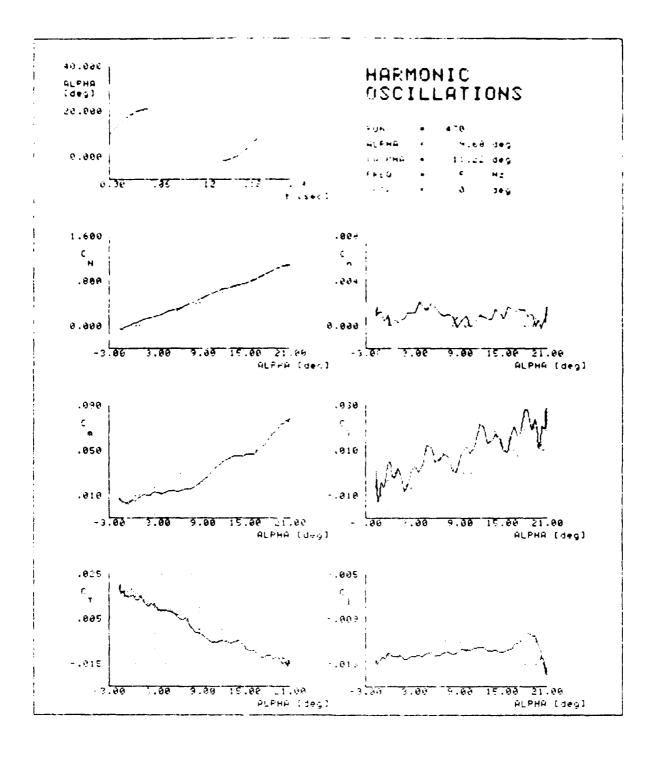


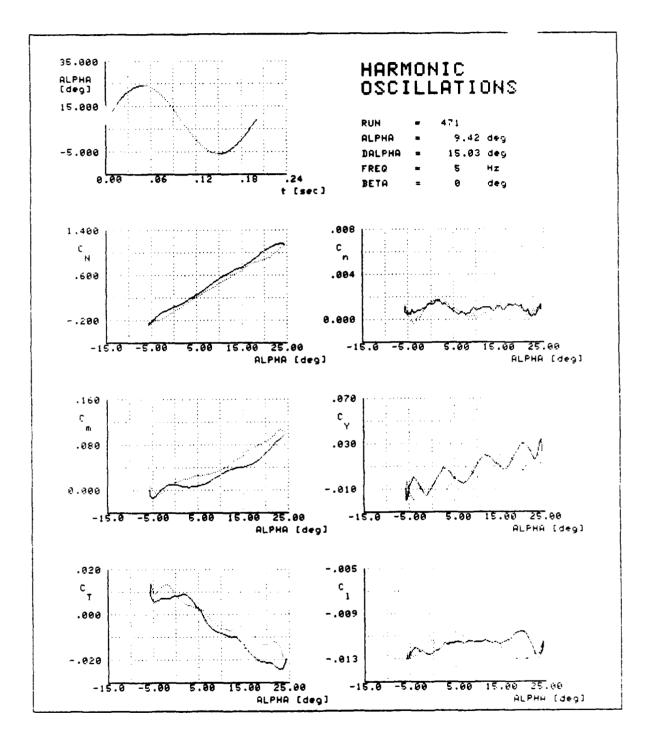


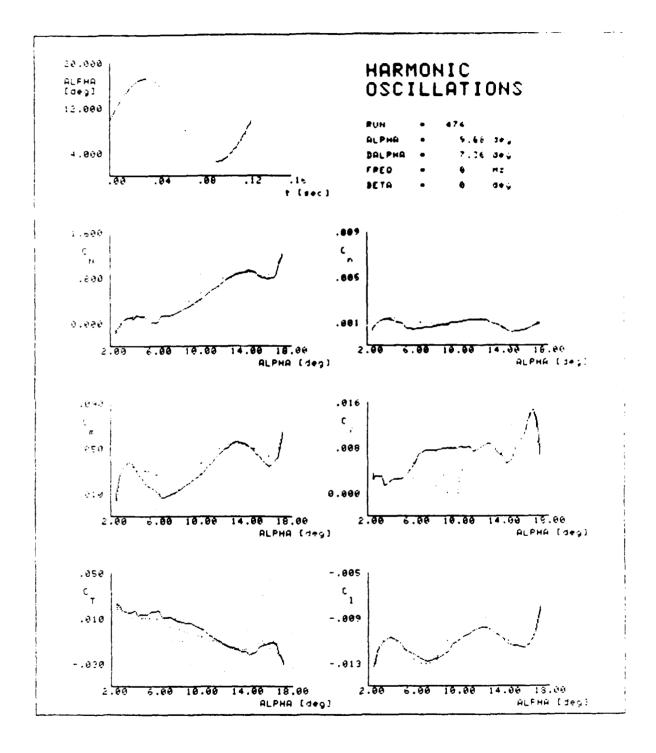








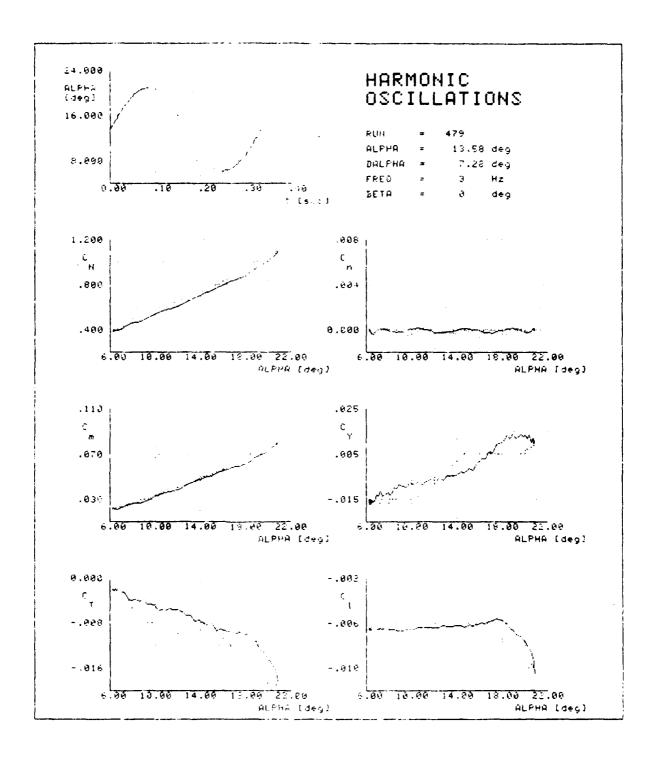


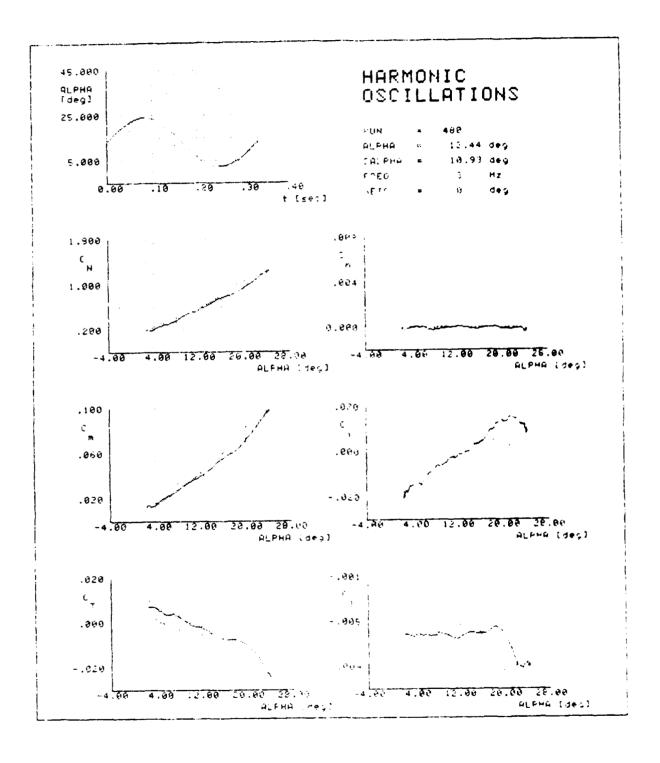


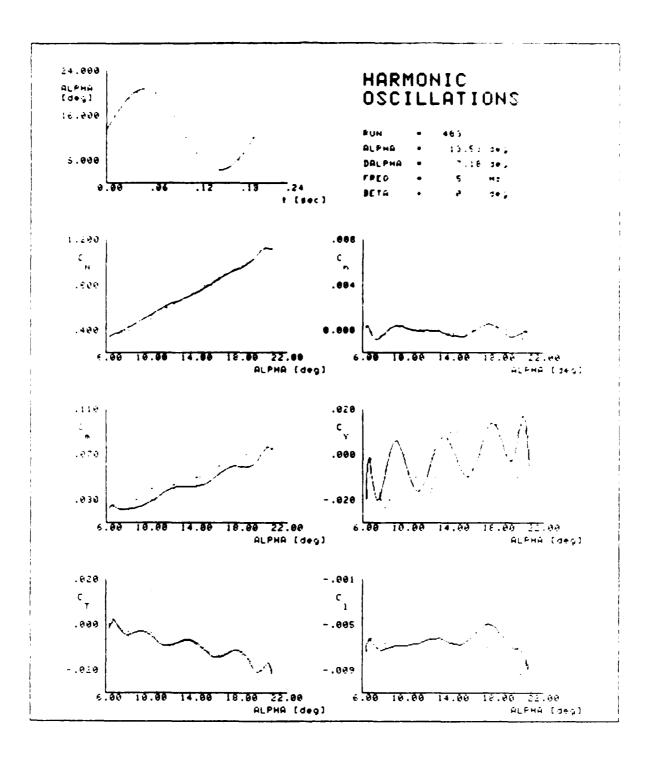
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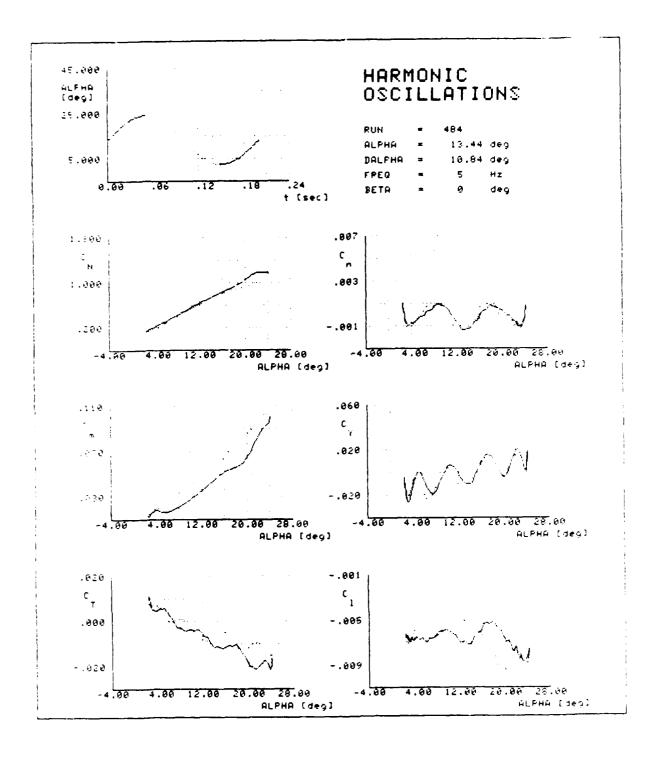
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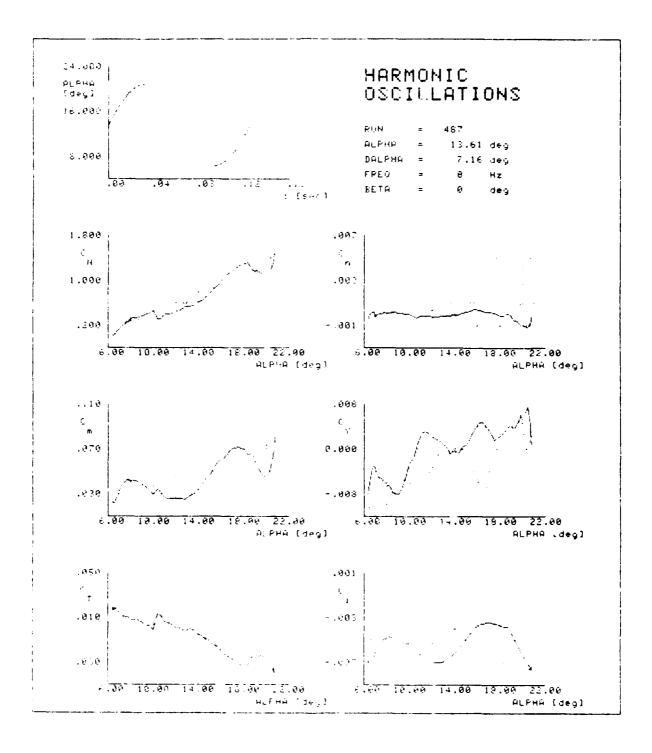
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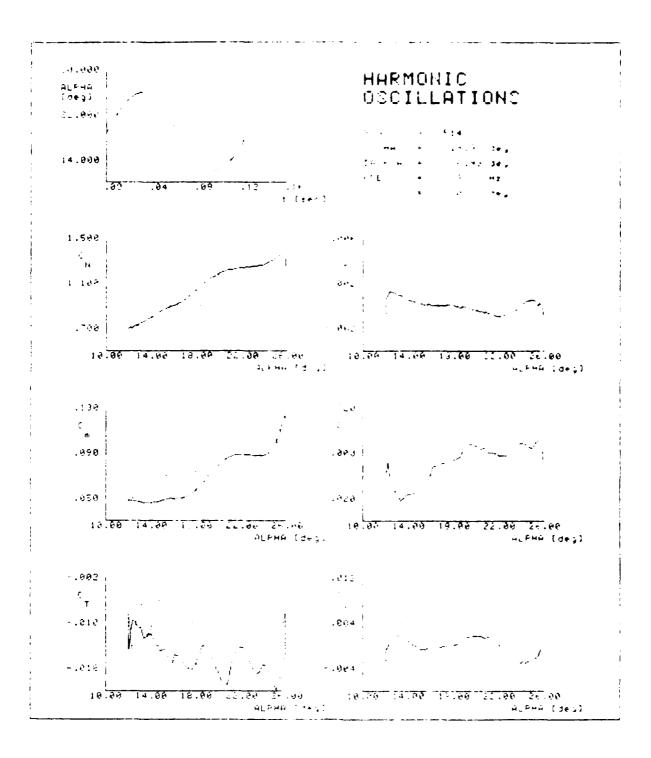


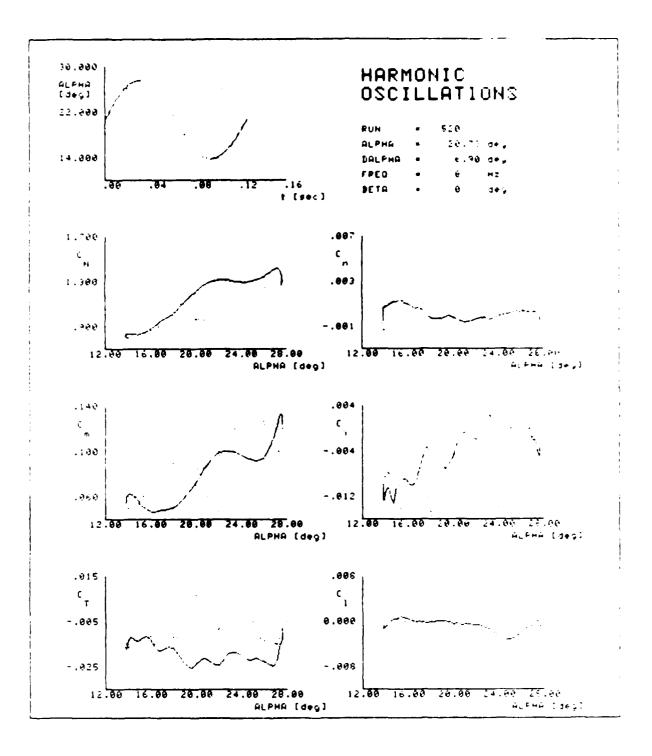


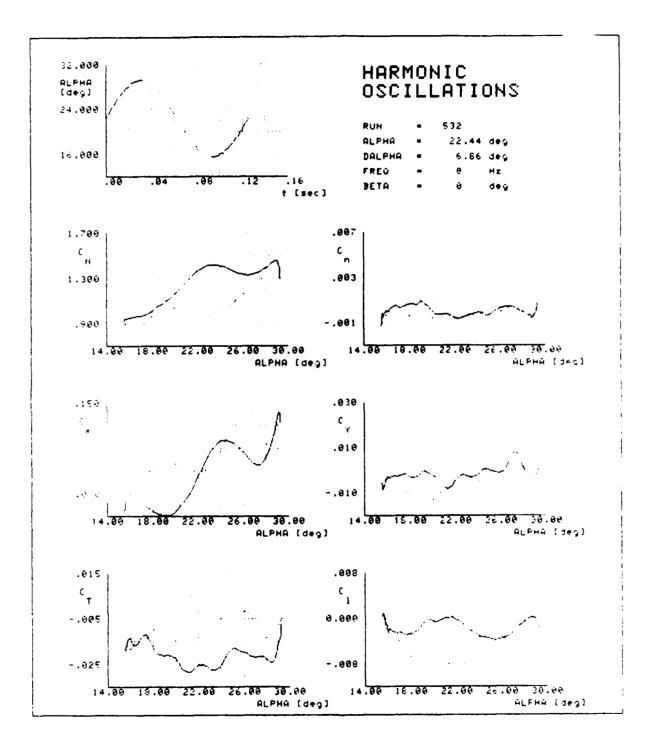








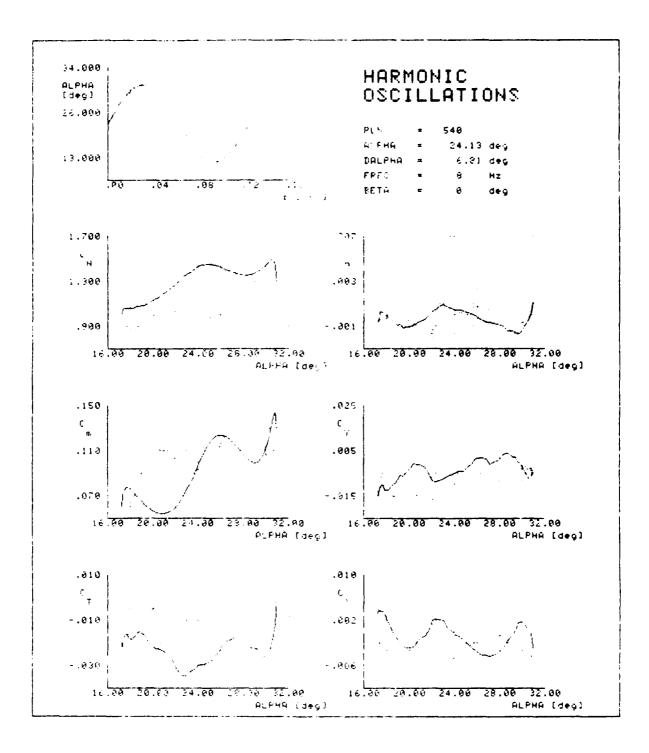




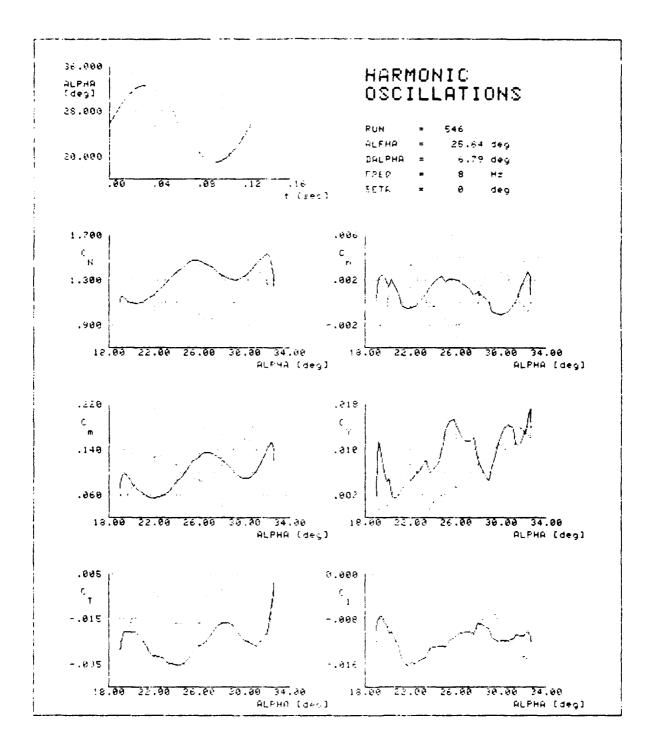
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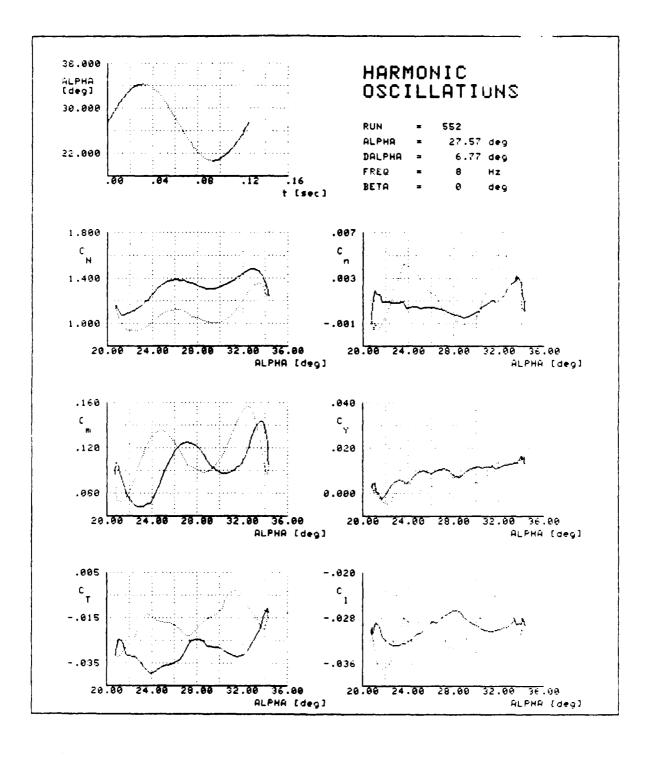
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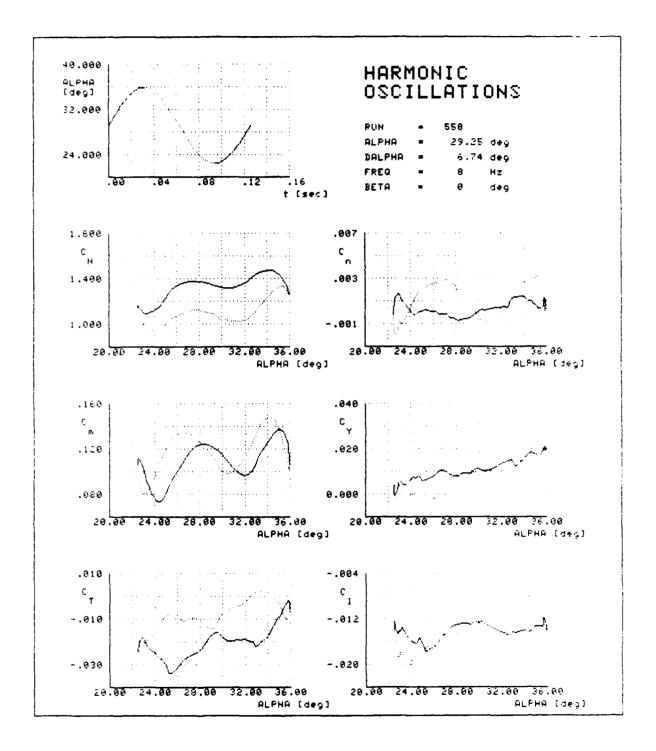


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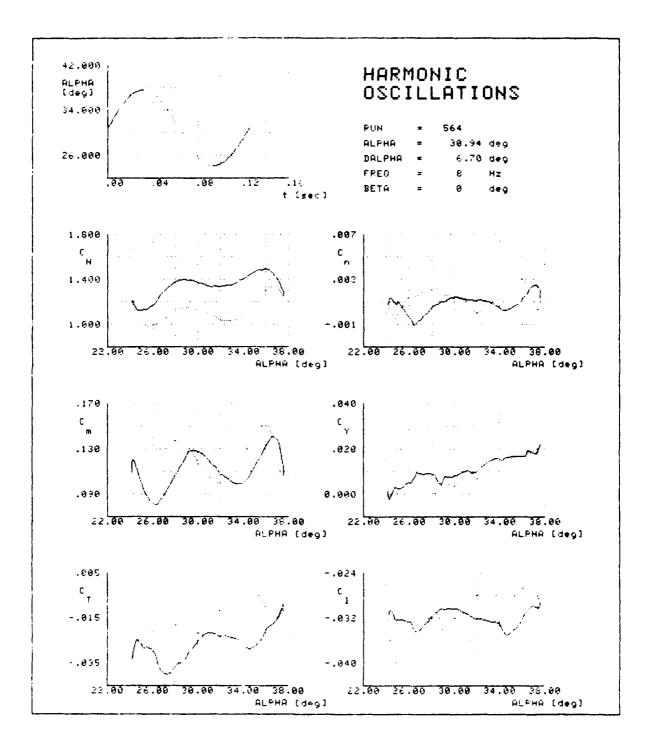


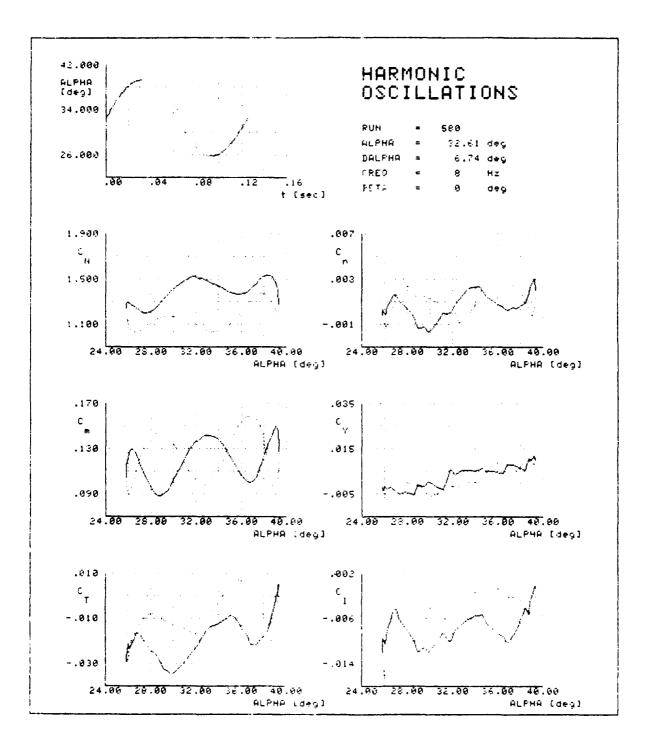


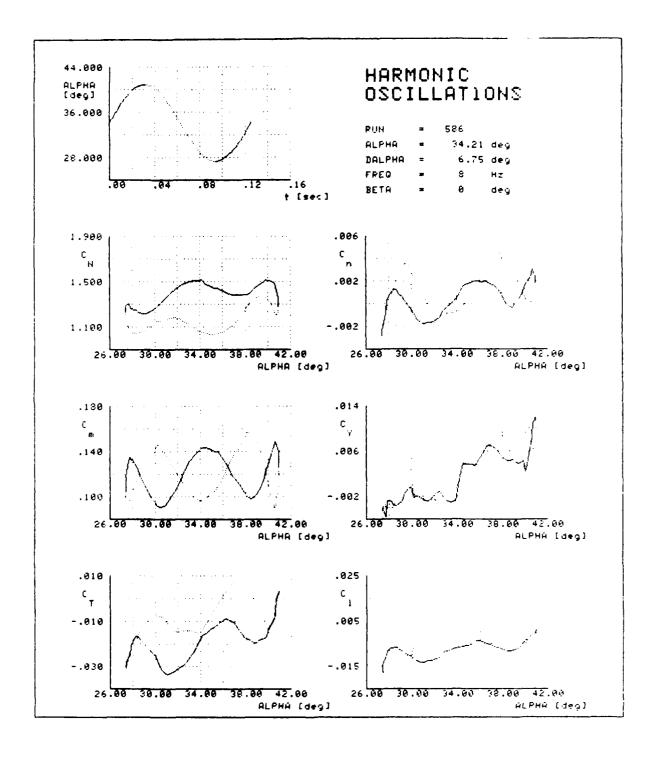
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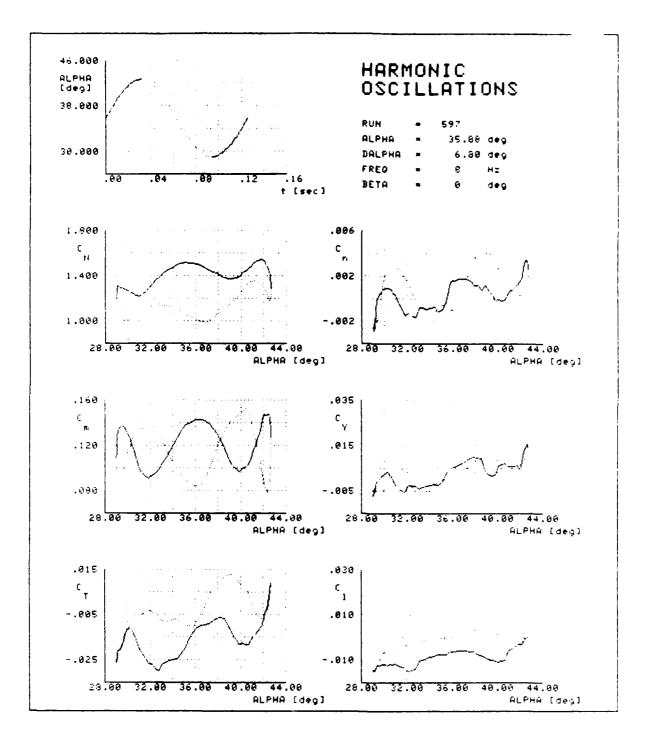


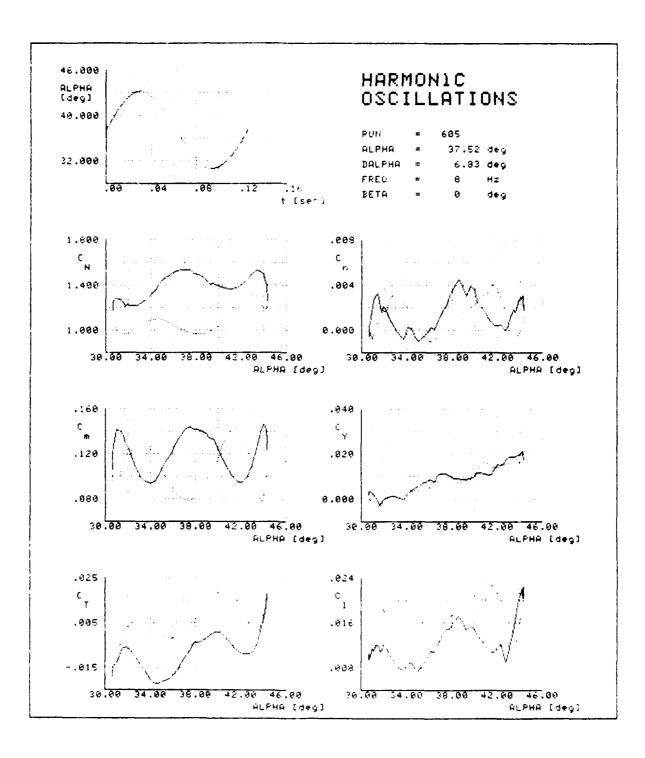
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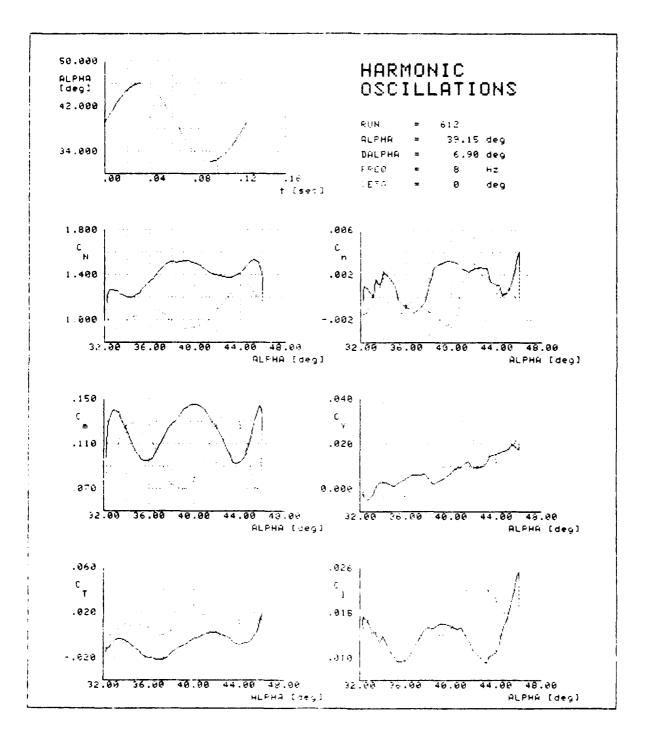


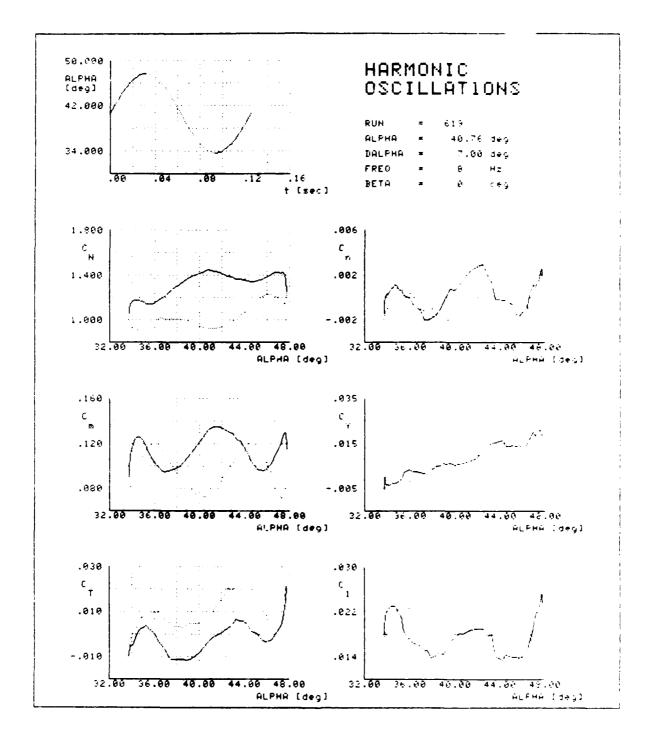


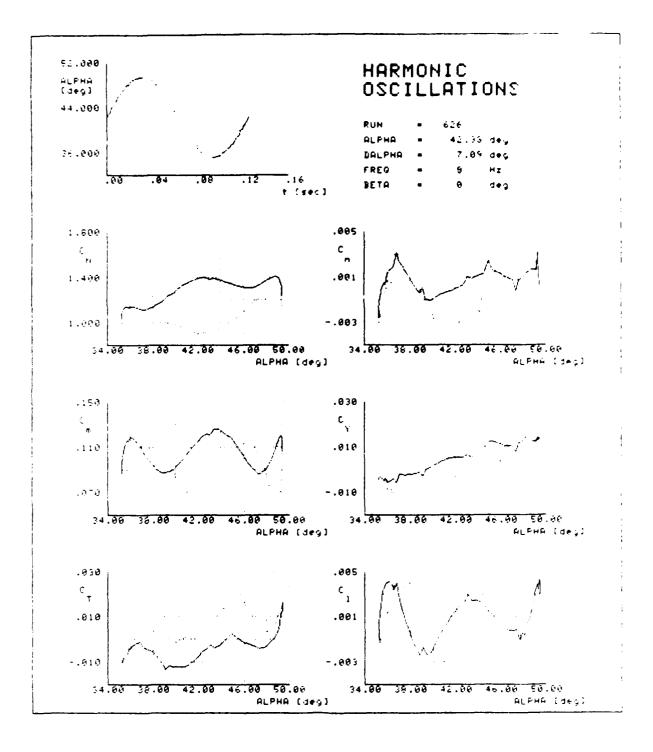


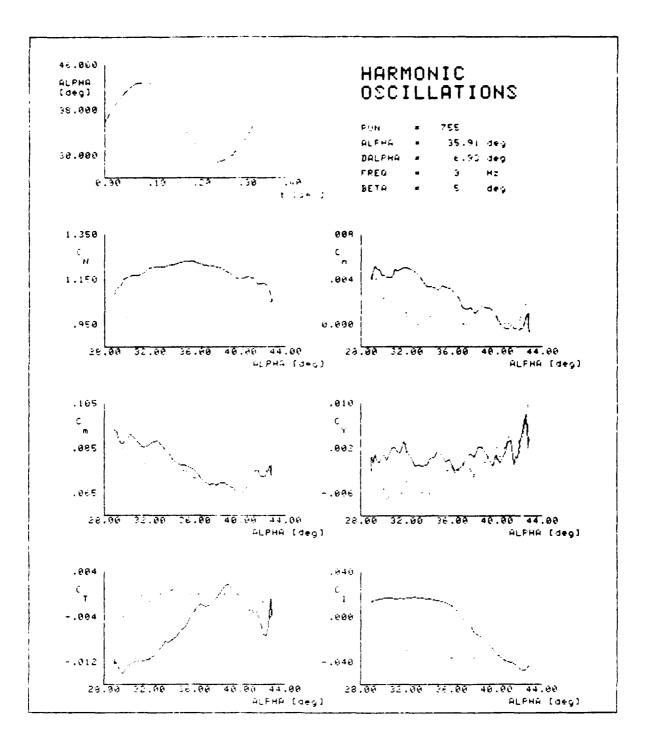


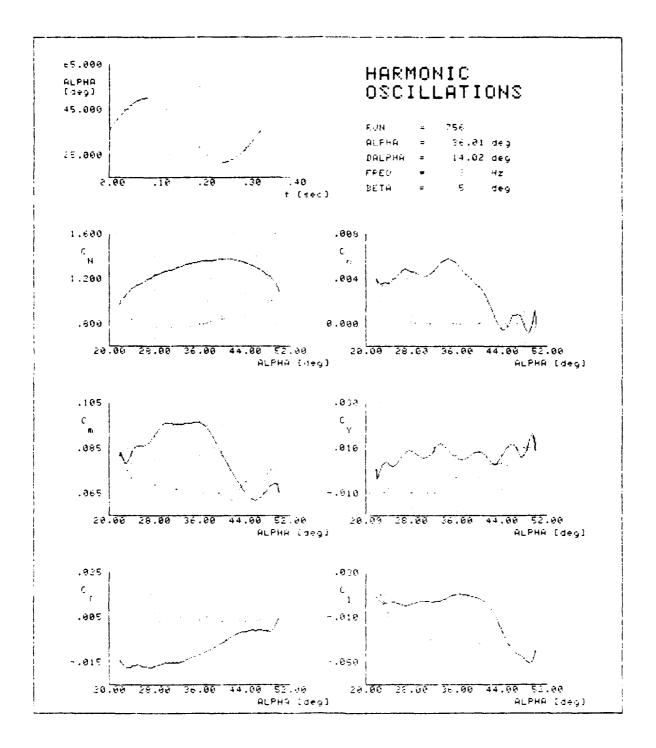


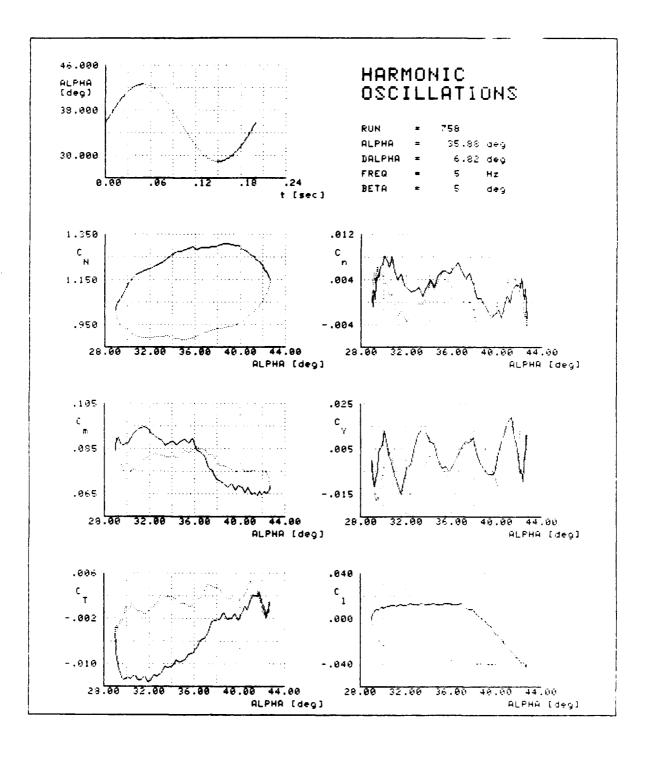


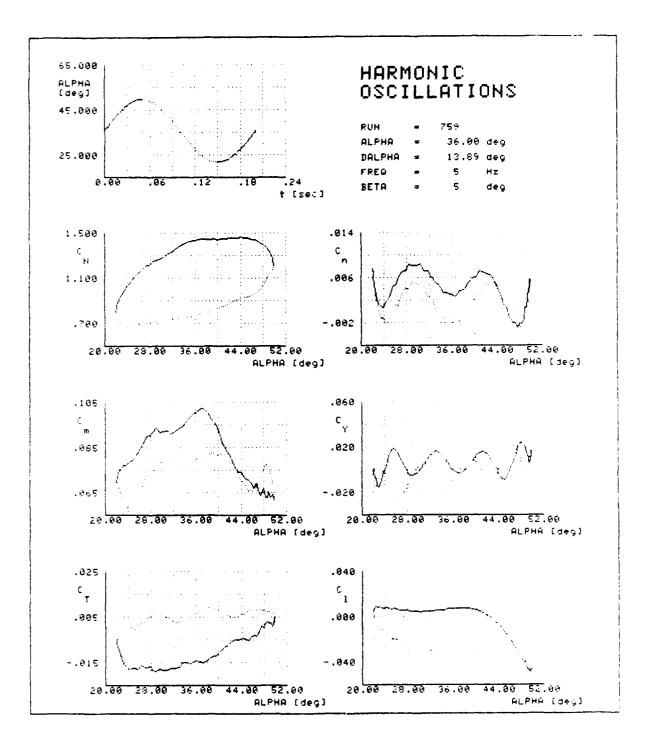




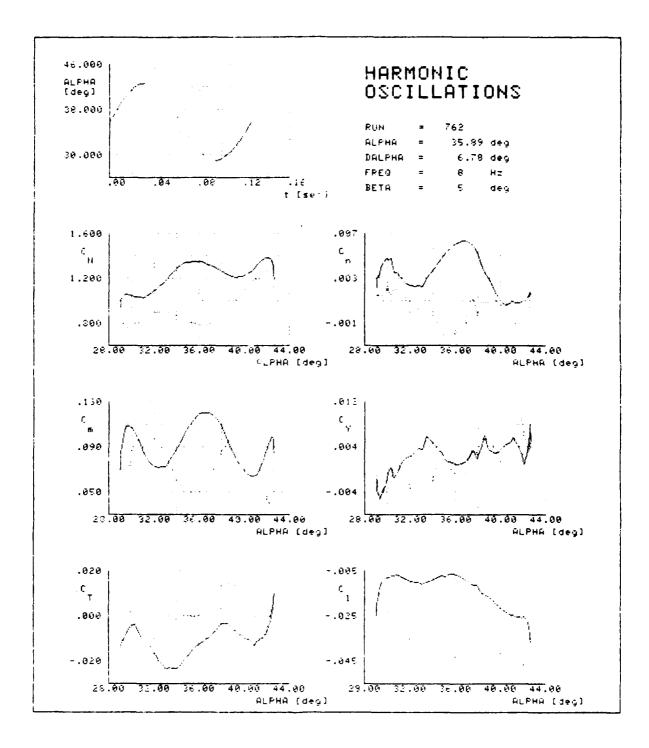


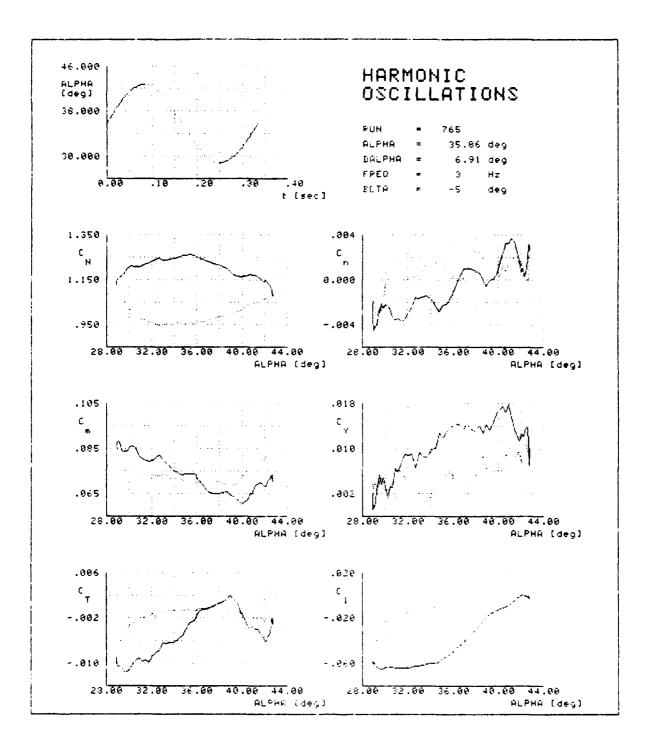


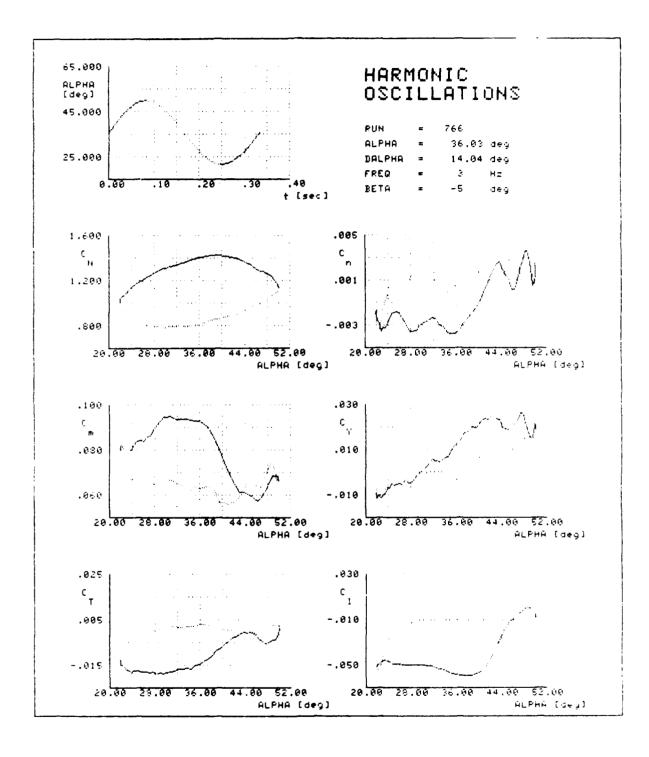




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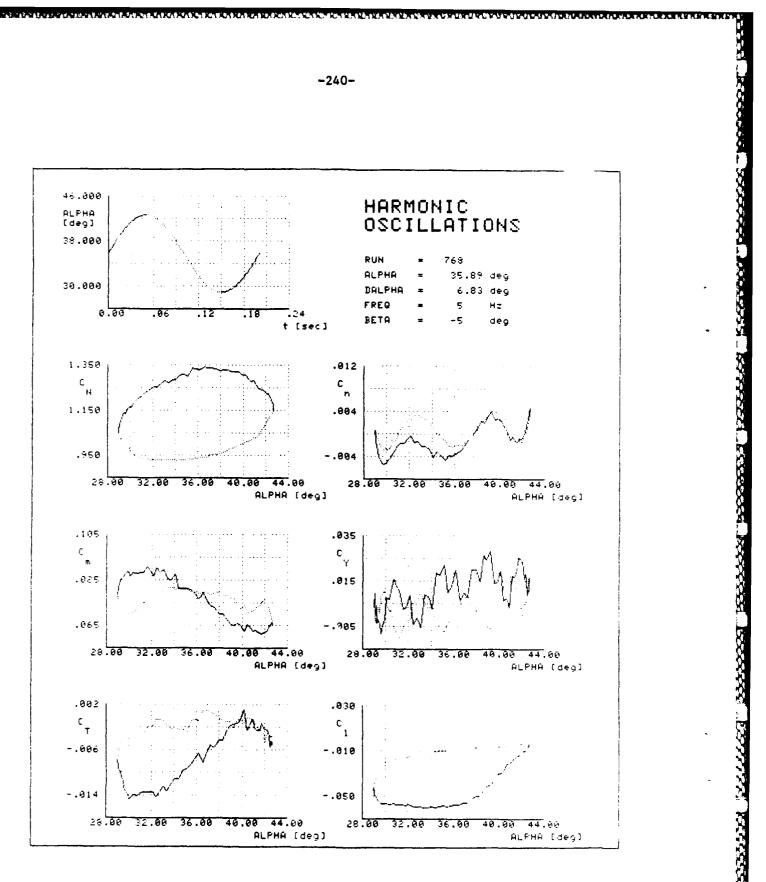




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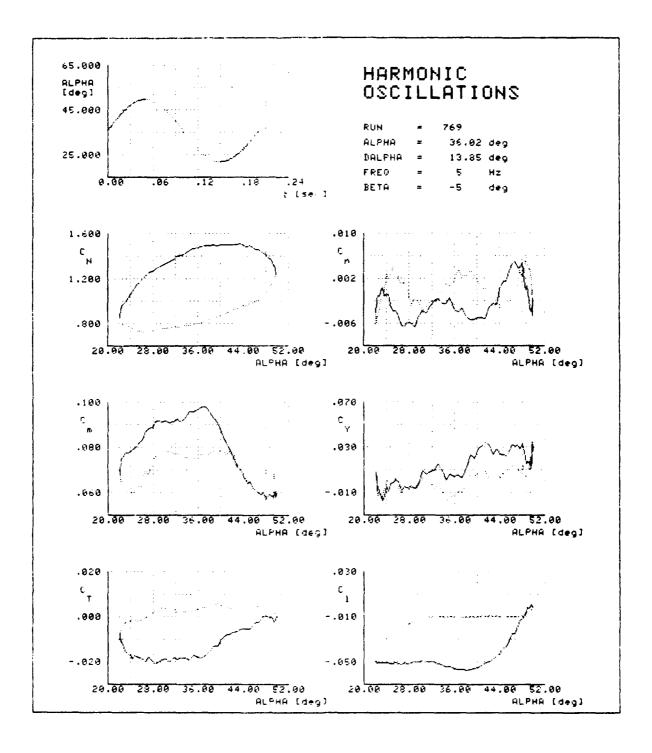
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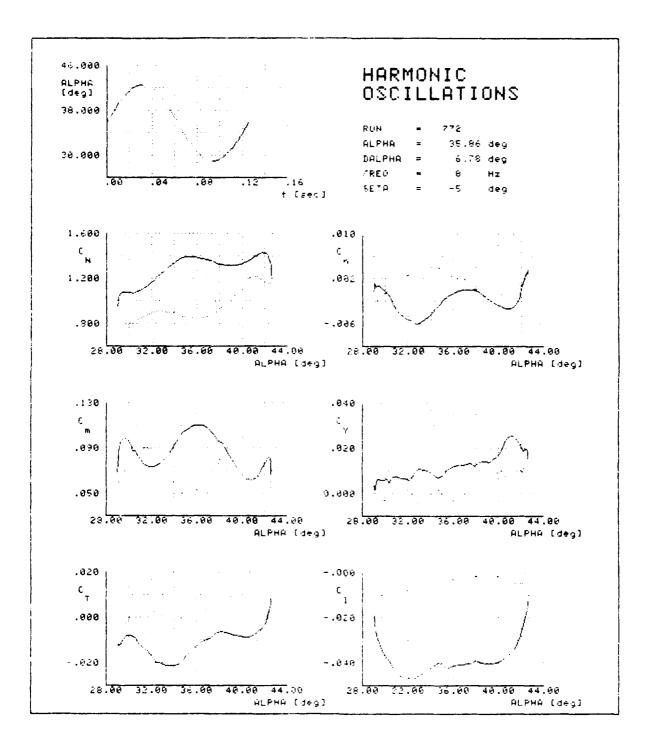
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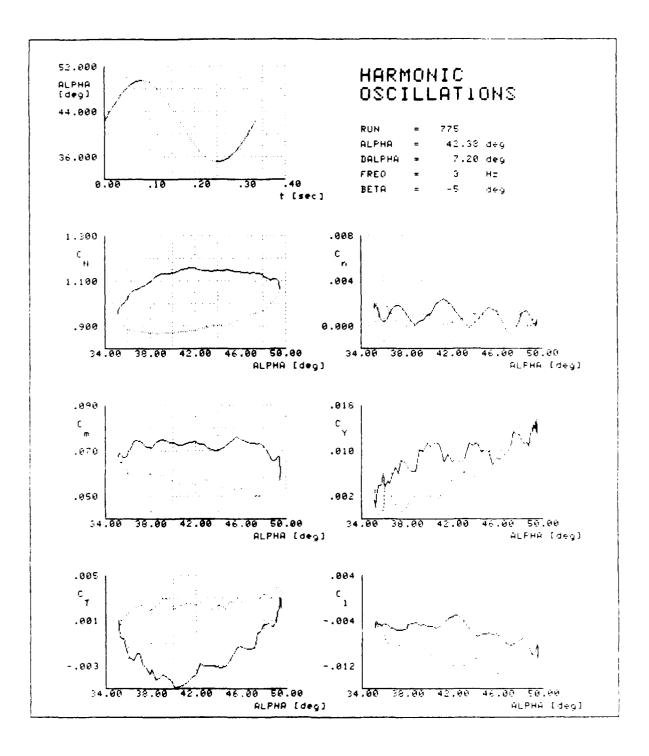


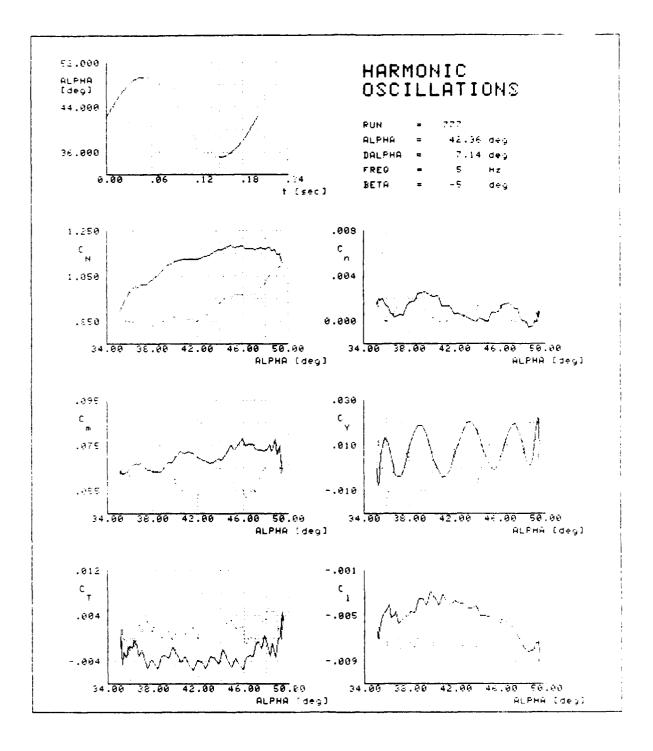
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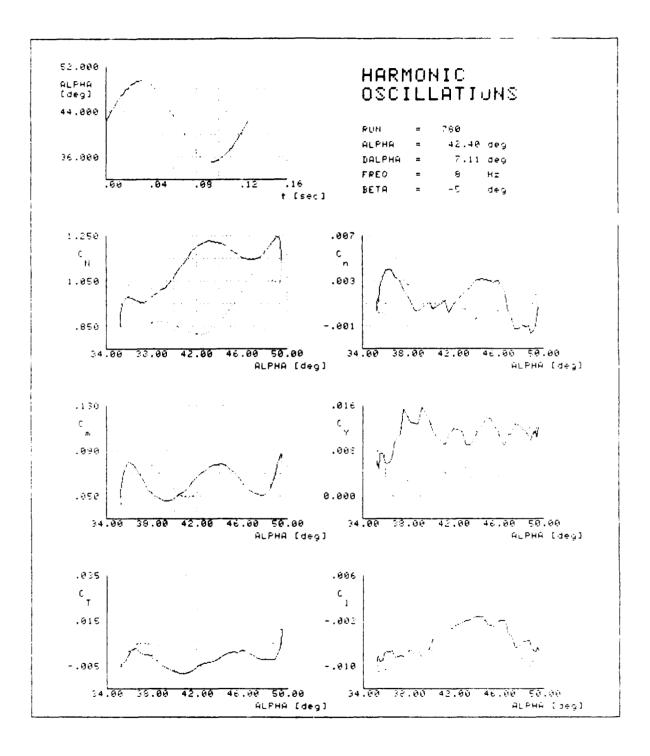
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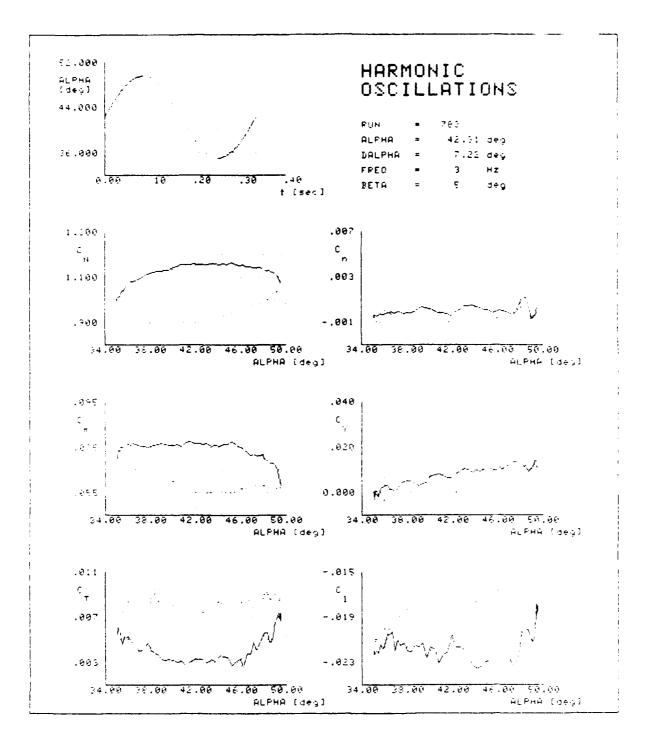




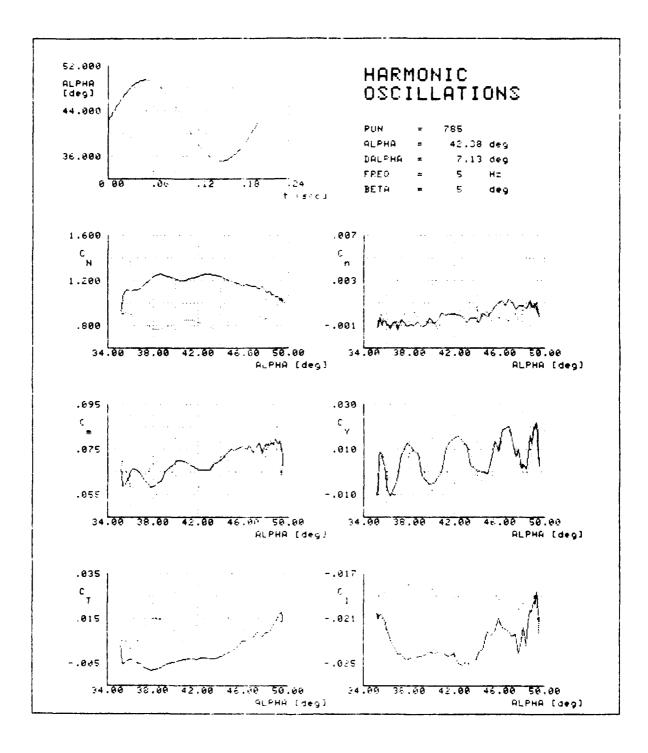


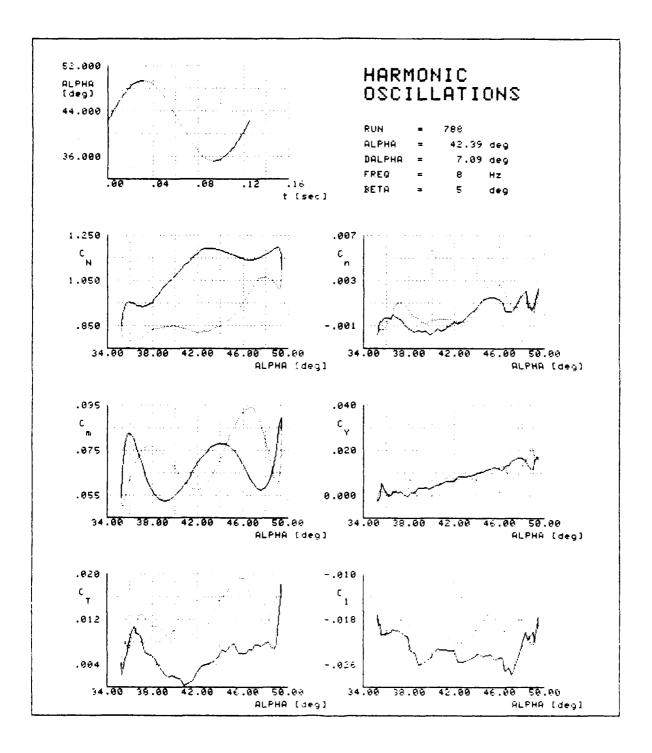


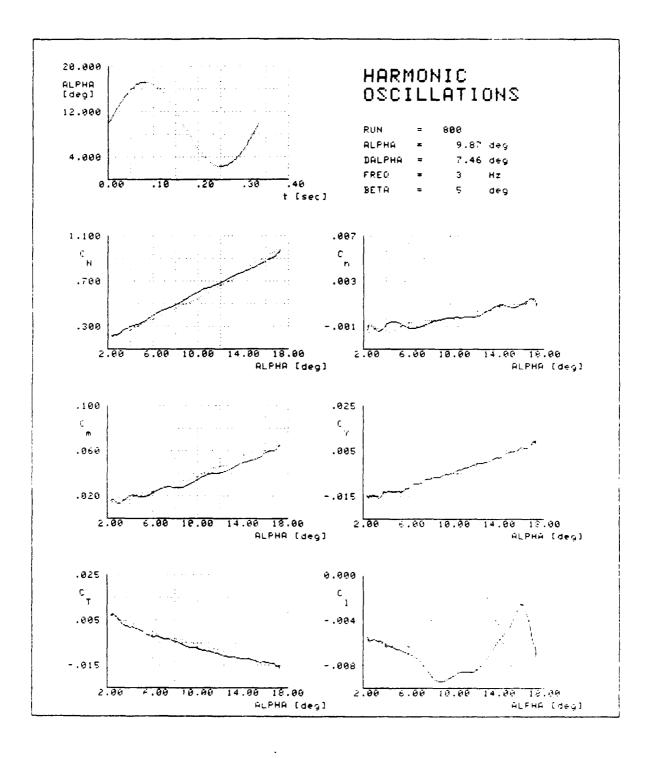
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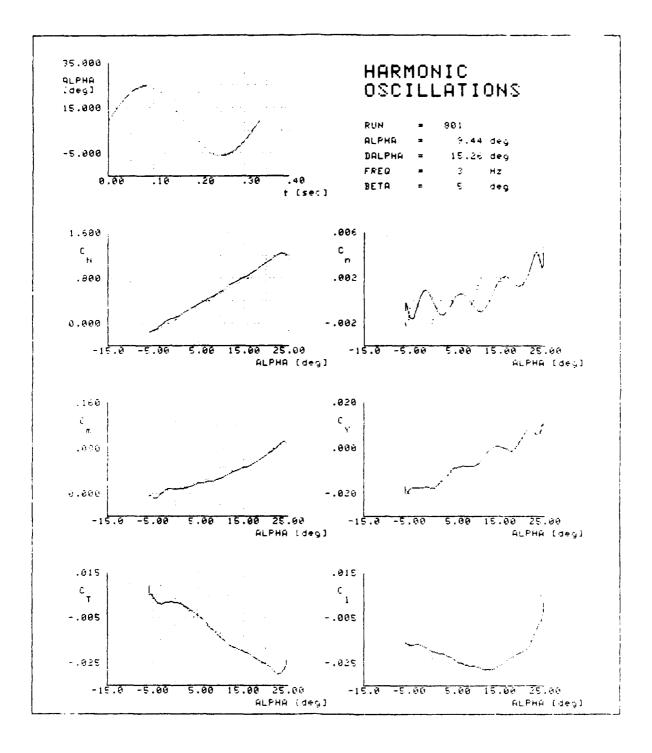
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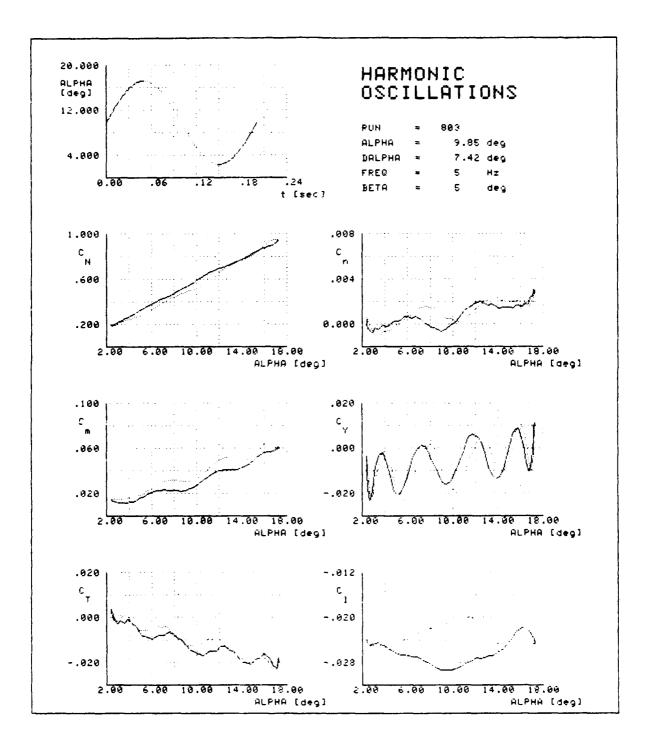




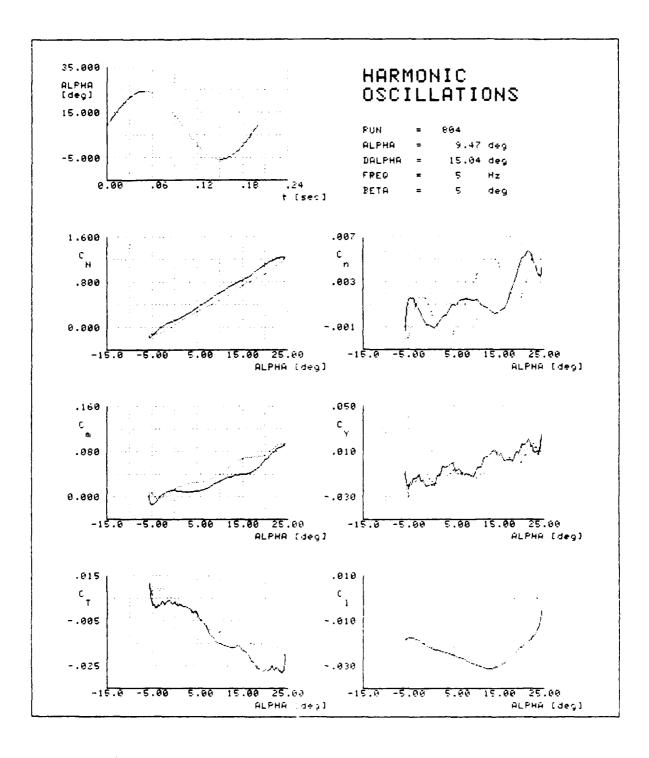


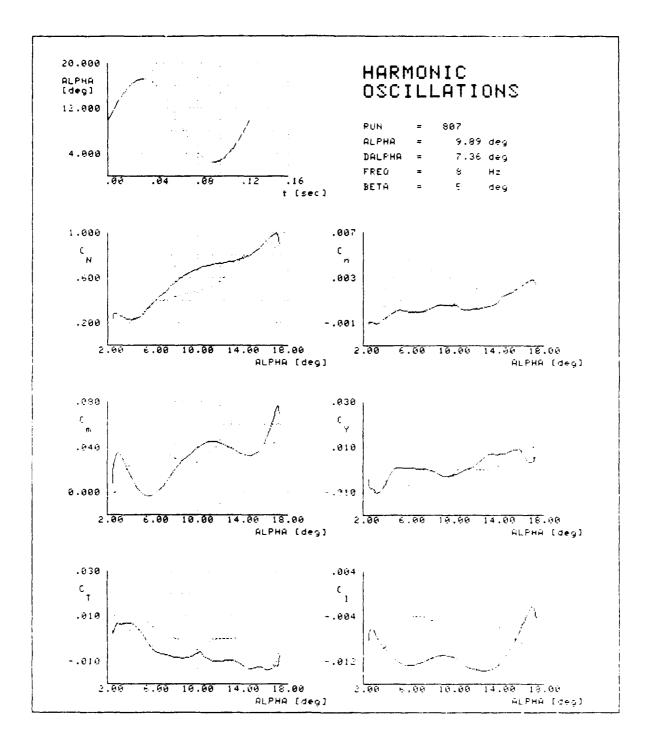
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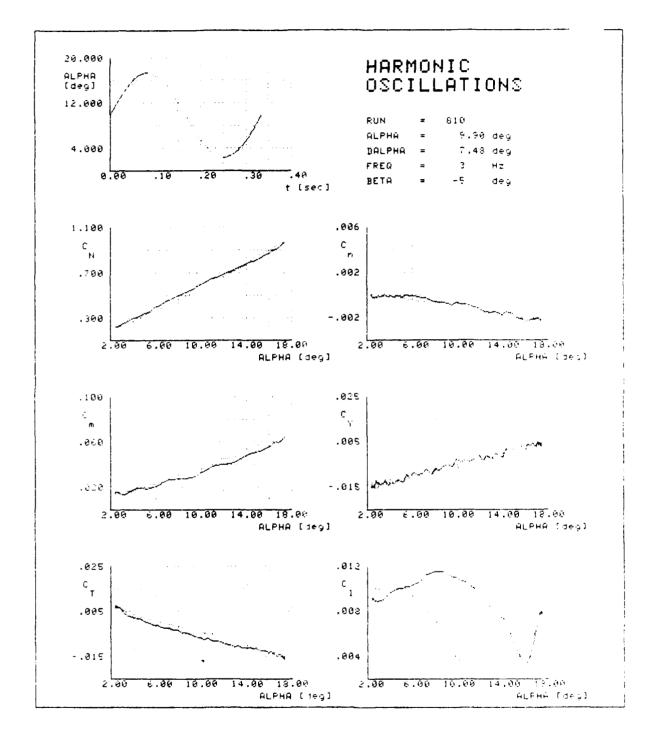


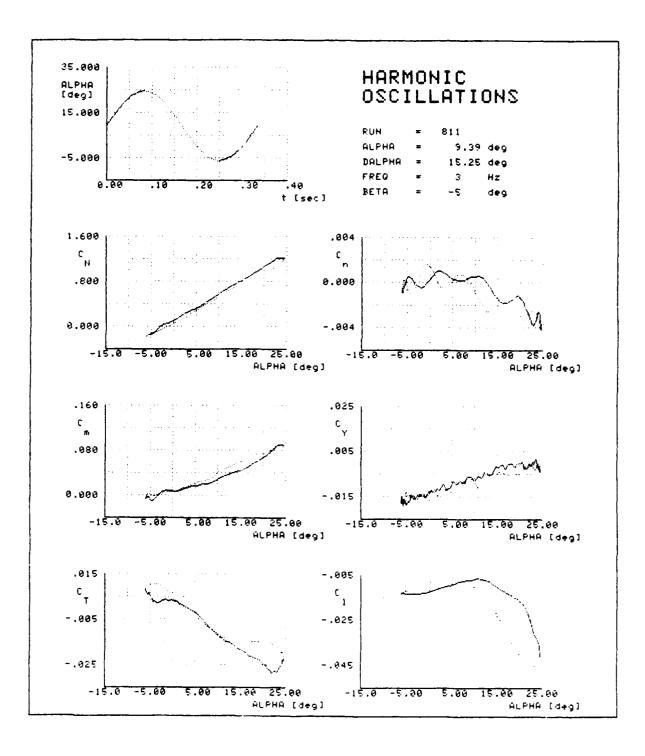


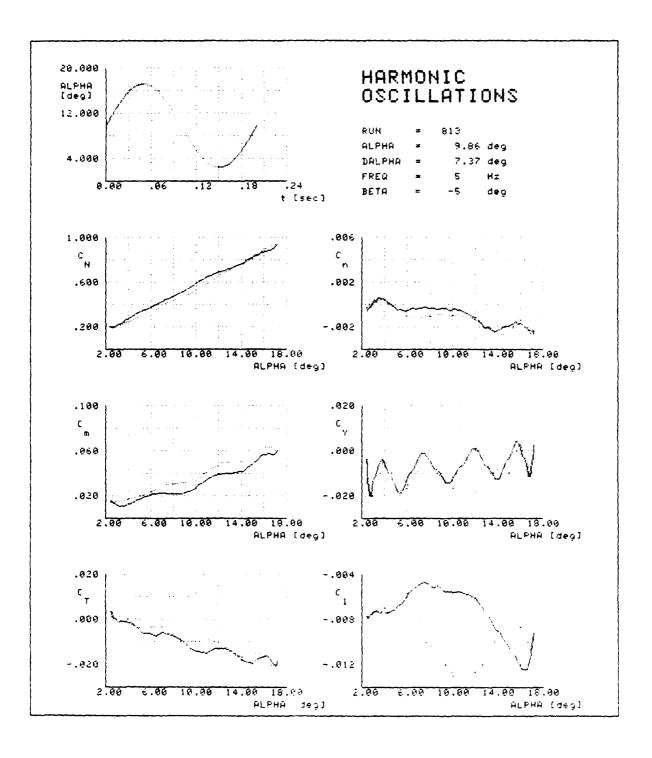
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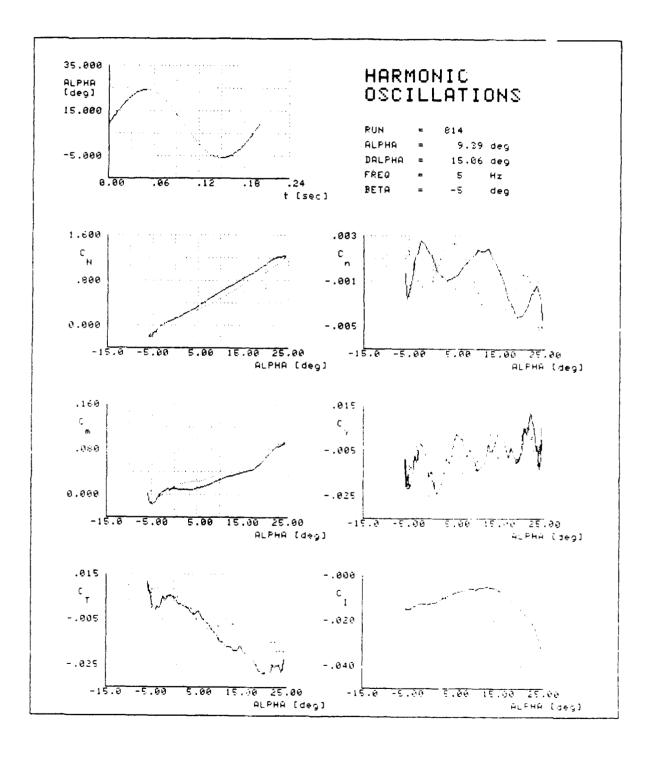




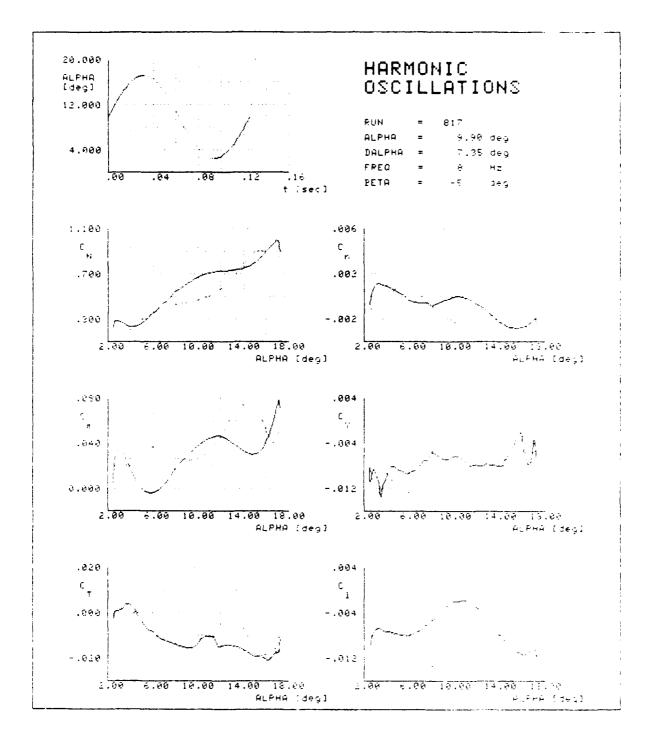




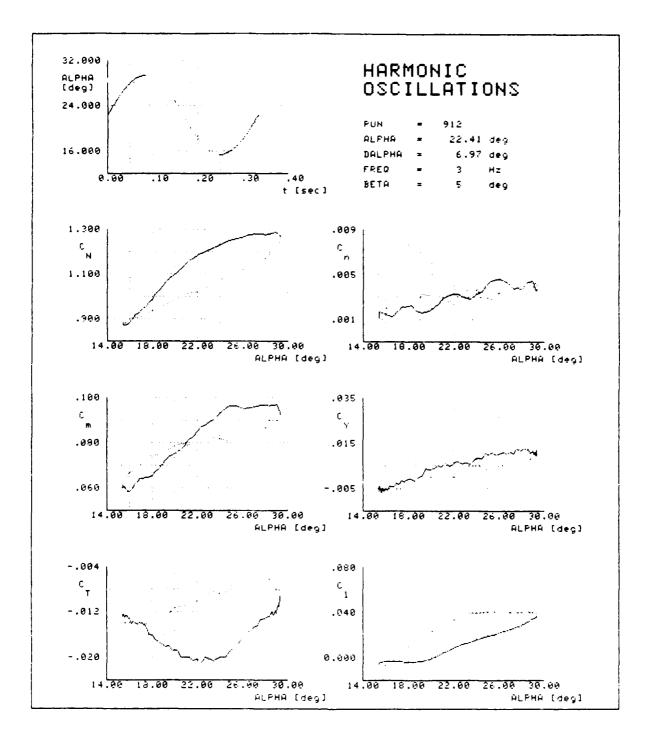


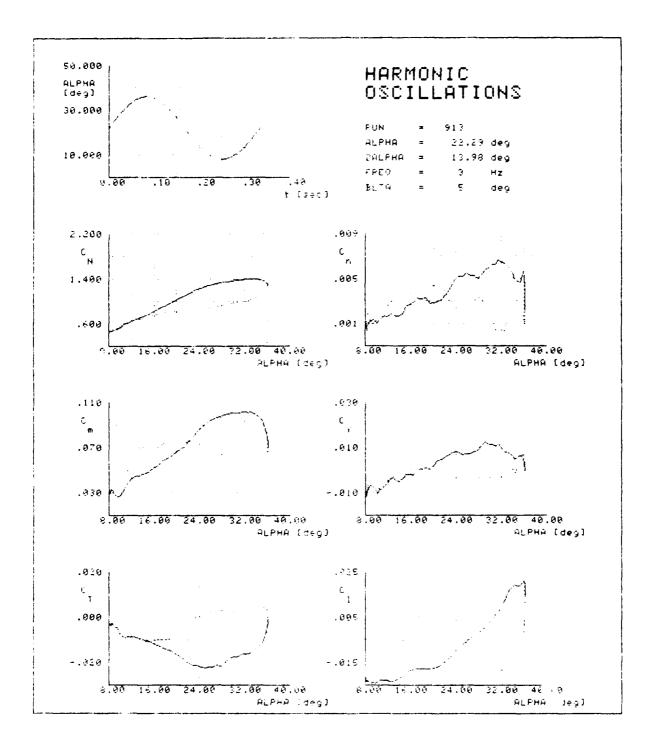


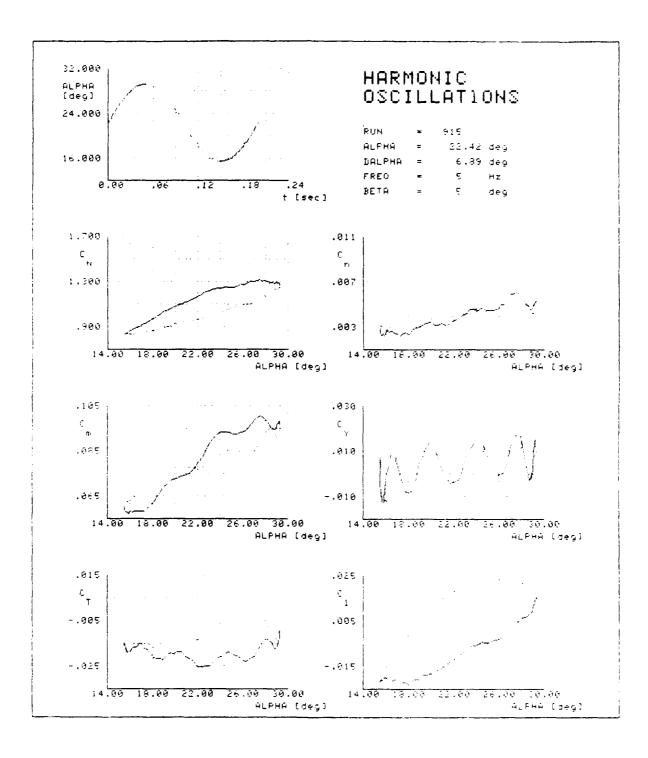
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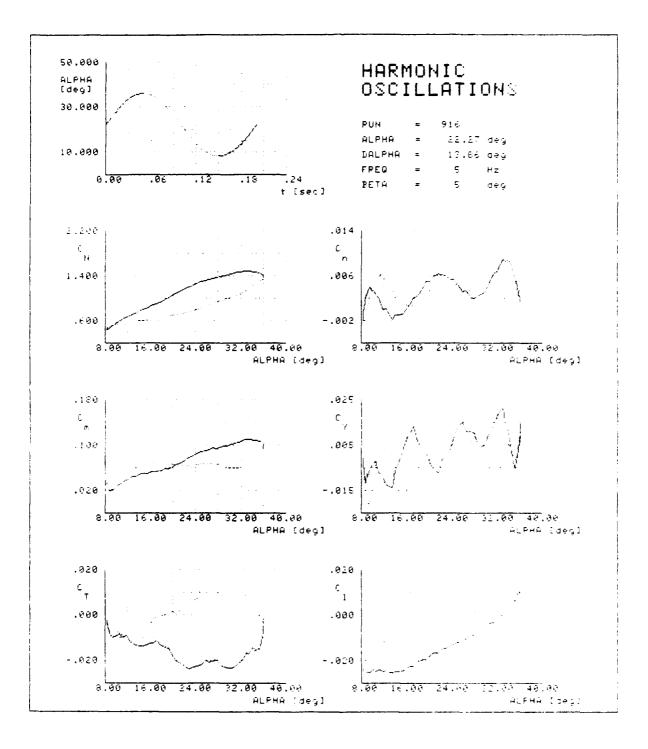


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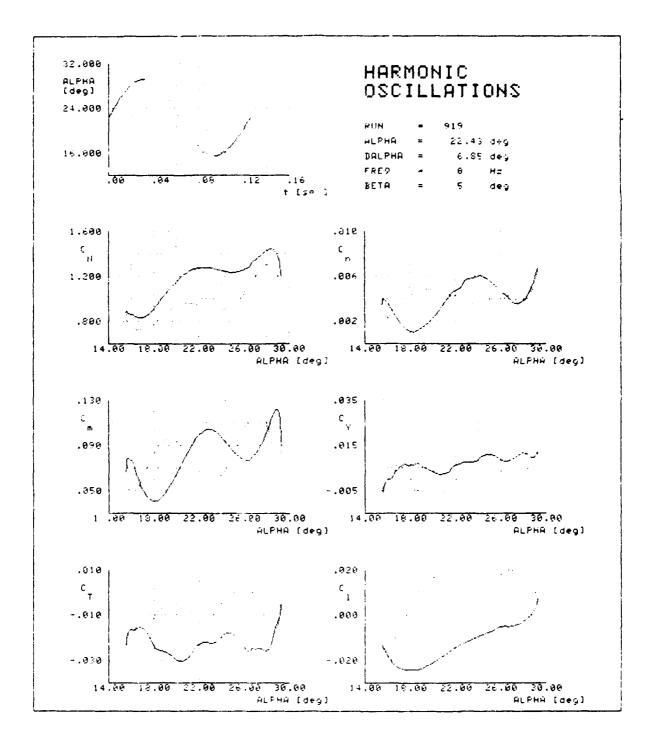


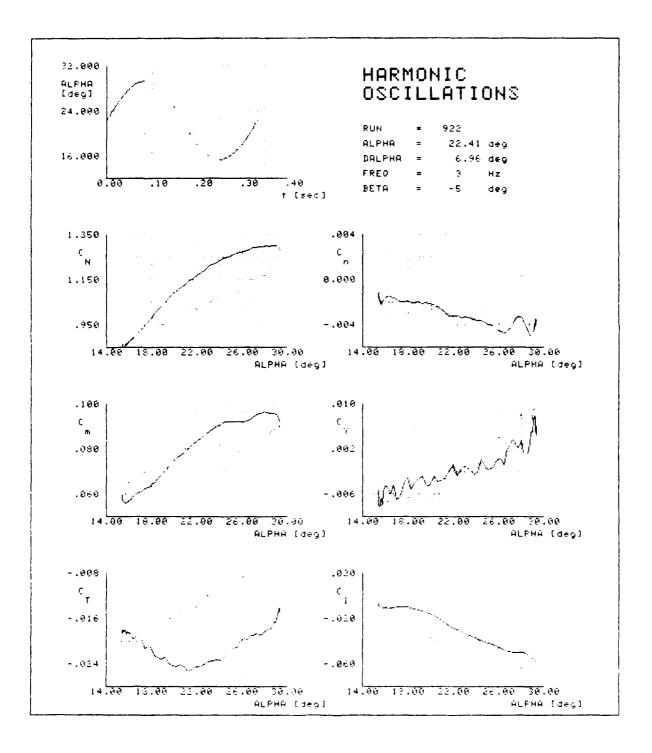


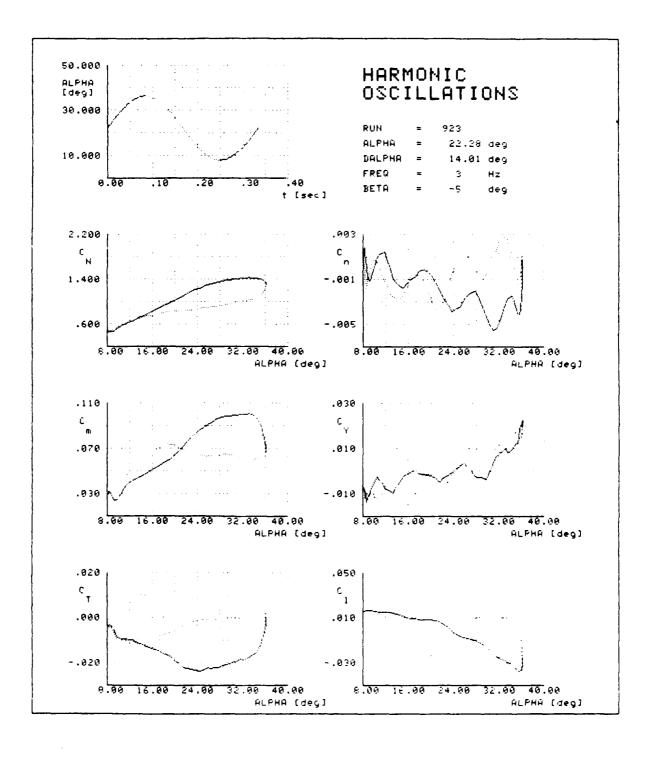


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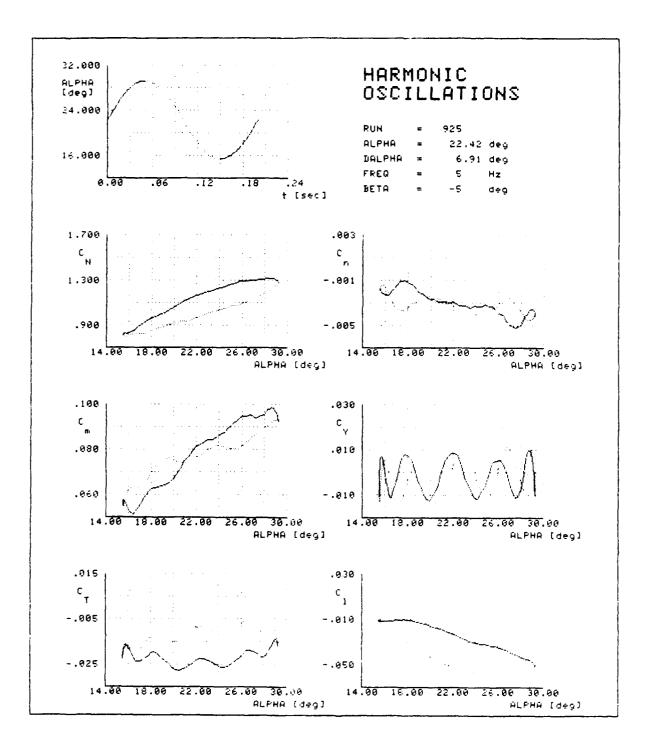
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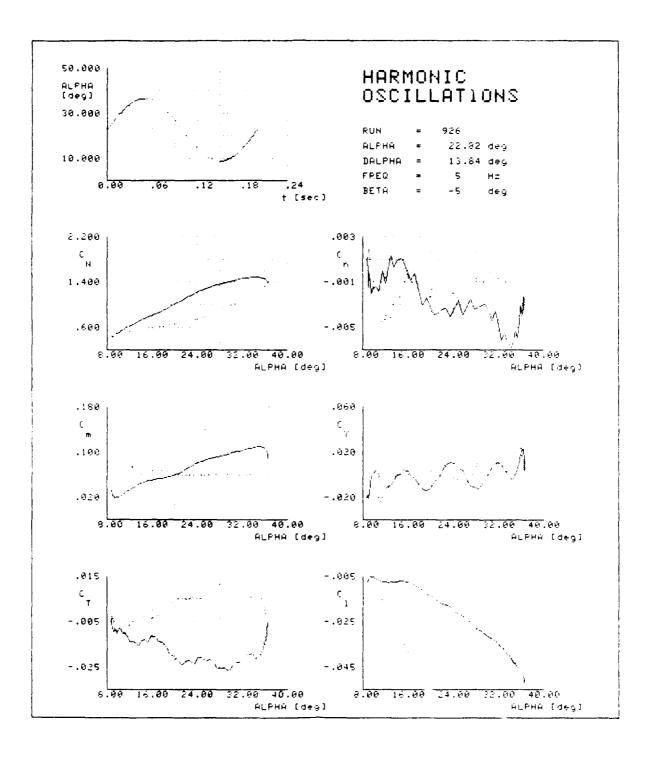


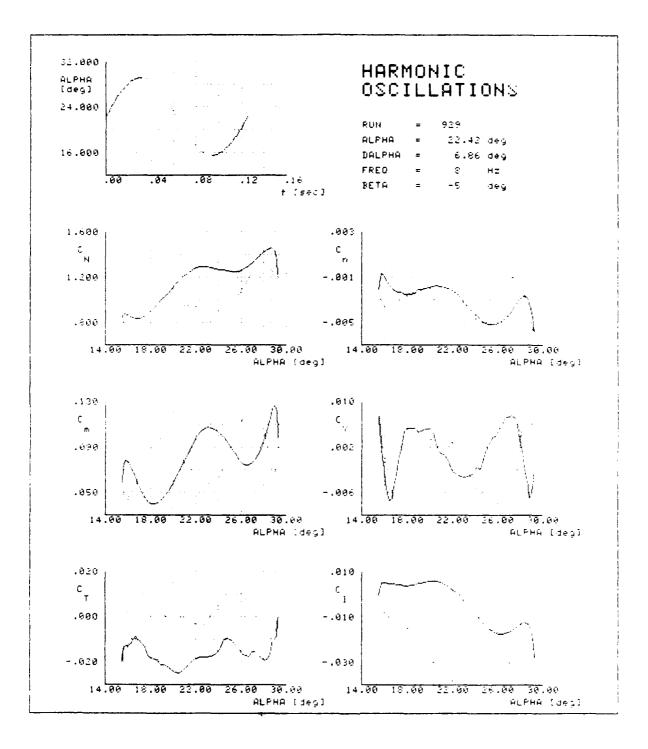


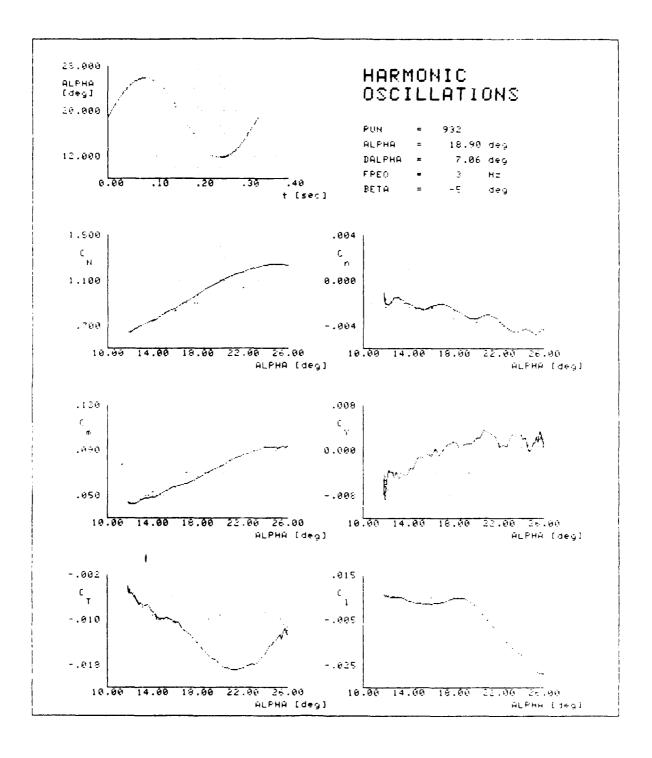


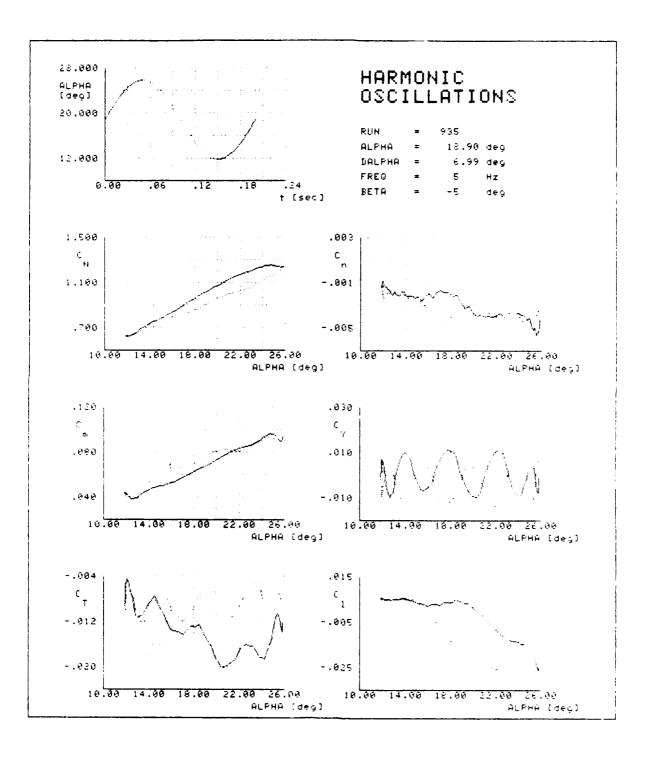
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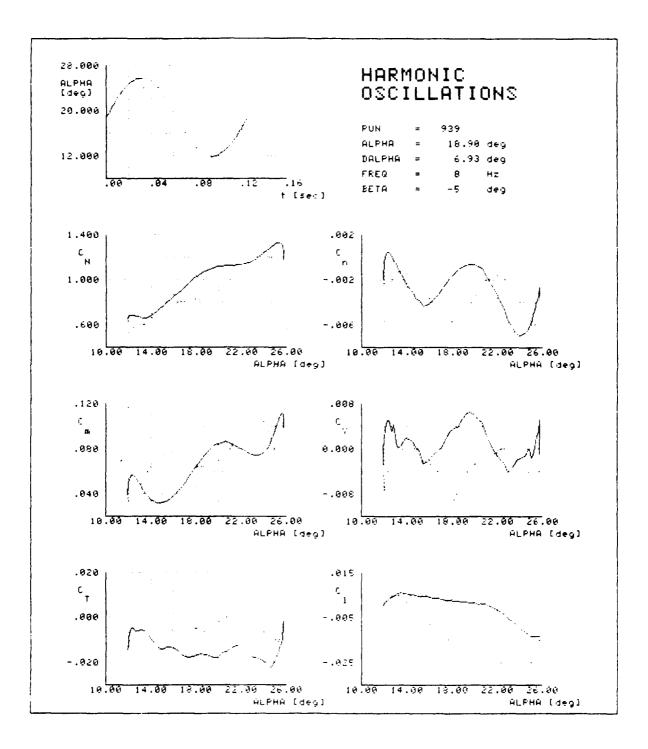


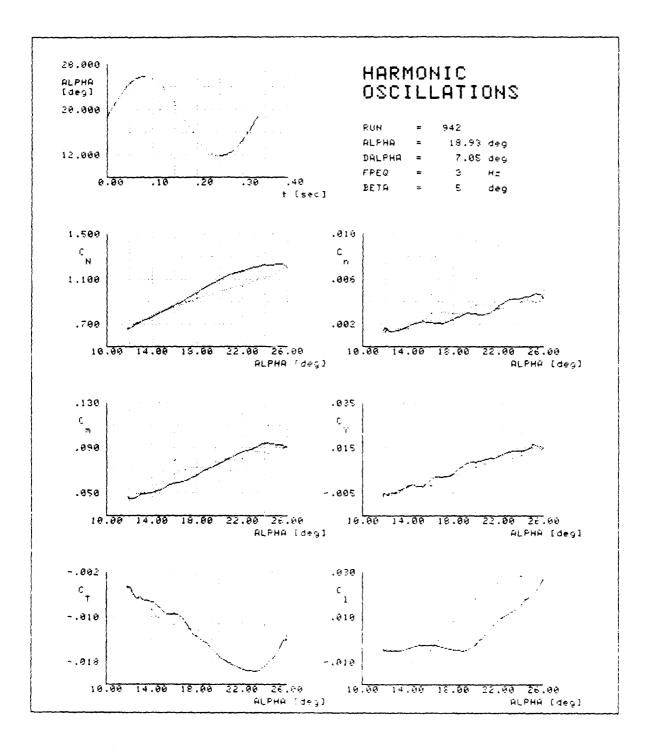


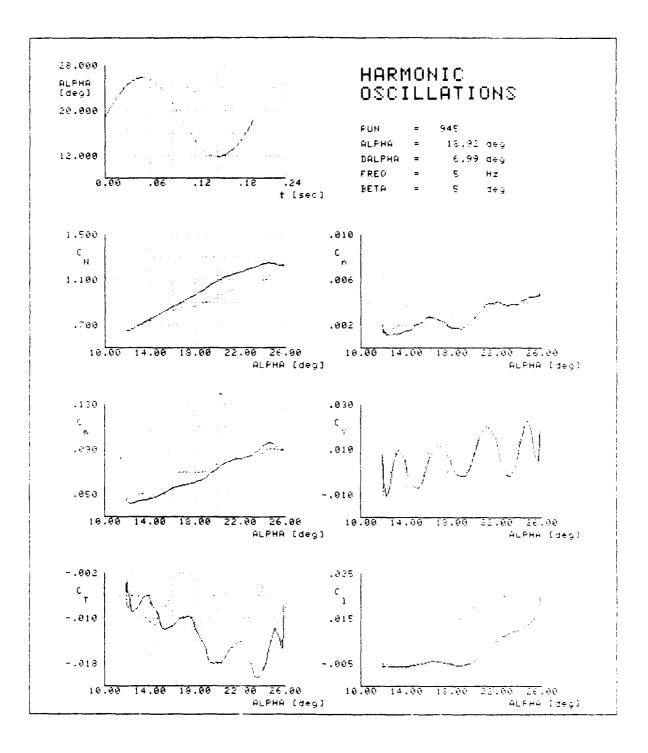


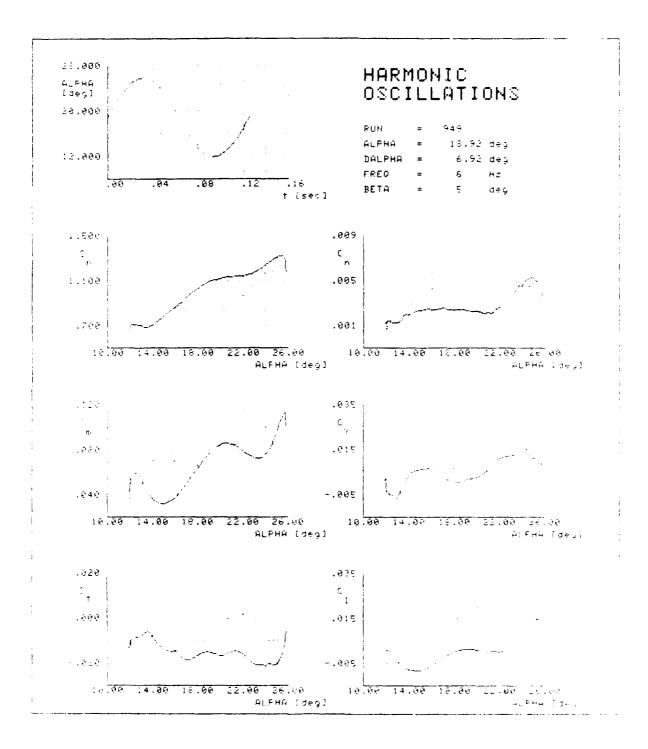


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